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U N C L A S S I F I E D

Security Classification

DOCUMENT CONTROL DATA - R & D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1. ORIGINATING ACTIVITY (Corporate authority)

NAVAL AIR DEVELOPMENT CENTER
AIR VEHICLE TECHNOLOGY DEPARTMENT
WARMINSYER, PENNSYLVANIA 18974

2a. REPORT SECURITY CLASSIFICATION

UNCLASSIFIED

2b. GROUP

REPORT TITLE

FINAL REPORT - EFFECT OF LUBRICATION ON THE JOINT BEARING STRENGTH OF RIVETED
LAP JOINTS

4. DESCRIPTIVE NOTES (Type of report and inclusive dates)

FINAL REPORT

5. AUTHOR(S) (First name, middle initial, last name)

FRANKLIN, T. PERRY

6. REPORT DATE

4 APRIL 1972

7a. TOTAL NO. OF PAGES

101

7b. NO. OF FIGS.

4

8a. CONTRACT OR GRANT NO.

b. PROJECT NO.

AIRTASK NO. A05-530/202-1/2000000000

c. WORK UNIT NO. 01

d.

9. ORIGINATOR'S REPORT NUMBER (S)

NADC-72055-VT

10. OTHER REPORT (S) (Any other numbers that may be assigned this report)

11. DISTRIBUTION STATEMENT

APPROVED FOR PUBLIC RELEASE; DISTRIBUTION UNLIMITED.

12. SUPPLEMENTARY NOTES

13. DISTRIBUTION STATEMENT

NAVAL AIR SYSTEMS COMMAND
DEPARTMENT OF THE NAVY

14. ABSTRACT

This report contains the results of an investigation
of joint shear strengths using solid rivet fasteners
lubricated with lauric acid.



DEPARTMENT OF THE NAVY
NAVAL AIR DEVELOPMENT CENTER
WARMINSTER, PA. 18974

AIR VEHICLE TECHNOLOGY DEPARTMENT

REPORT NO. NADC-72055-VT

4 APRIL 1972

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STRENGTH OF RIVETED LAP JOINTS

FINAL REPORT
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EVALUATION AND DISCUSSION

INTRODUCTION

The yield and ultimate shear strength of joints fabricated from various metals using solid rivet fasteners lubricated with lauric acid is reported herein. The results of the investigations showing a reduction of material bearing strength when pins and threaded fasteners were lubricated with lauric acid have been reported in references (a) and (b) respectively.

TEST PROCEDURE

Joint yield and ultimate strengths were determined in accordance with reference (c), using a Tinius Olsen Universal Testing Machine, Model Super "L" UTM Serial 54984-3, and a Baldwin Extensometer, Model TSMD Serial 1029 (Figures 1 and 2). All the rivets and sheet material were initially cleaned ultrasonically in chloroethene V.G.S.A. 1192A. Tests were performed on the clean riveted lap joint specimens, and the yield and ultimate strength was recorded. To determine the effect of lubrication, rivets were then coated with lauric acid ($\text{CH}_3(\text{CH}_2)_{10}\text{COOH}$) and specimens fabricated. The tests were repeated. The test specimens were .063 inches thick, and the rivet holes in the specimens were within a tolerance range of .253 to .257 inches. The installation requirements to form the flat driven heads on the rivets used in the test were in accordance with reference (d).

The four materials used in this investigation included aluminum (2024-T3 Sheet-Heats 1-2), magnesium (AZ31B-H24 Sheet), and steel (PH15-7 Mo Sheet). Rivets of the following types and the driving pressures that were required to form the fastener heads in the lap joints are shown below:

<u>Type</u>	<u>Material</u>	<u>Driving Pressure</u>
MS20470D8-6	Aluminum	12,000 lbs.
MS20470B8-6	Magnesium	9,000 lbs.
NAS1198-8-6	Steel	22,000 lbs.

DISCUSSION

All specimens were subjected to the joint shear test specified in reference (c). One half of the ultrasonically cleaned specimens were tested with rivets that had been lubricated with lauric acid. Careful control of all significant parameters was exercised to determine any effect upon the lap joints' bearing yield and bearing ultimate strength produced by lubrication of the rivets.

Joint yield strength was determined from load deflection curves using the second modulus method for hole filling fasteners in accordance with reference (c). The bearing yield loads are shown on the load deflection charts, Figures 3 through 82. The joint bearing yield and bearing ultimate strength was calculated by dividing the applicable load carried by the bearing area. The results obtained are shown in Tables I through VIII. The average strength of the lap joint specimens tested with lubricated rivets was consistently lower than those of the specimens tested with non-lubricated rivets, Table IX.

CONCLUSIONS

It is concluded that joints fabricated with lubricated rivets, like those fabricated with lubricated threaded fasteners, have lower bearing yield and bearing ultimate joint strengths than when fabricated with clean fasteners.

RECOMMENDATIONS

It is recommended that this effect be considered in the preparation of MIL-HDBK-5 since the reductions are not the same for hole filling fasteners (rivets), non-hole filling fasteners (bolts), and sheet materials.

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R E F E R E N C E S

- (a) NAVAIRDEVCON Report No. NADC-MA-7007 of 31 Dec 1970, Effect of Lubrication on the Bearing Strength of Various Metallic Materials
- (b) NAVAIRDEVCON Report No. NADC-MA-7162 of 27 Sep 1971, Effect of Lubrication on the Joint Bearing Strength of Metal Joints
- (c) MIL-STD-1312 Notice 1 - Test 4, Joint Shear Strength
- (d) NAVAIR 01-1A-8 Technical Manual Structural Hardware

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ALUMINUM
2024-T3
HEAT-1
(ALCOA)

NOT LUBRICATED			LUBRICATED		
SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)	SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)
1-A	101,269	138,095	4-AW	93,650	106,031
2-A	101,587	135,238	3-AW	91,746	111,111
3-A	101,587	136,507	5-AW	91,746	114,920
5-A	101,904	136,825	2-AW	92,063	116,825
7-A	98,412	136,825	6-AW	90,793	118,095
AVG.	100,951	136,698		91,999	113,346

NOTE:

8.8% decrease in bearing yield strength when lubricated.

17.0% decrease in bearing ultimate strength when lubricated.

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ALUMINUM
2024-T3
HEAT-2
(HARVEY)

NOT LUBRICATED			LUBRICATED		
SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)	SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)
2-H	103,174	136,507	12-HW	90,476	111,746
3-H	107,396	137,142	14-HW	89,841	113,333
4-H	108,888	137,777	18-HW	90,158	115,555
7-H	106,349	139,047	11-HW	87,619	117,460
1-H	99,682	145,396	16-HW	93,333	119,682
AVG.	105,097	139,173		90,285	115,555

NOTE:

14.0% decrease in bearing yield strength when lubricated.

16.9% decrease in bearing ultimate strength when lubricated.

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MAGNESIUM
H-5070
(DOW)

NOT LUBRICATED			LUBRICATED		
SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)	SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)
3-D	66,349	86,349	15-DL	60,317	83,809
1-D	71,428	88,571	18-DL	63,492	83,492
6-D	72,065	88,888	17-DL	60,372	84,444
7-D	65,714	89,523	10-DL	66,031	87,301
11-D	65,079	90,476	16-DL	61,904	86,031
AVG.	68,126	88,761		62,423	85,015

NOTE:

8.3% decrease in bearing yield strength when lubricated.

4.2% decrease in bearing ultimate strength when lubricated.

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MAGNESIUM
7546
AZ31B

NCT LUBRICATED			LUBRICATED		
SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)	SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)
2-M	67,619	82,539	4-ML	58,412	79,047
5-M	68,571	85,079	1-ML	58,095	81,904
3-M	68,253	85,714	8-ML	57,142	81,904
4-M	68,888	86,984	6-ML	60,317	81,904
10-M	69,841	88,253	5-ML	59,365	82,539
AVG.	68,634	85,713		58,666	81,459

NOTE:

14.5% decrease in bearing yield strength when lubricated.

4.9% decrease in bearing ultimate strength when lubricated.

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MAGNESIUM
C-70065
(DOW)

NOT LUBRICATED			LUBRICATED		
SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)	SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)
D-2	60,317	82,222	13-DL	55,555	77,142
D-1	60,317	82,857	16-DL	55,873	78,412
D-5	60,634	83,492	10-DL	55,873	78,730
D-7	63,492	84,126	12-DL	57,142	79,882
D-8	60,634	85,398	11-DL	56,825	80,000
AVG.	61,078	83,619		56,253	78,833

NOTE:

7.8% decrease in bearing yield strength when lubricated.

5.7% decrease in bearing ultimate strength when lubricated.

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STEEL
870255

NOT LUBRICATED			LUBRICATED		
SPECIMEN NO.	BEARING YIELD STRENGTH (FSI)	BEARING ULTIMATE STRENGTH (PSI)	SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)
SA-4	126,666	229,841	SAL-8	104,761	205,714
SA-9	133,650	234,920	SAL-1	104,761	204,444
SA-2	133,333	228,571	SAL-4	93,650	195,873
SA-5	126,984	228,253	SAL-6	101,587	182,539
SA-6	139,682	225,079	SAL-9	107,936	208,888
AVG.	132,063	229,332		102,539	199,491

NOTE:

22.3% decrease in bearing yield strength when lubricated.

13.0% decrease in bearing ultimate strength when lubricated.

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STEEL
851064

NOT LUBRICATED			LUBRICATED		
SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)	SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)
SB-3	101,587	208,571	SBL-9	111,111	193,650
SB-5	120,634	213,650	SBL-3	117,460	196,190
SB-4	129,841	214,920	SBL-7	104,761	199,365
SB-2	123,809	215,555	SBL-4	111,111	187,619
SB-7	128,571	215,873	SBL-5	117,460	187,619
AVG.	120,888	213,713		112,380	192,888

NOTE:

7.0% decrease in bearing yield strength when lubricated.

9.7% decrease in bearing ultimate strength when lubricated.

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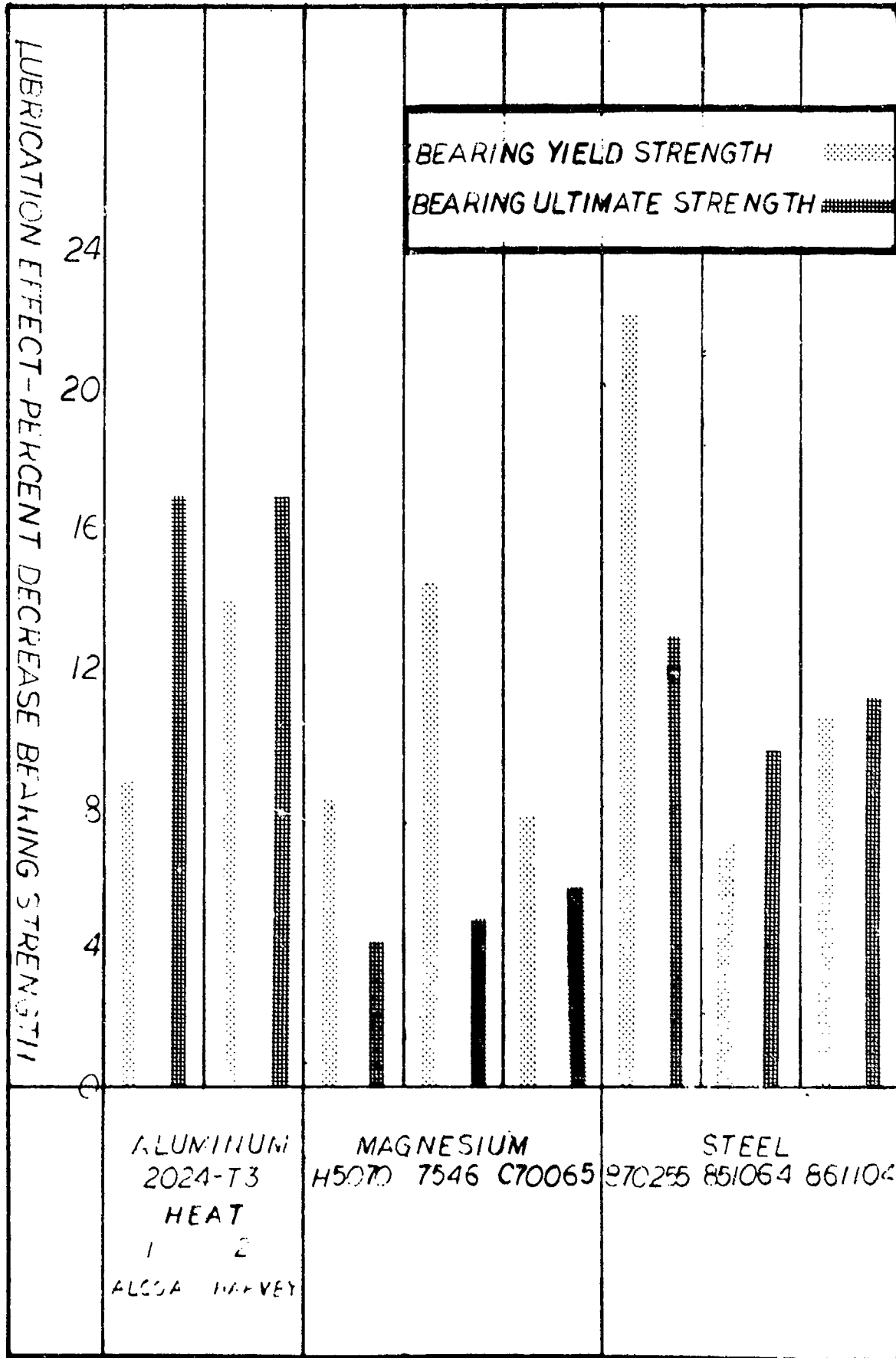
STEEL
861104

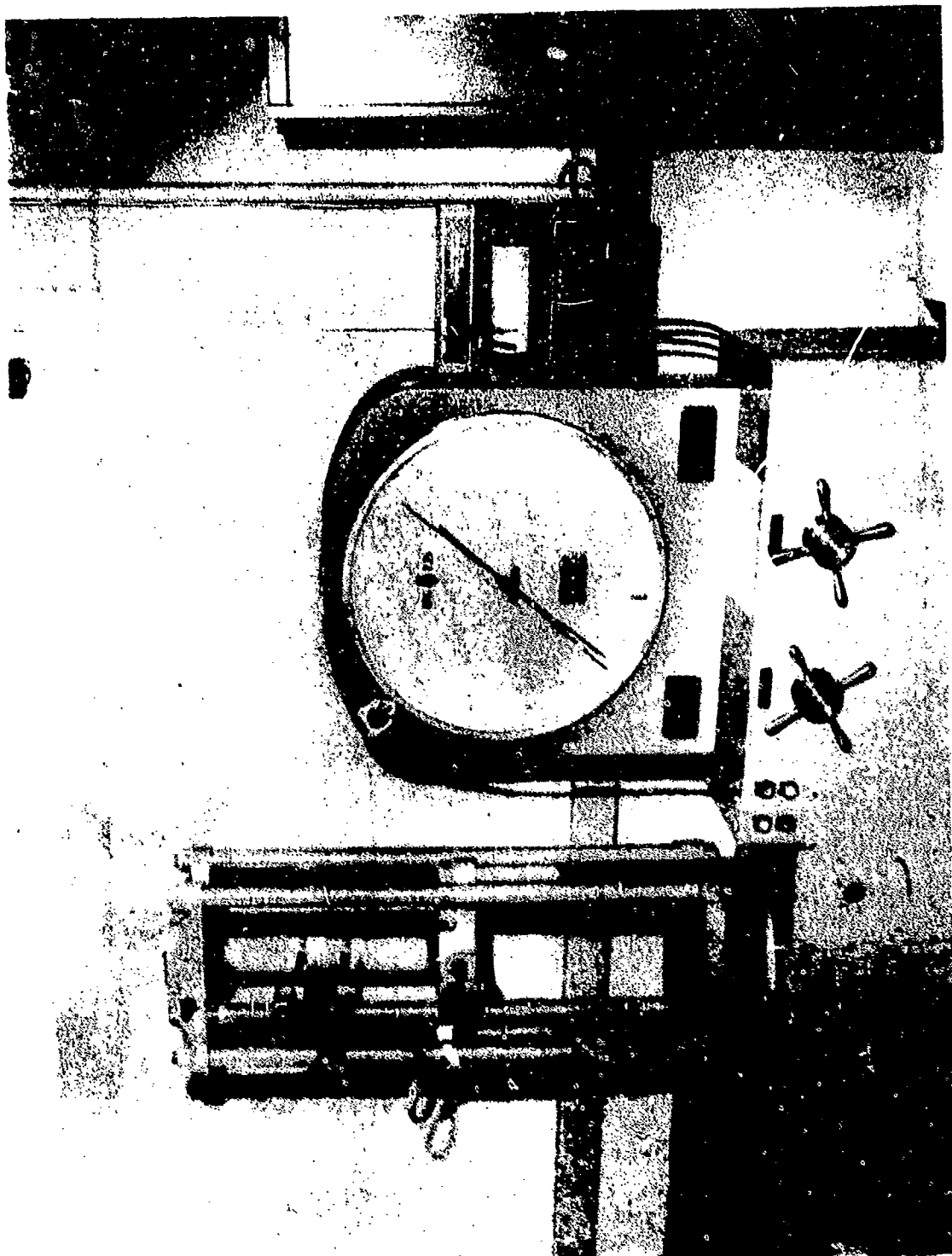
NOT LUBRICATED			LUBRICATED		
SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)	SPECIMEN NO.	BEARING YIELD STRENGTH (PSI)	BEARING ULTIMATE STRENGTH (PSI)
SC-6	117,460	215,555	SCL-18	114,285	196,190
SC-4	123,174	216,507	SCL-12	104,761	193,015
SC-7	120,634	219,047	SCL-15	107,936	191,111
SC-3	125,396	219,047	SCL-17	111,111	186,349
SC-5	128,235	226,349	SCL-11	111,111	205,079
AVG.	123,047	219,301		109,840	194,348

NOTE:

10.7% decrease in bearing yield strength when lubricated.

11.3% decrease in bearing ultimate strength when lubricated.



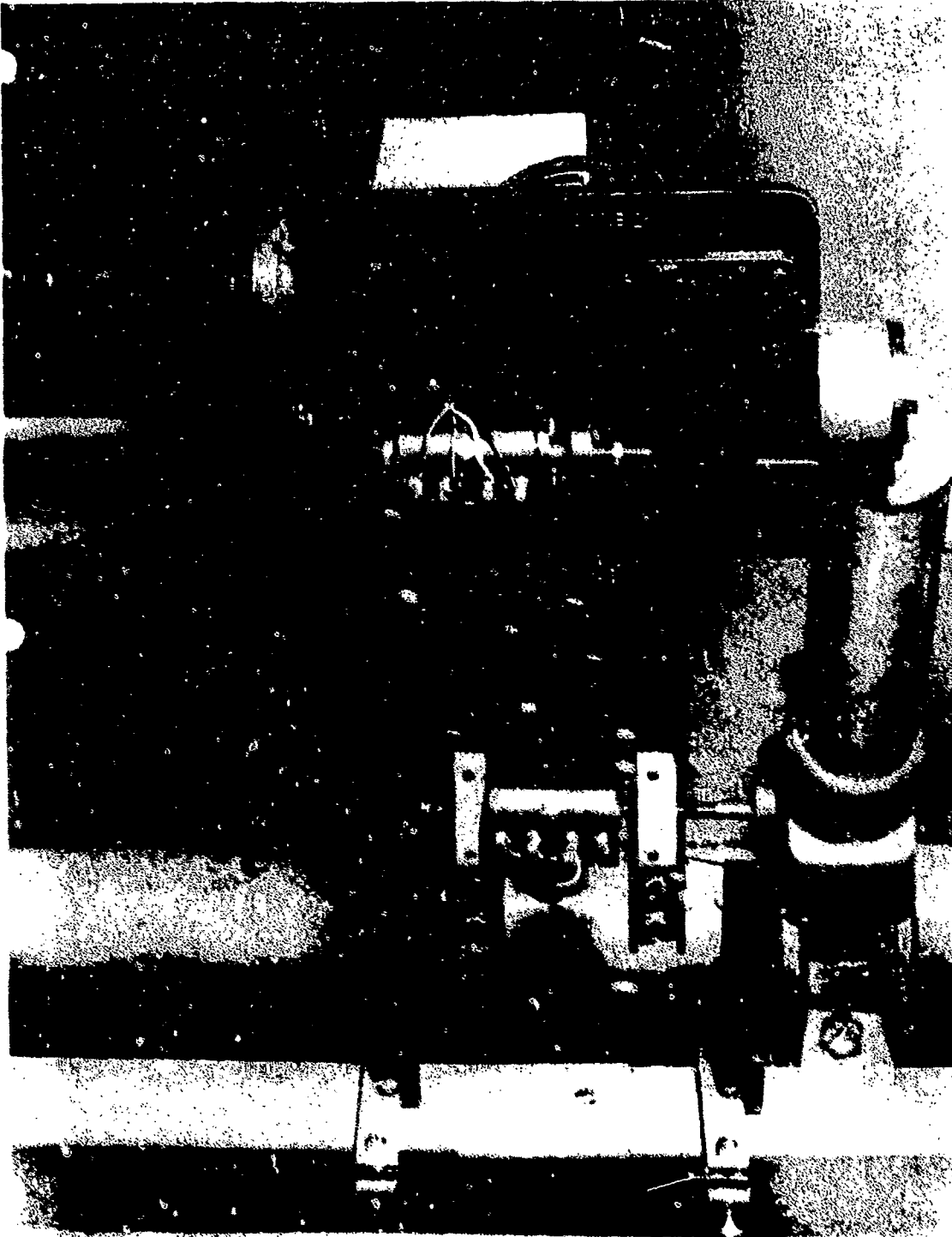


TINIUS OLSEN 60,000 LB. UNIVERSAL TESTING MACHINE

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TEST PICTURE

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best available copy.



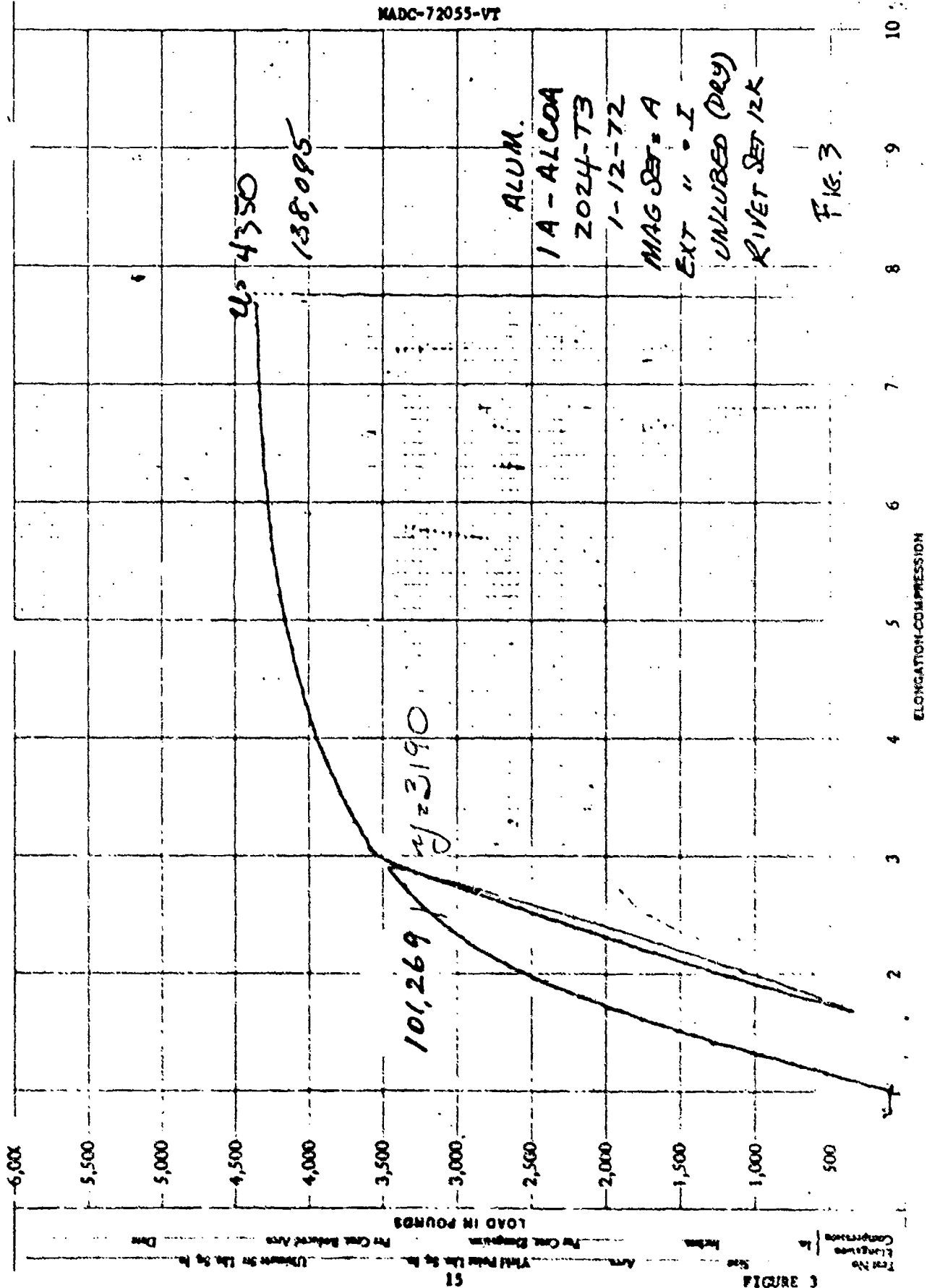
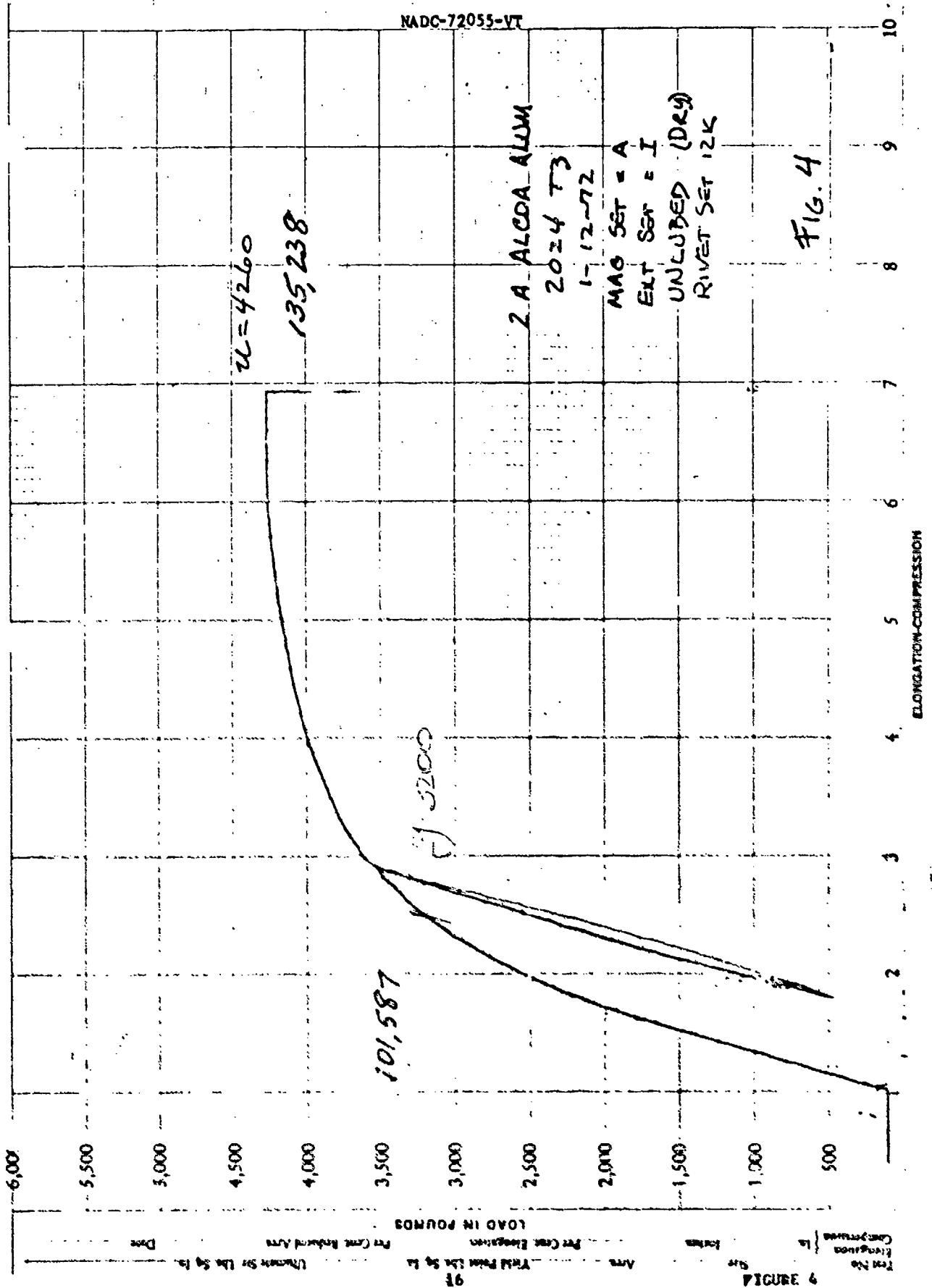


FIGURE 3



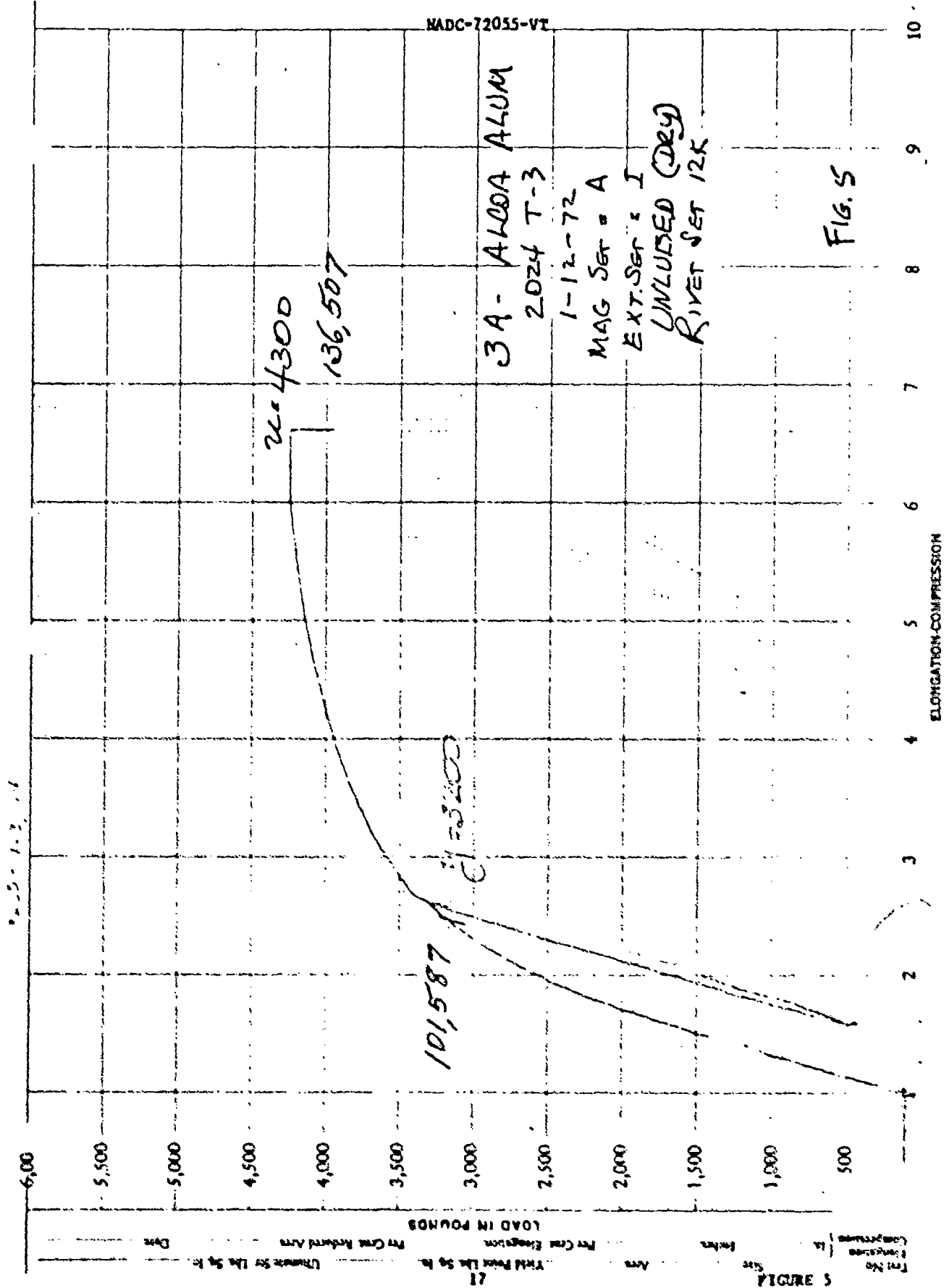
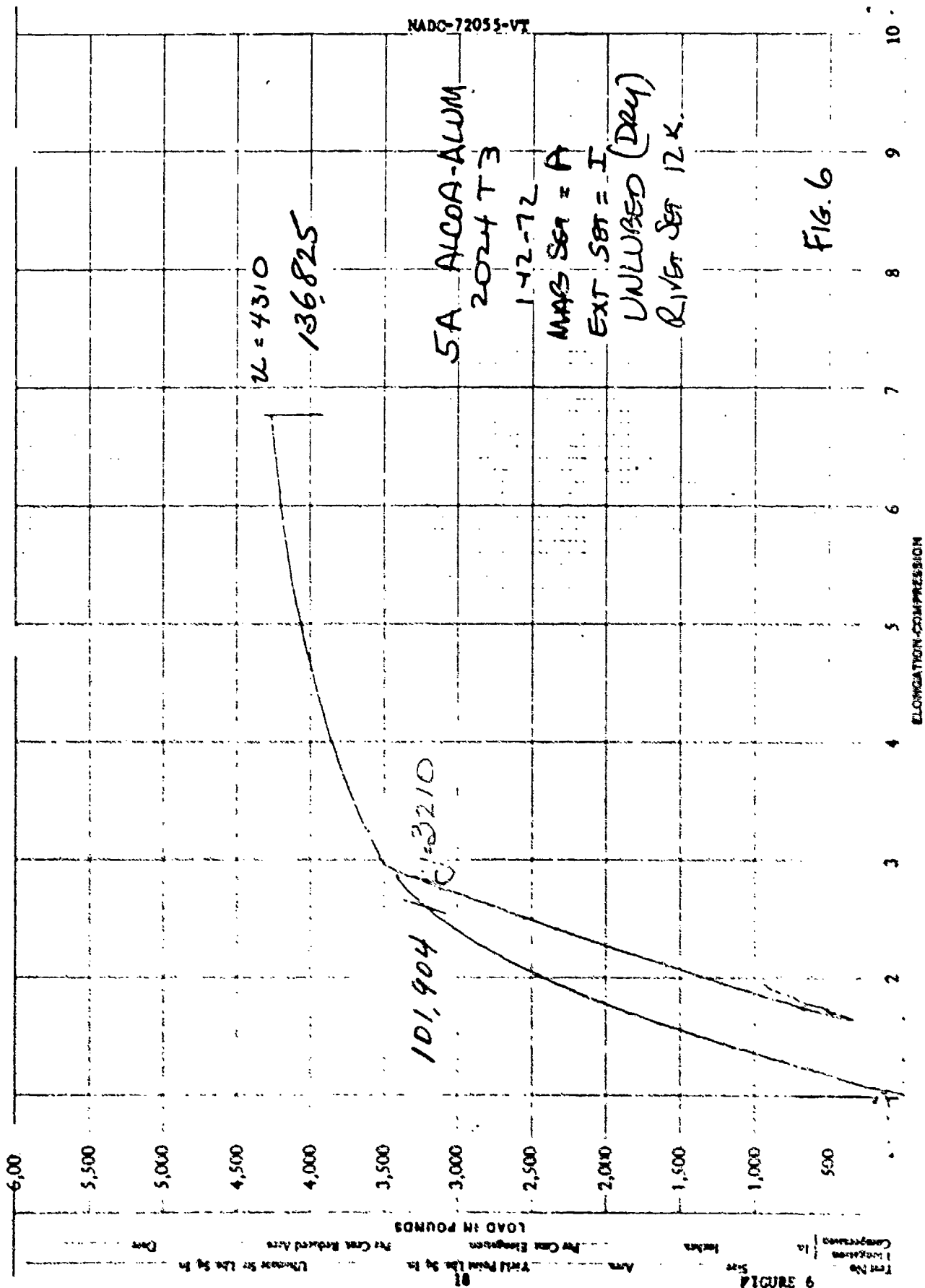


FIGURE 5

Test No. _____
 Compression _____
 Load _____
 Area _____
 Yield Point _____
 Ultimate _____
 Date _____

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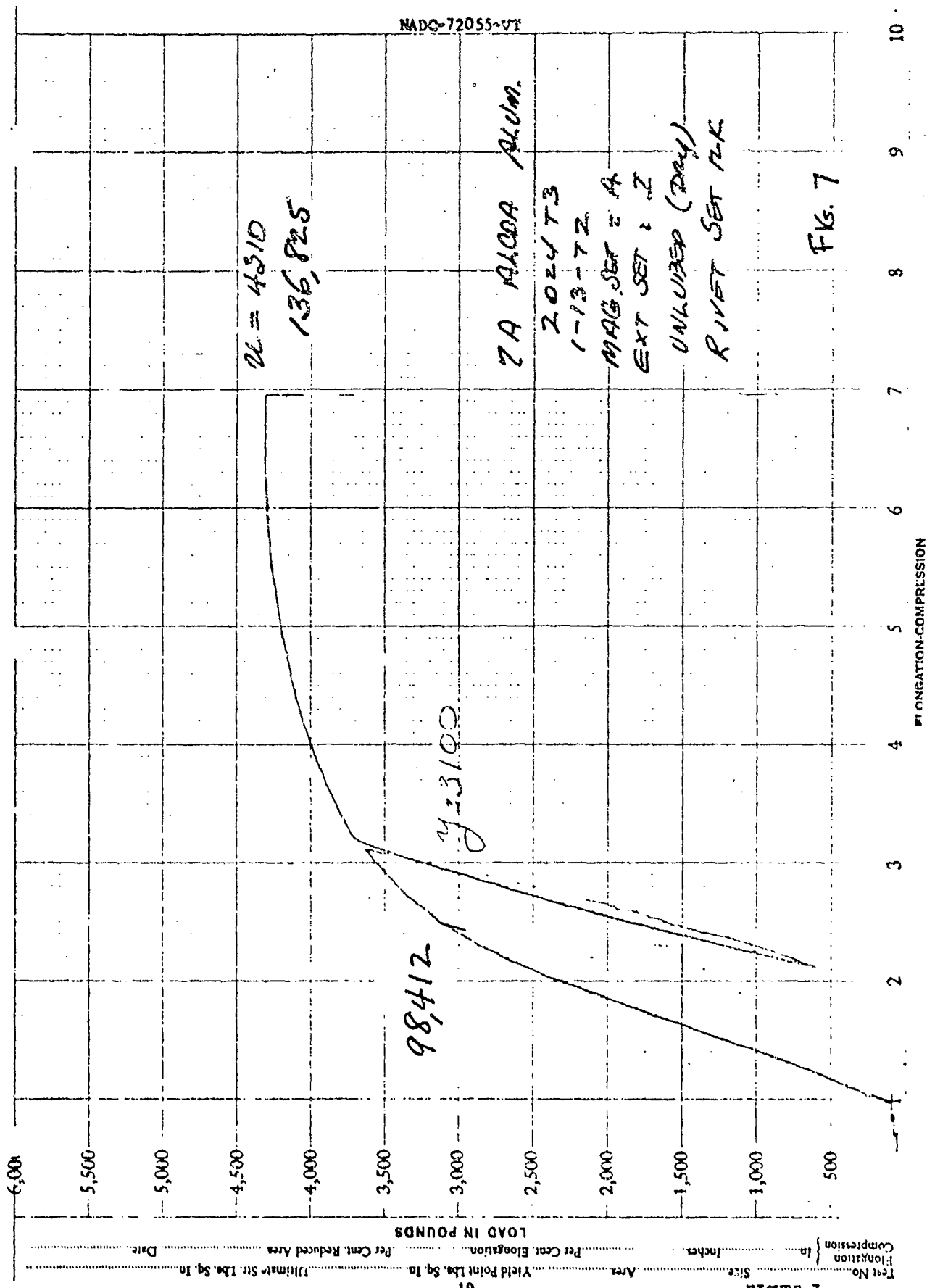
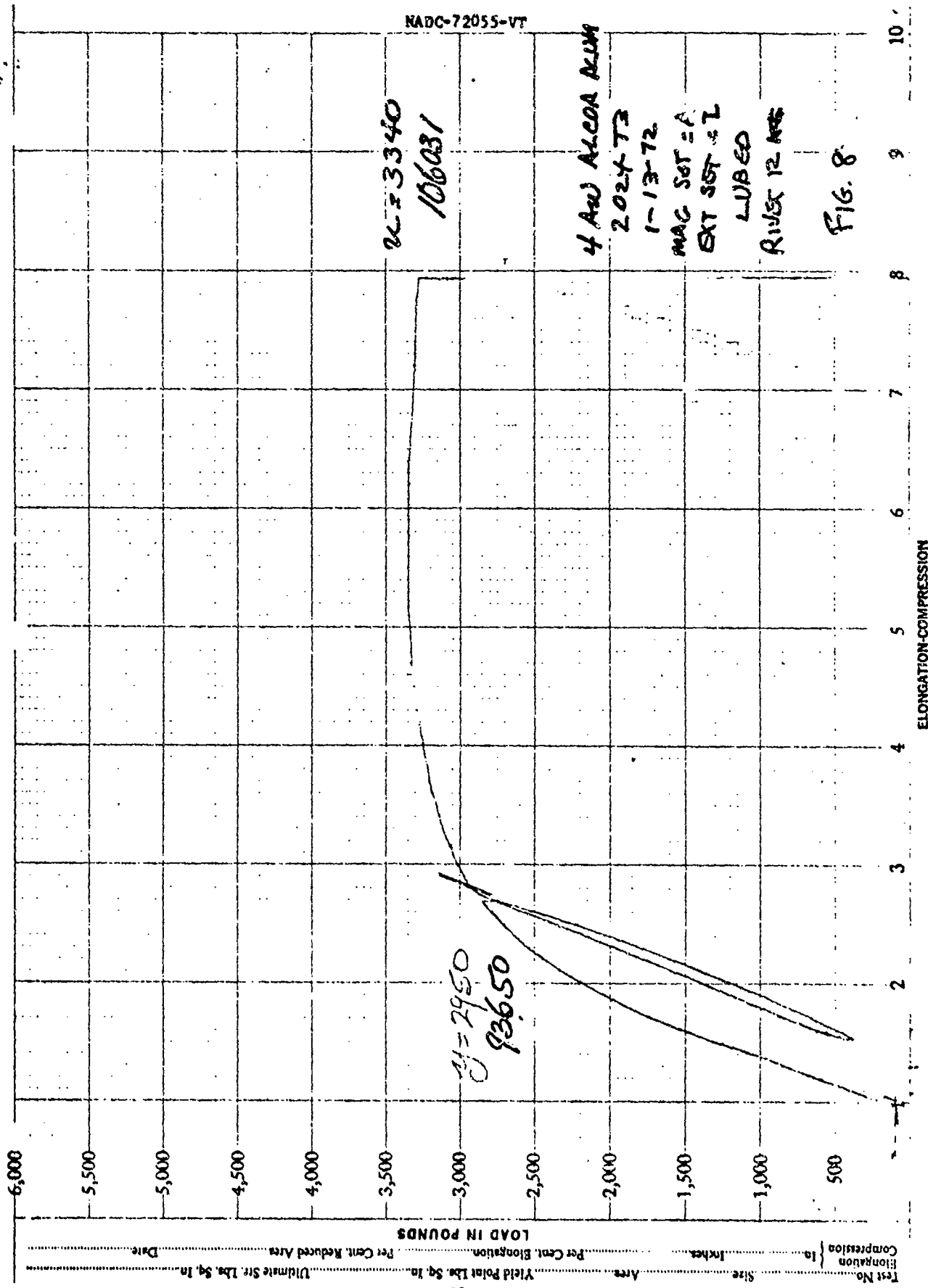


FIGURE 7

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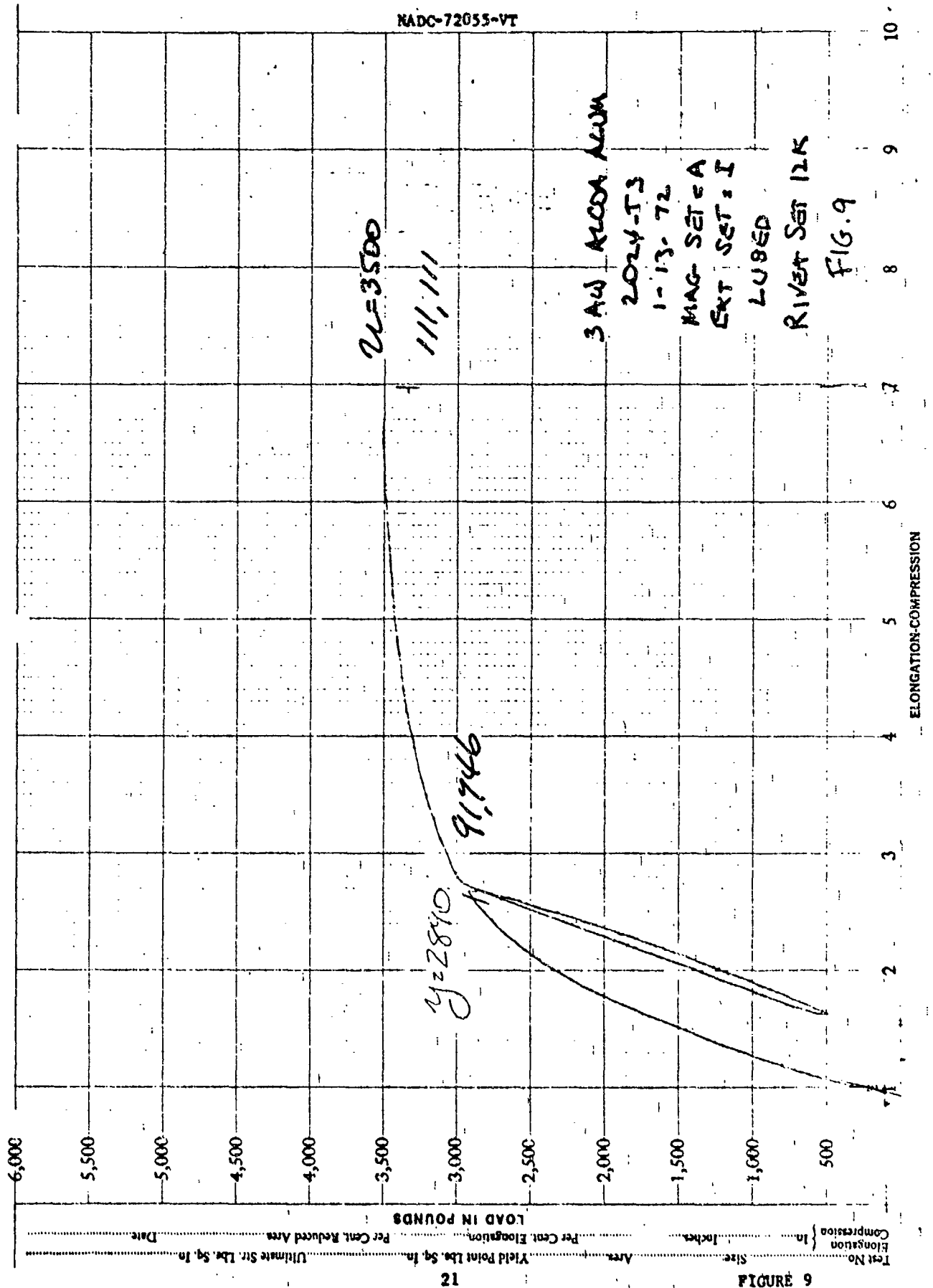
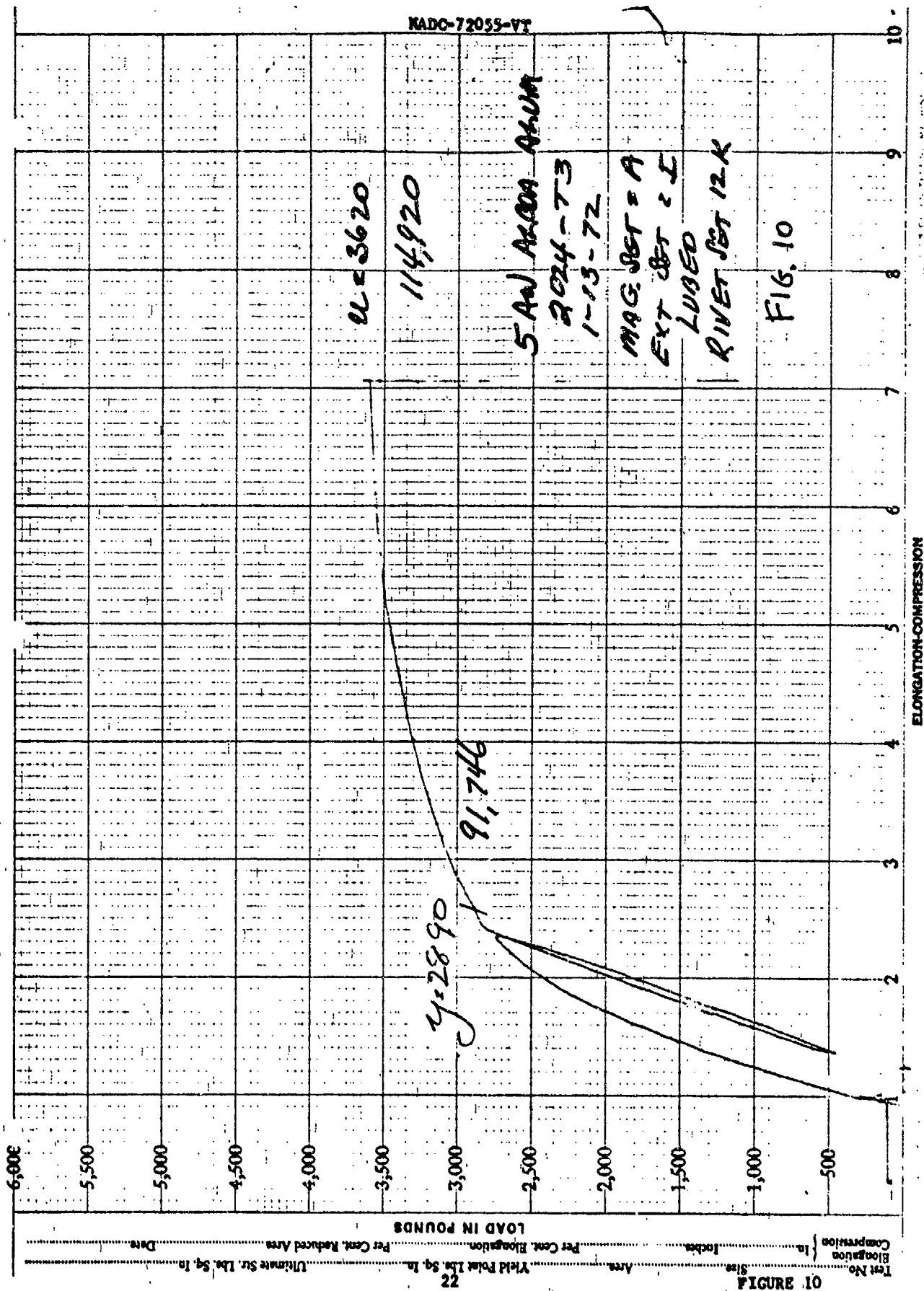


FIGURE 9



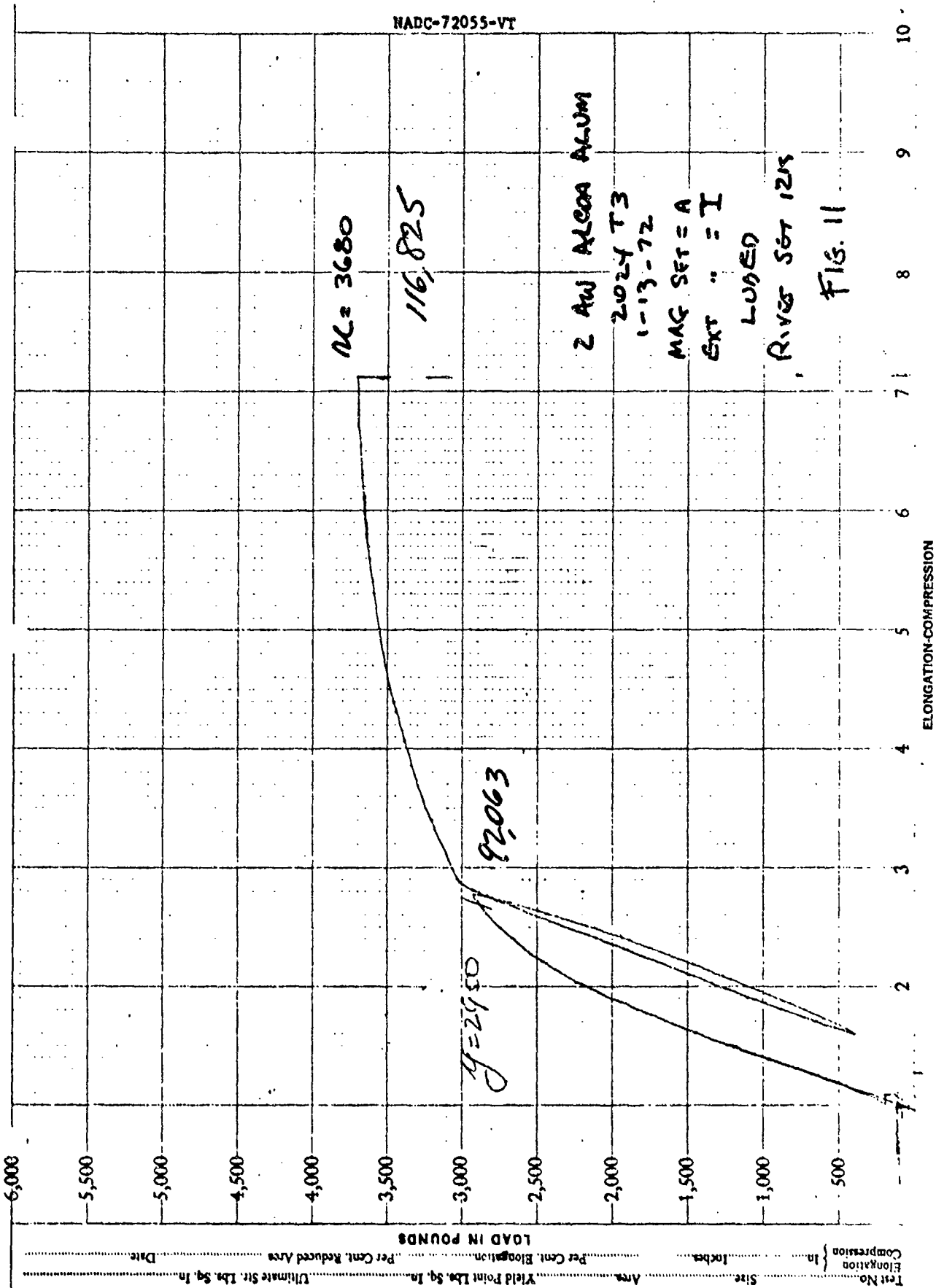


FIGURE 11

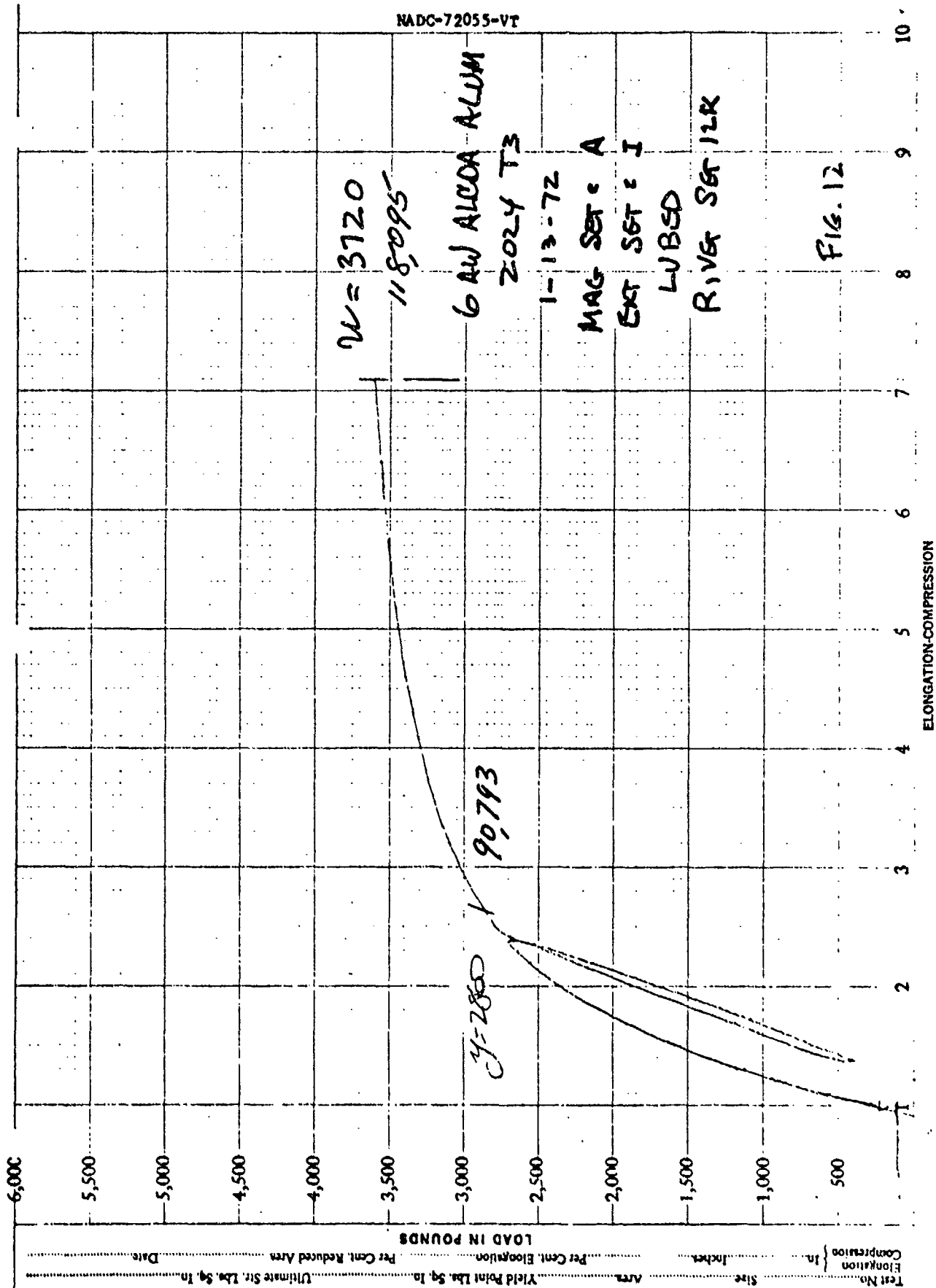
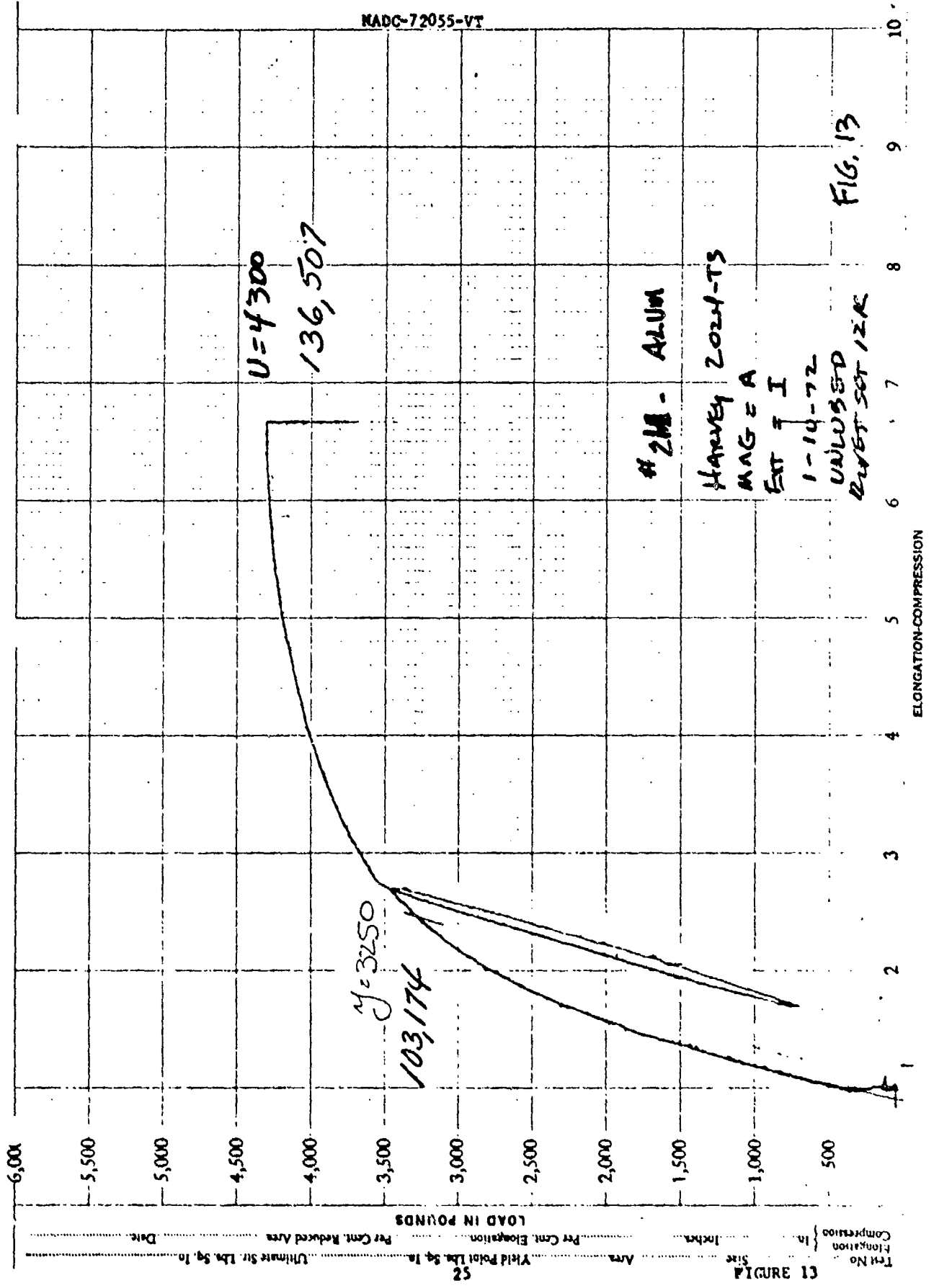


FIGURE 12



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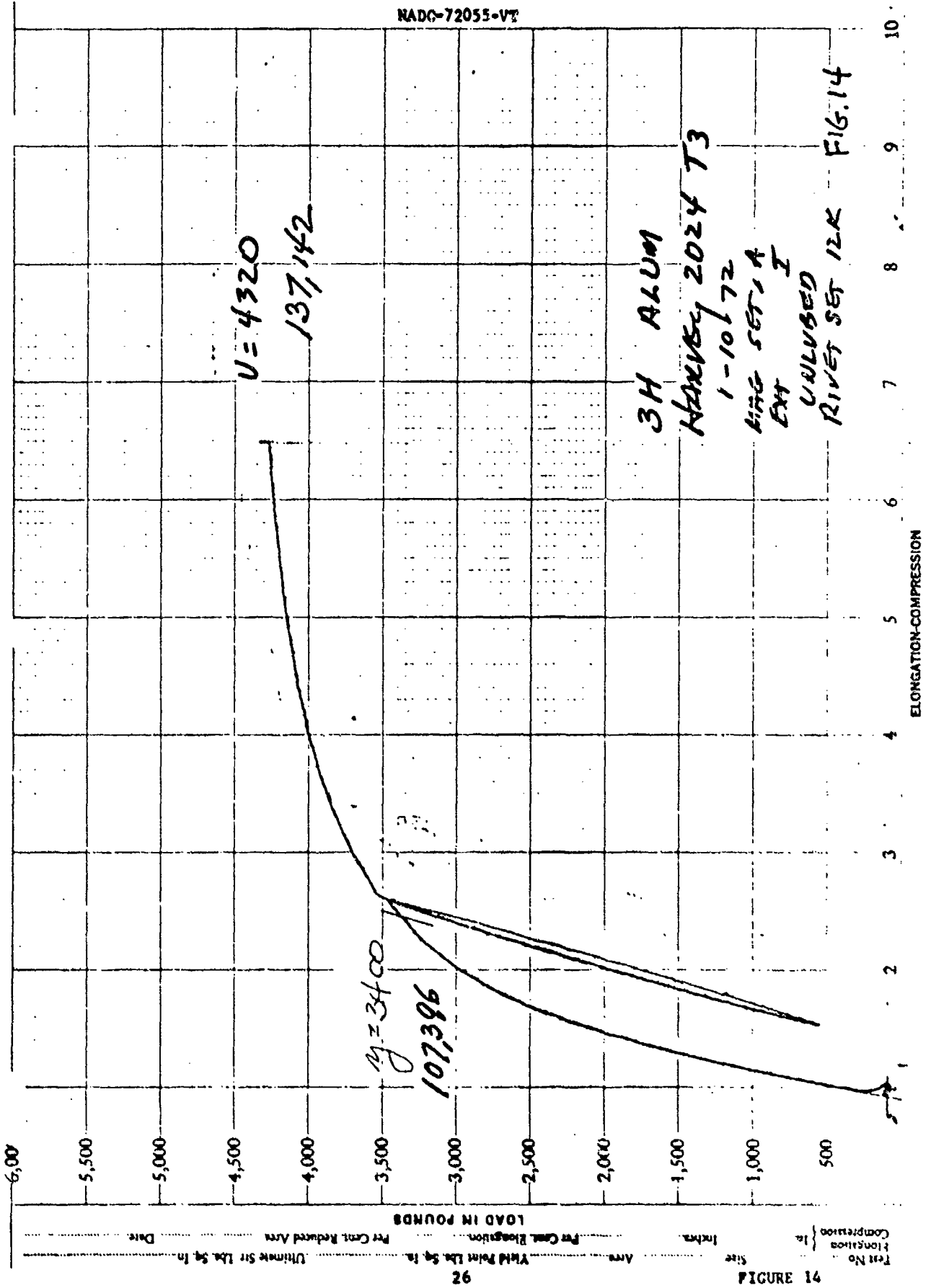
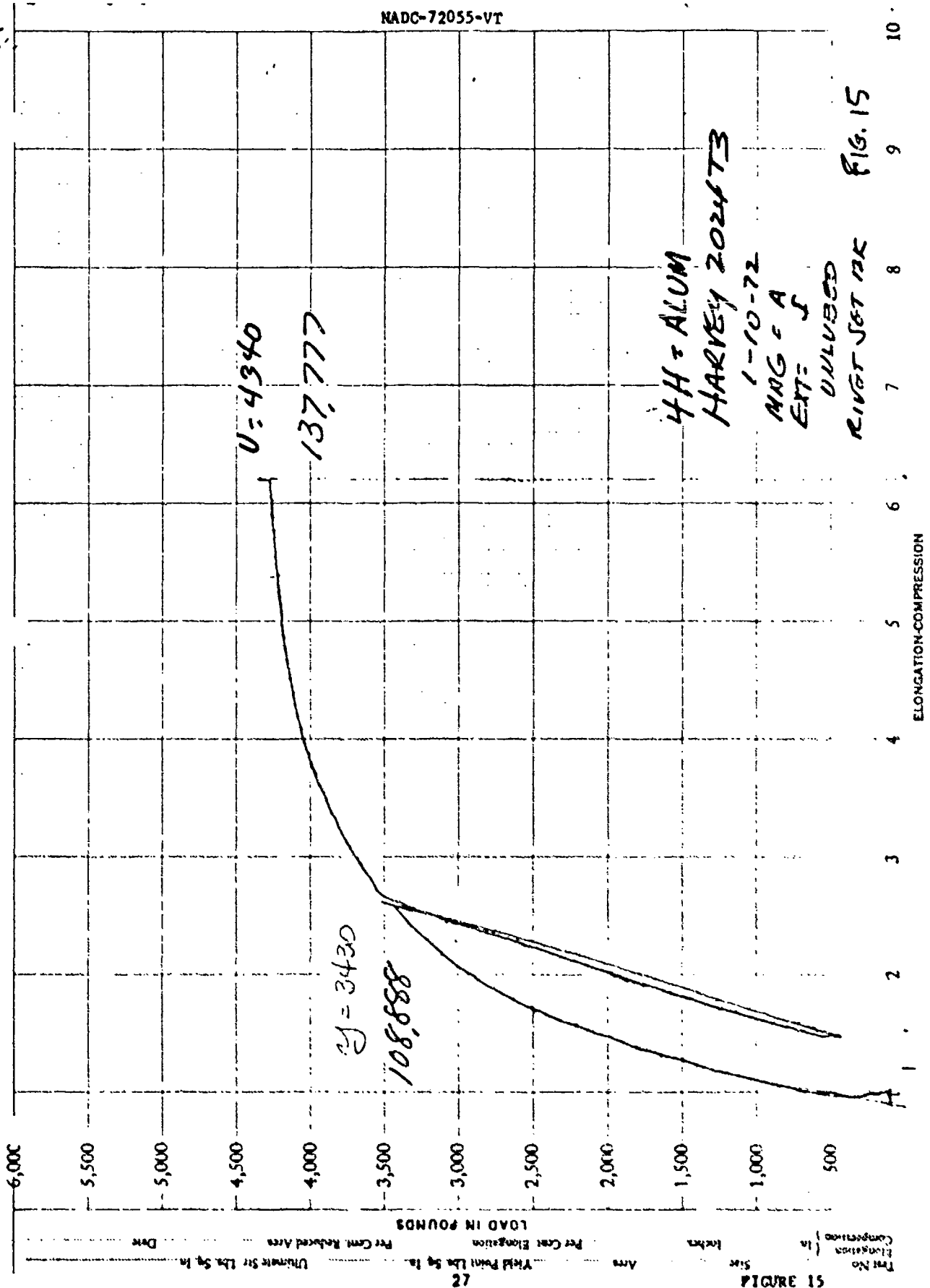
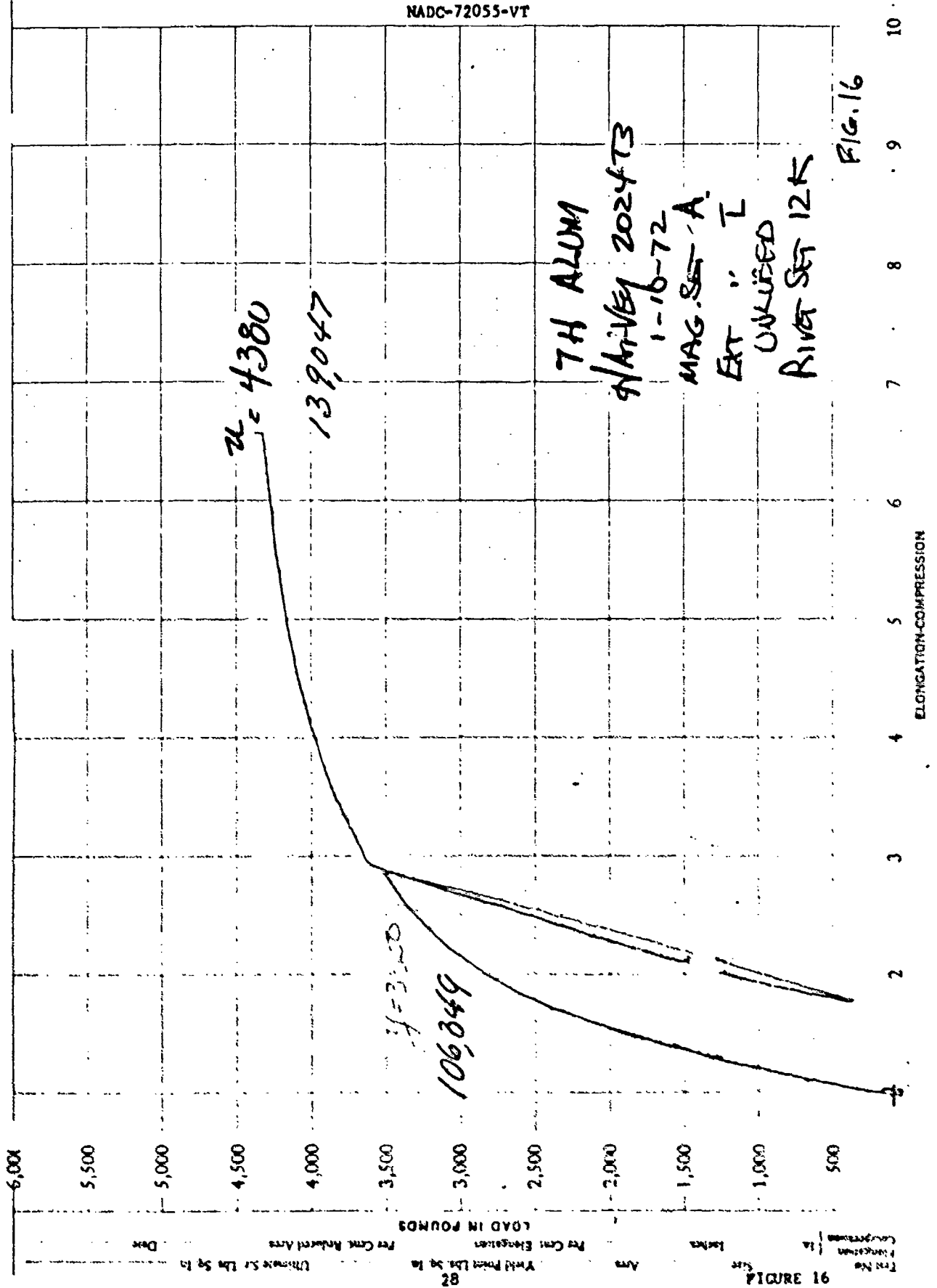
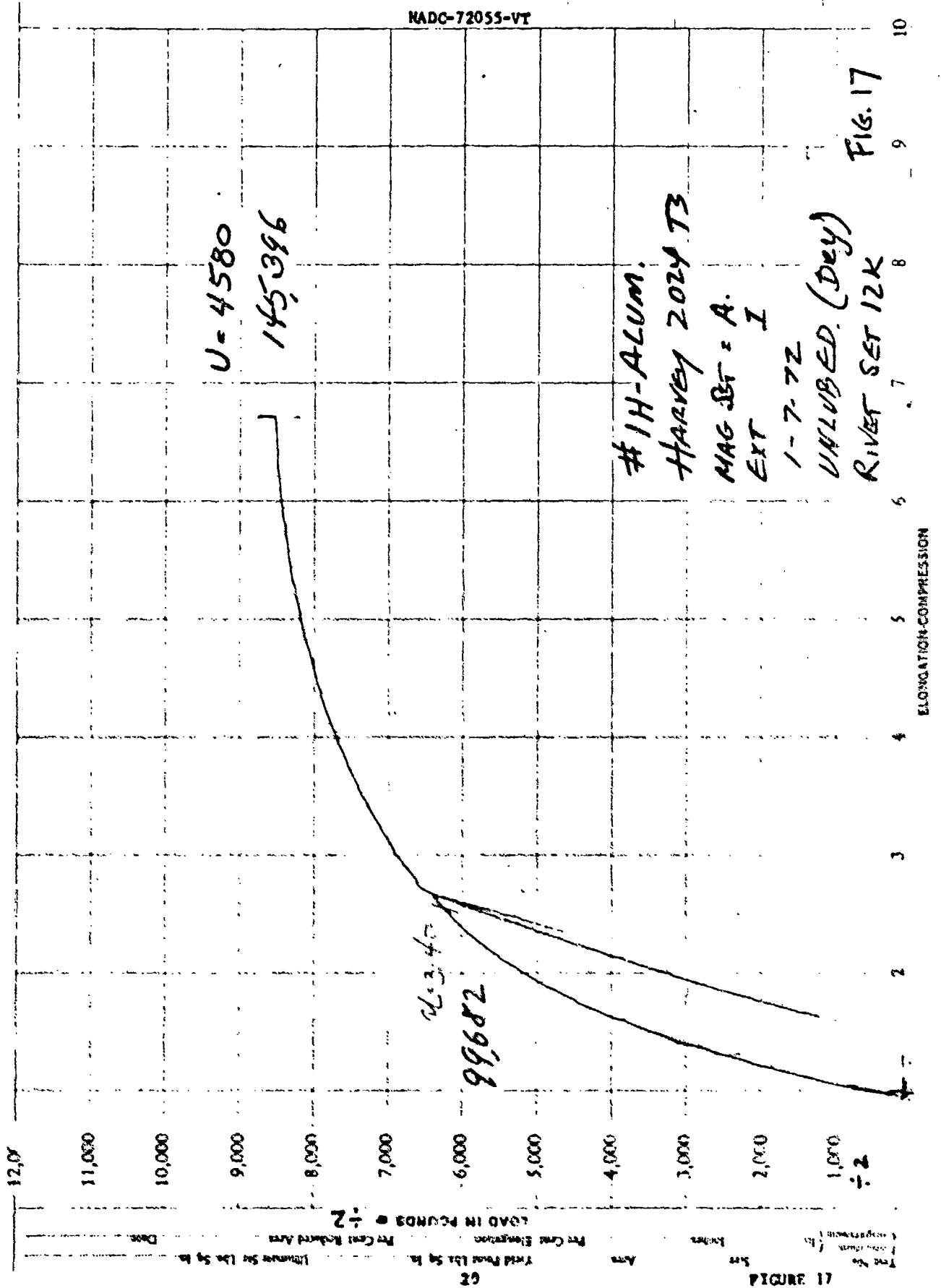


FIGURE 14







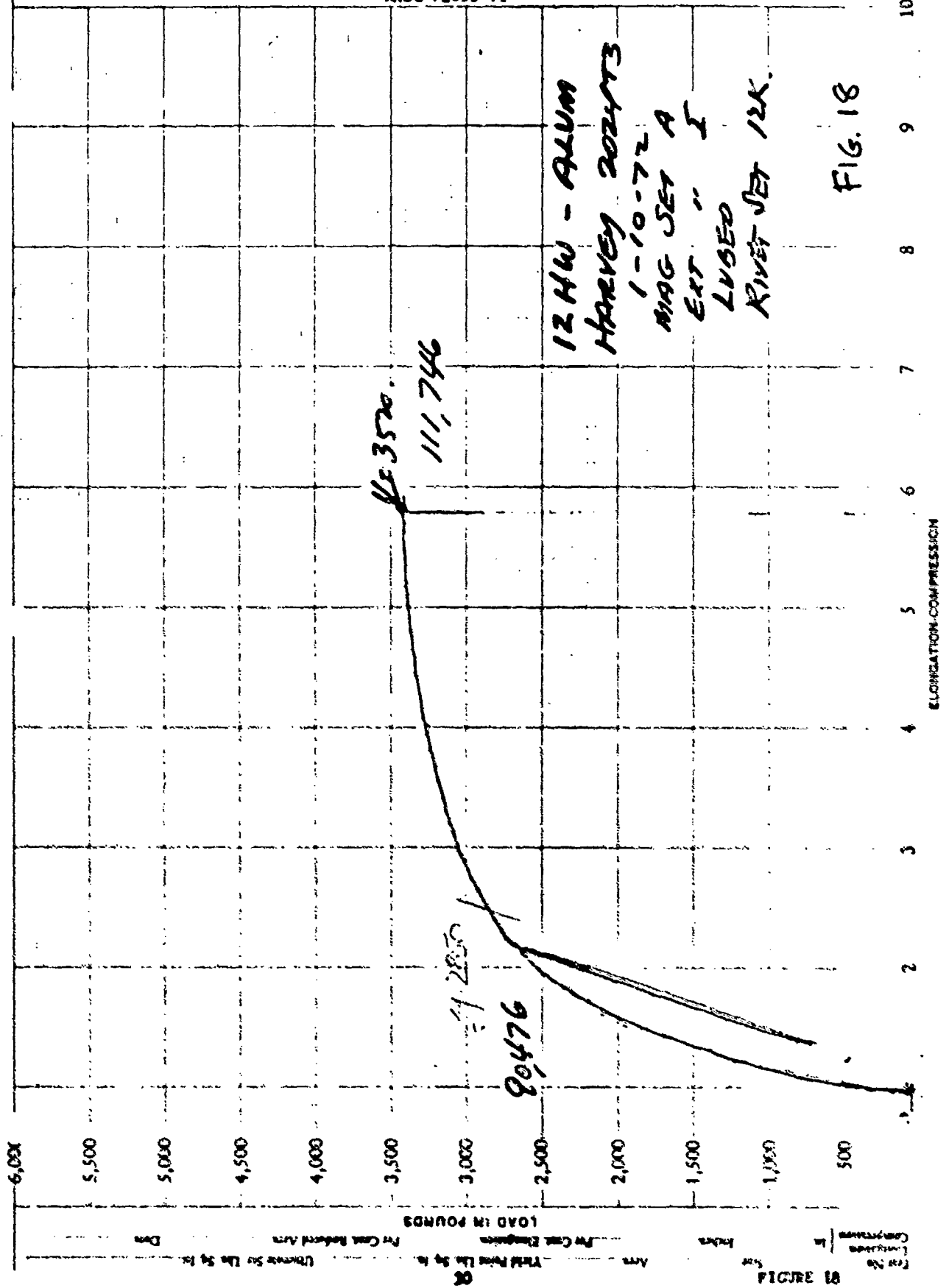


FIG. 18

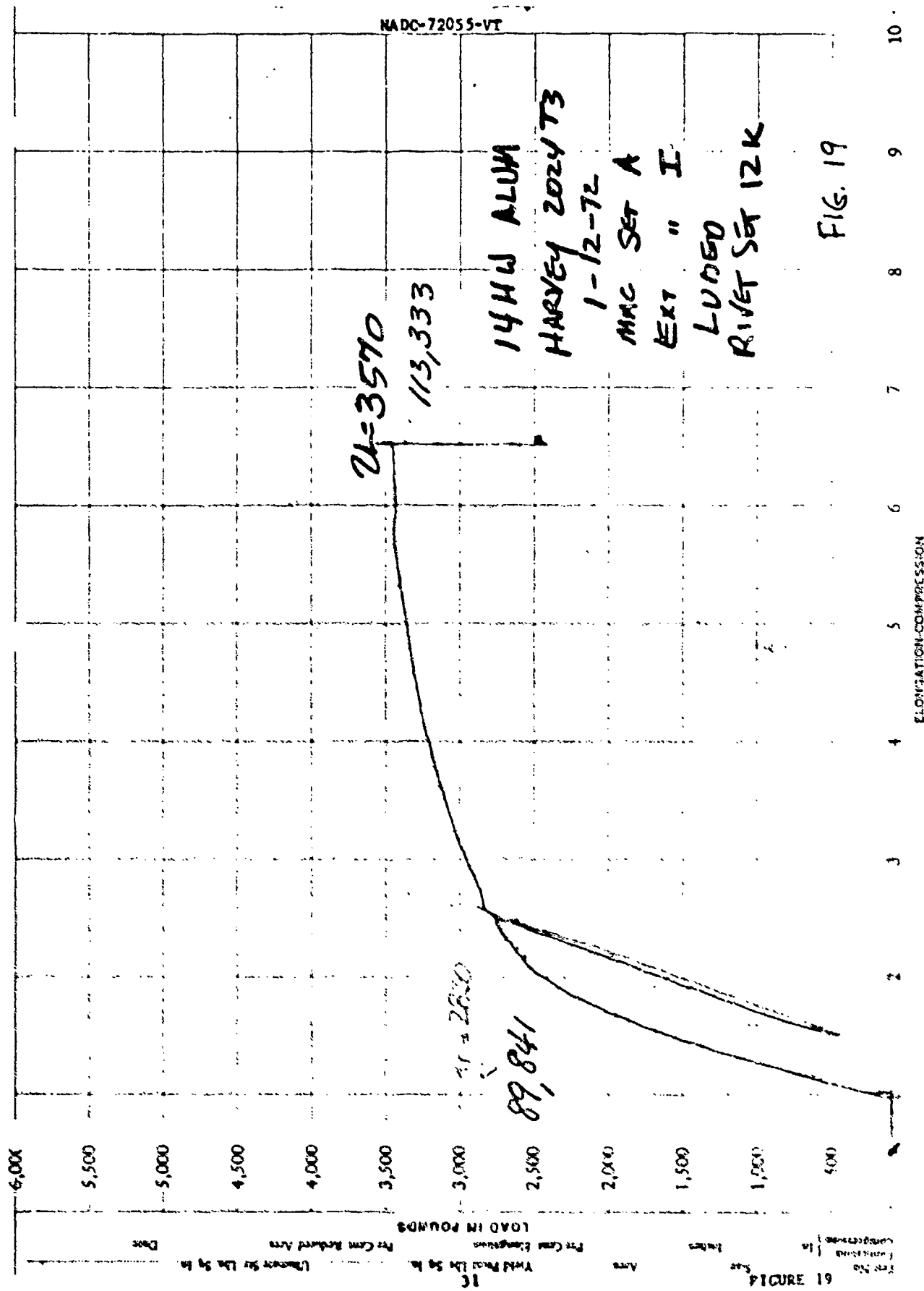


FIG. 19

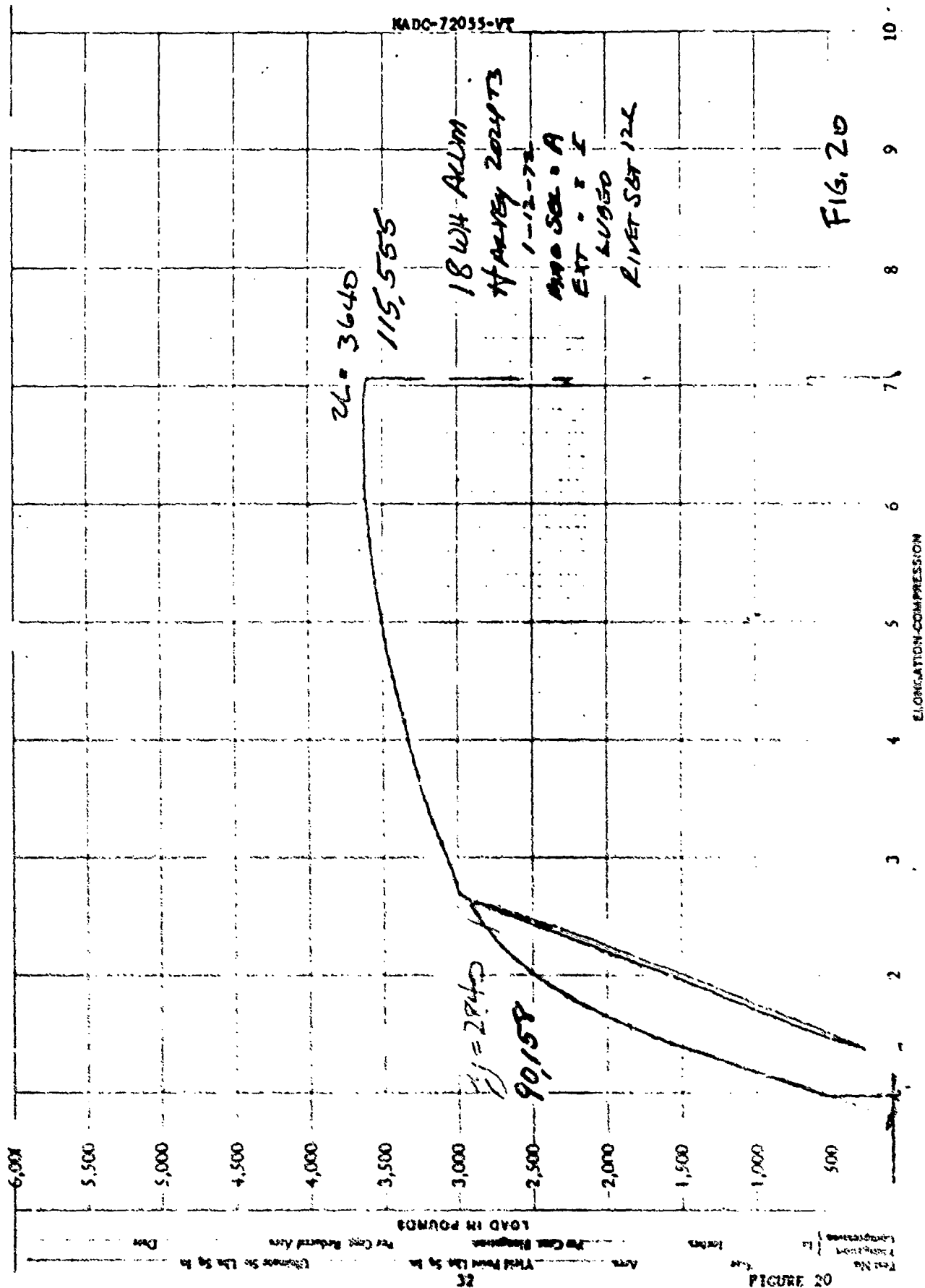


FIG. 20

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FIGURE 20

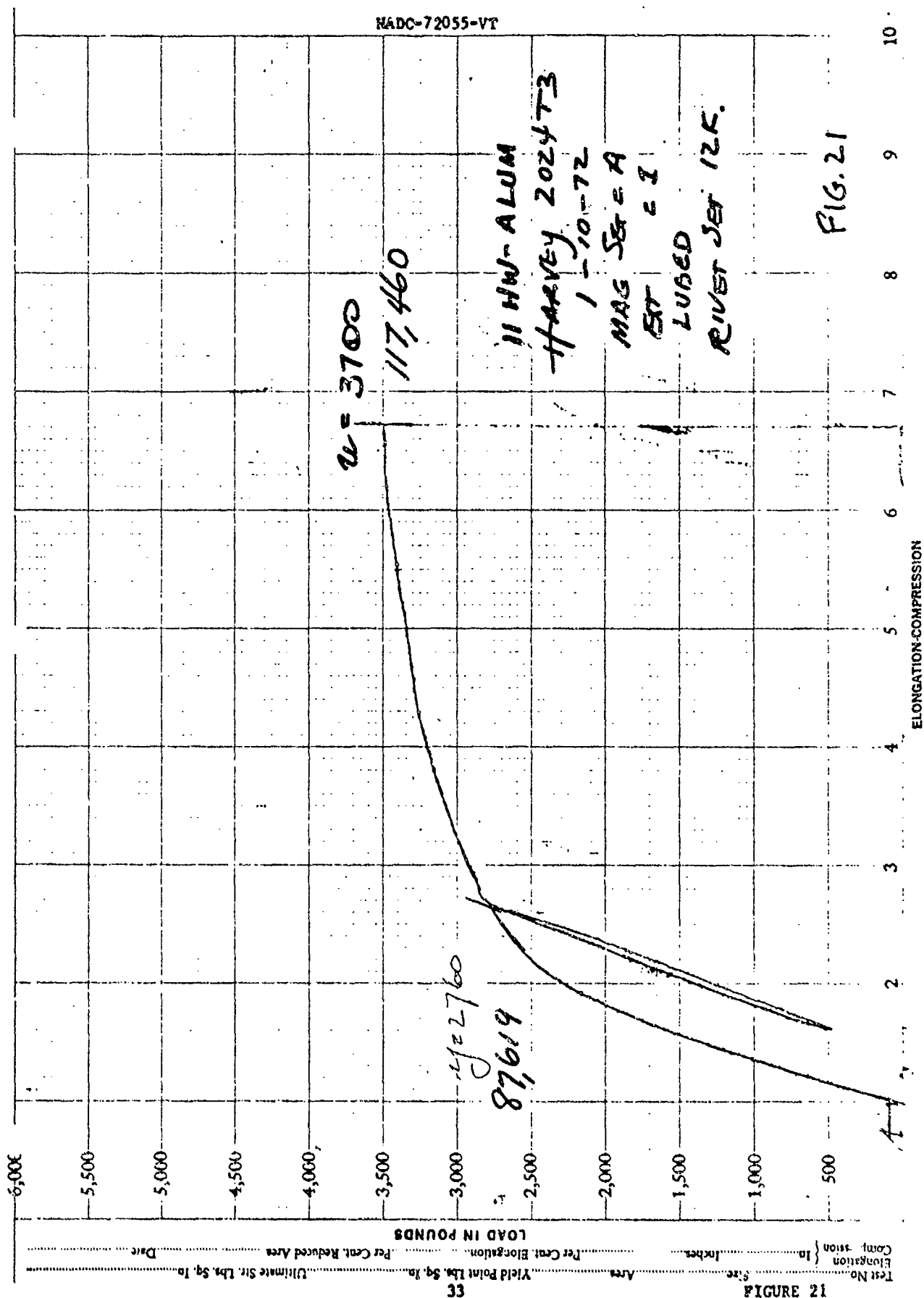
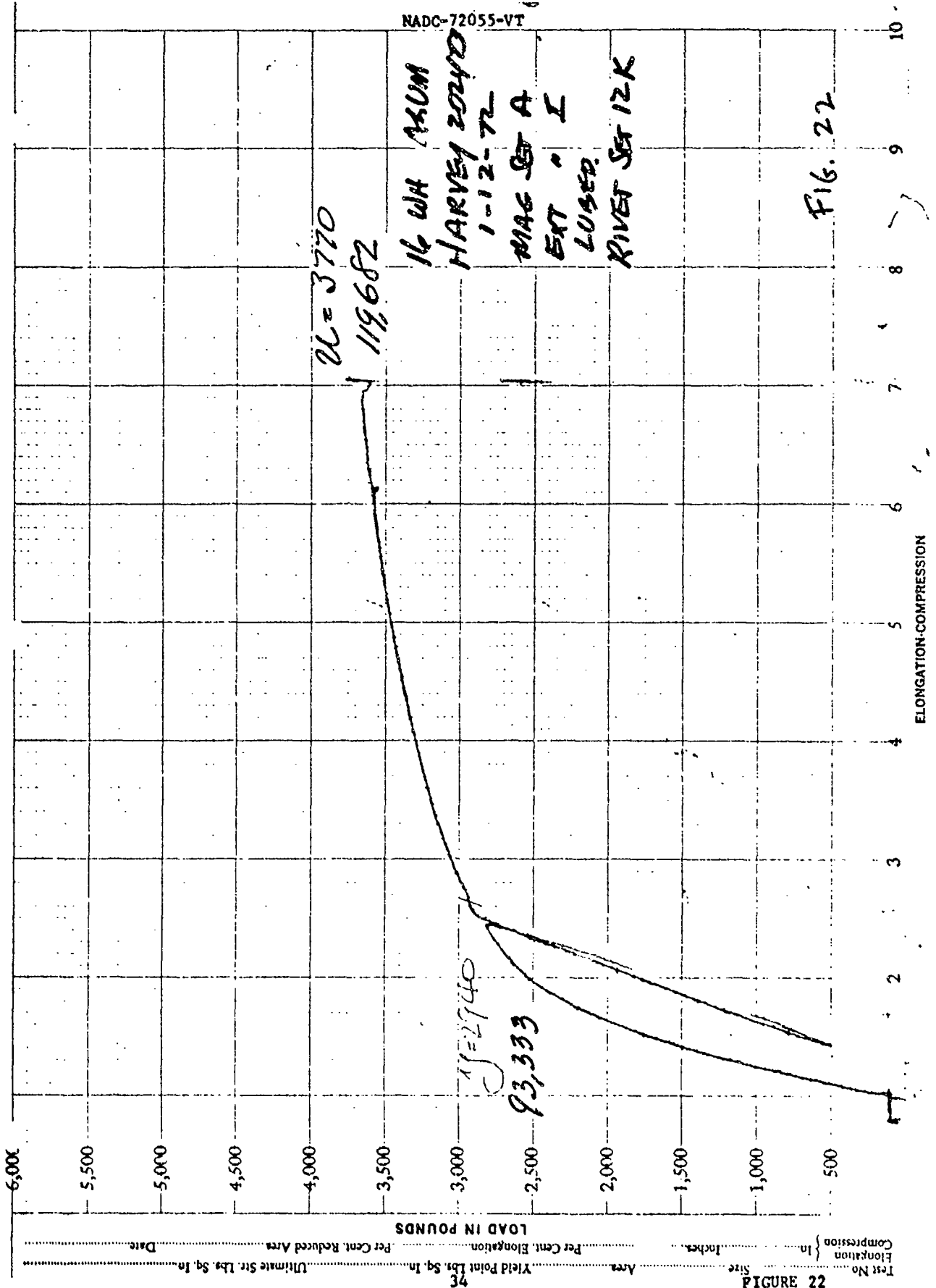
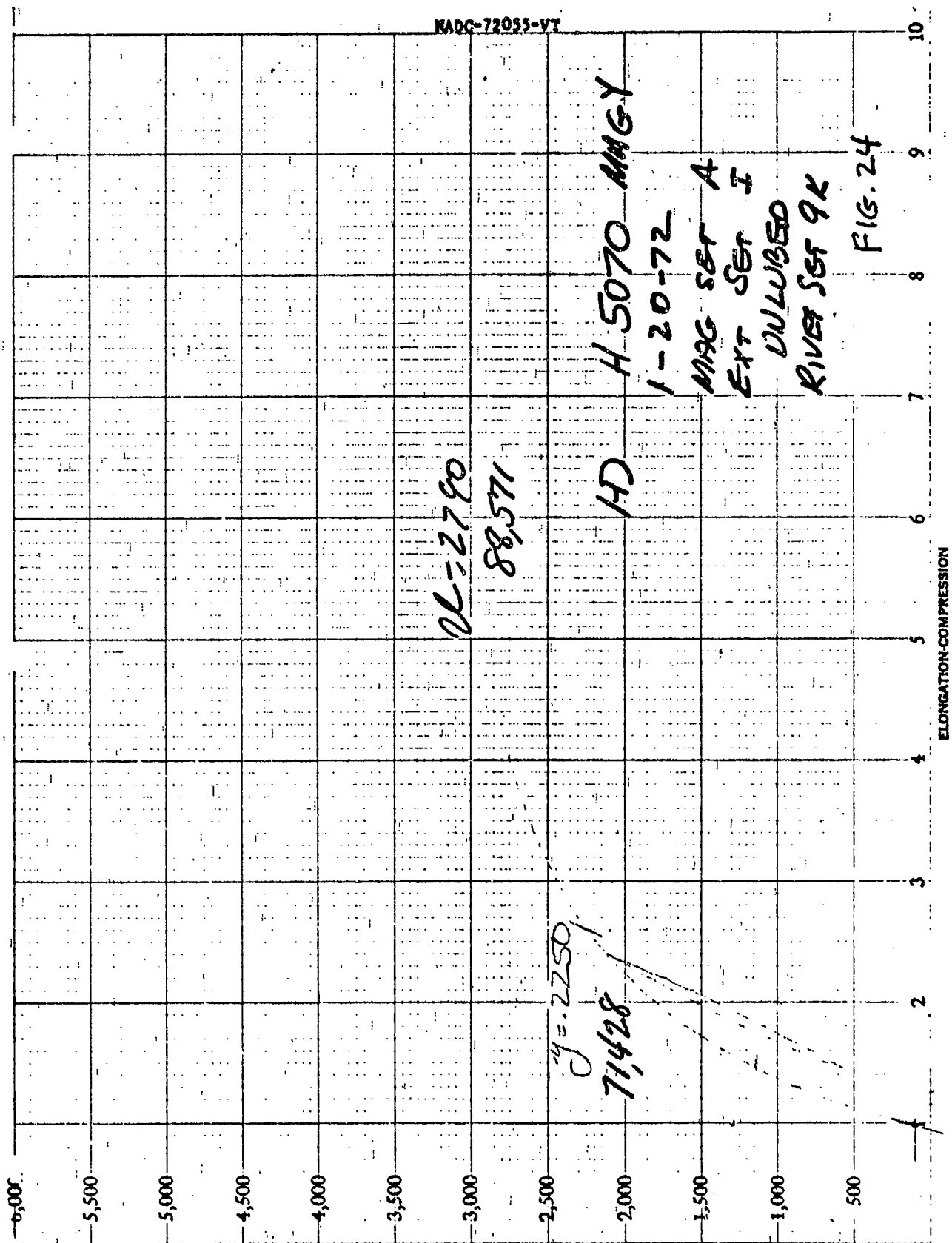


FIG. 21

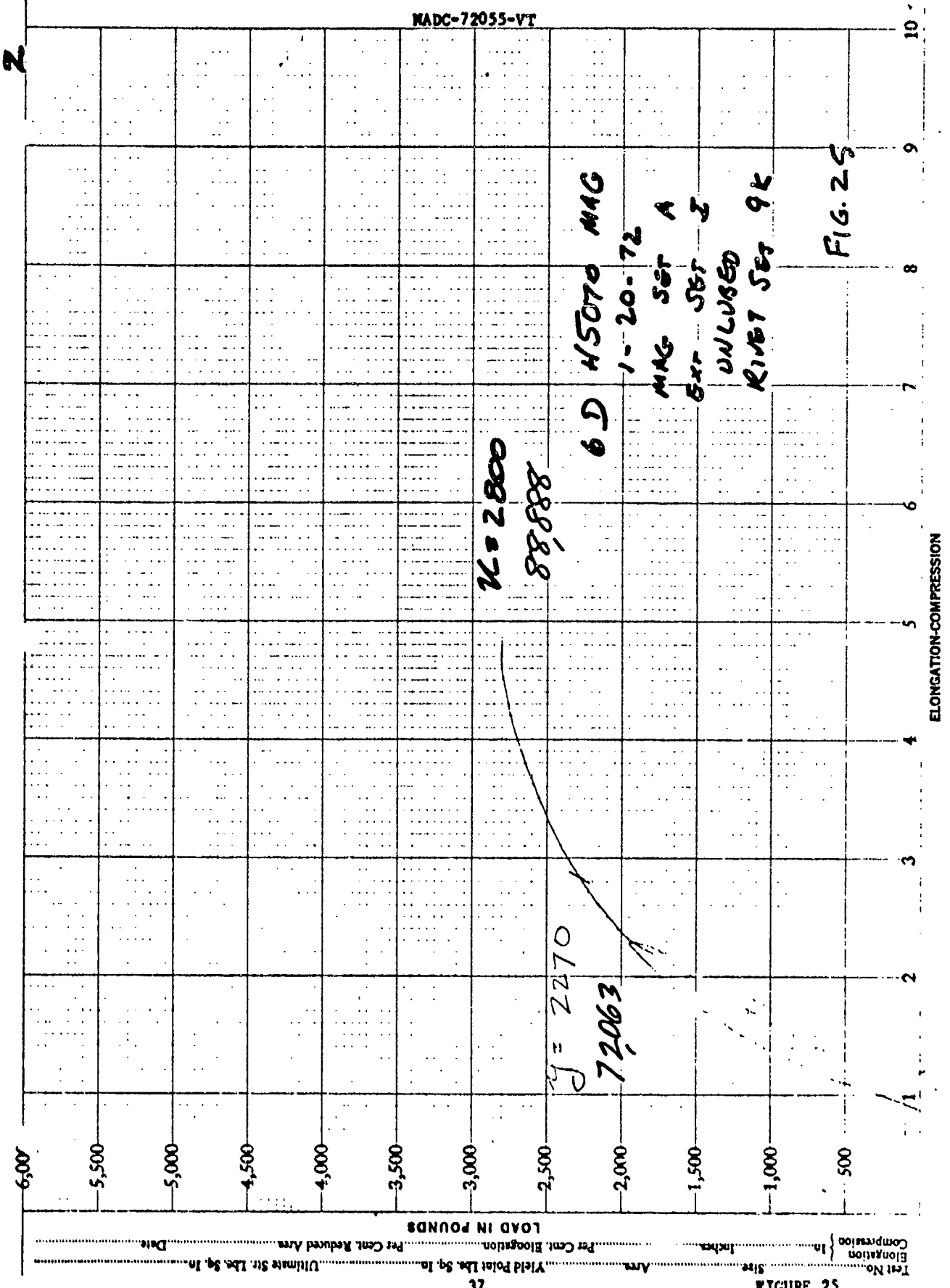


 α

2



Test No. 93
Elongation {
Compression {
Inches {
Per Cent. Elongation {
Yield Point Lbs. Sq. In. {
Ultimate Str. Lbs. Sq. In. {
Date {
Per Cent. Reduced Area {



Test No. _____

Size _____

Area _____

Yield Point Lbs. Sq. In. _____

Per Cent. Elongation _____

Per Cent. Reduced Area _____

Ultimate Str. Lbs. Sq. In. _____

Date _____

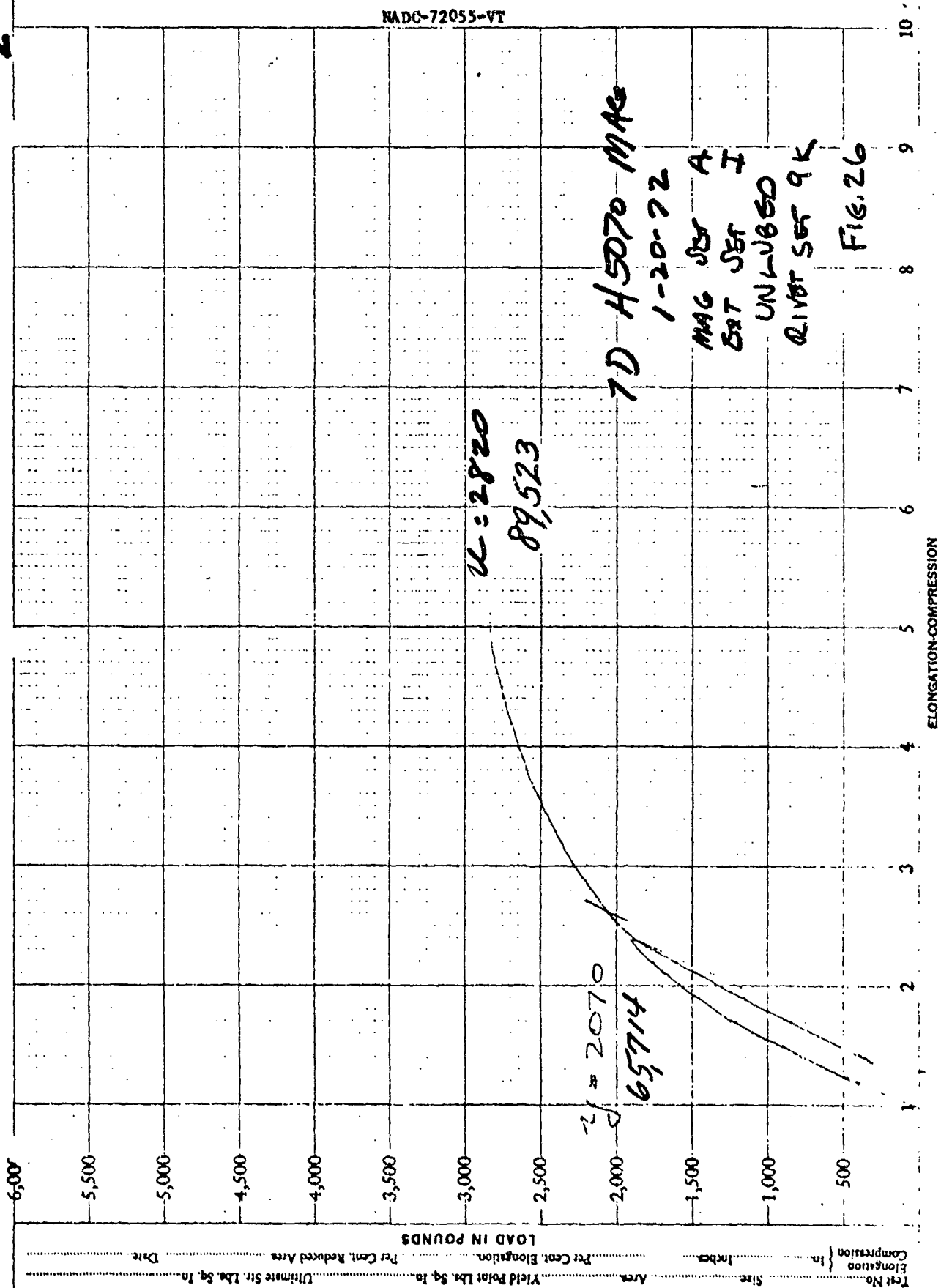
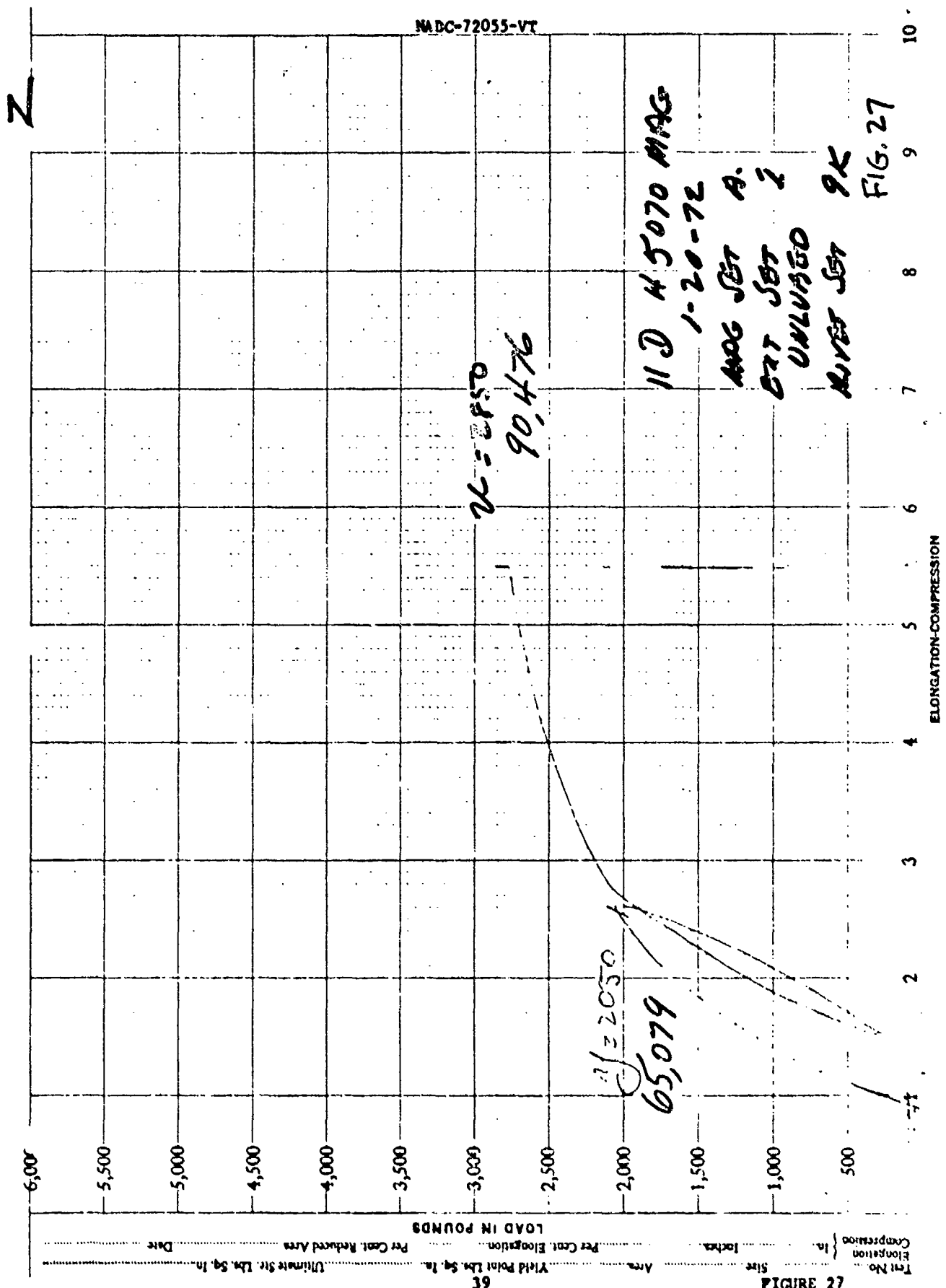
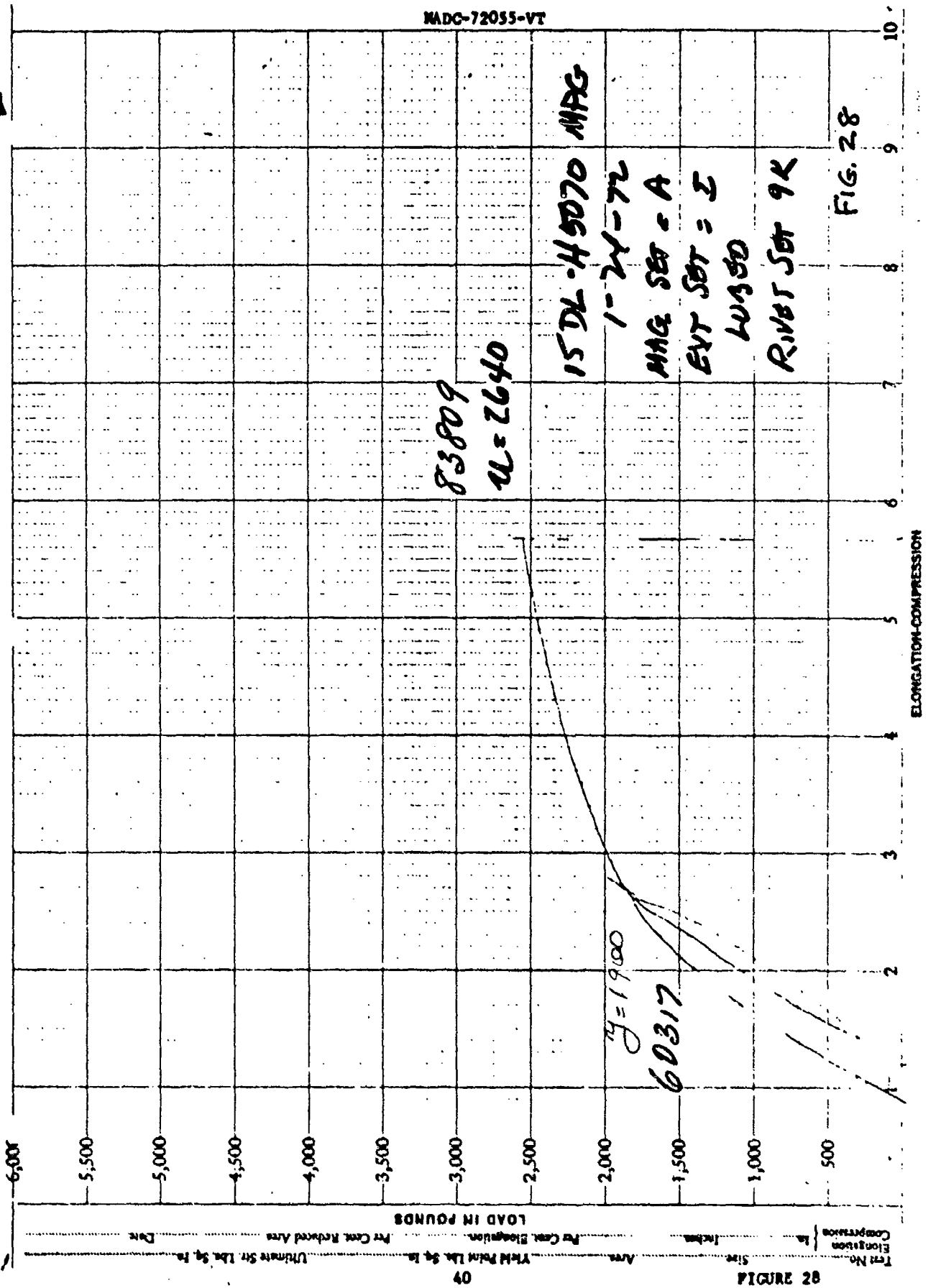


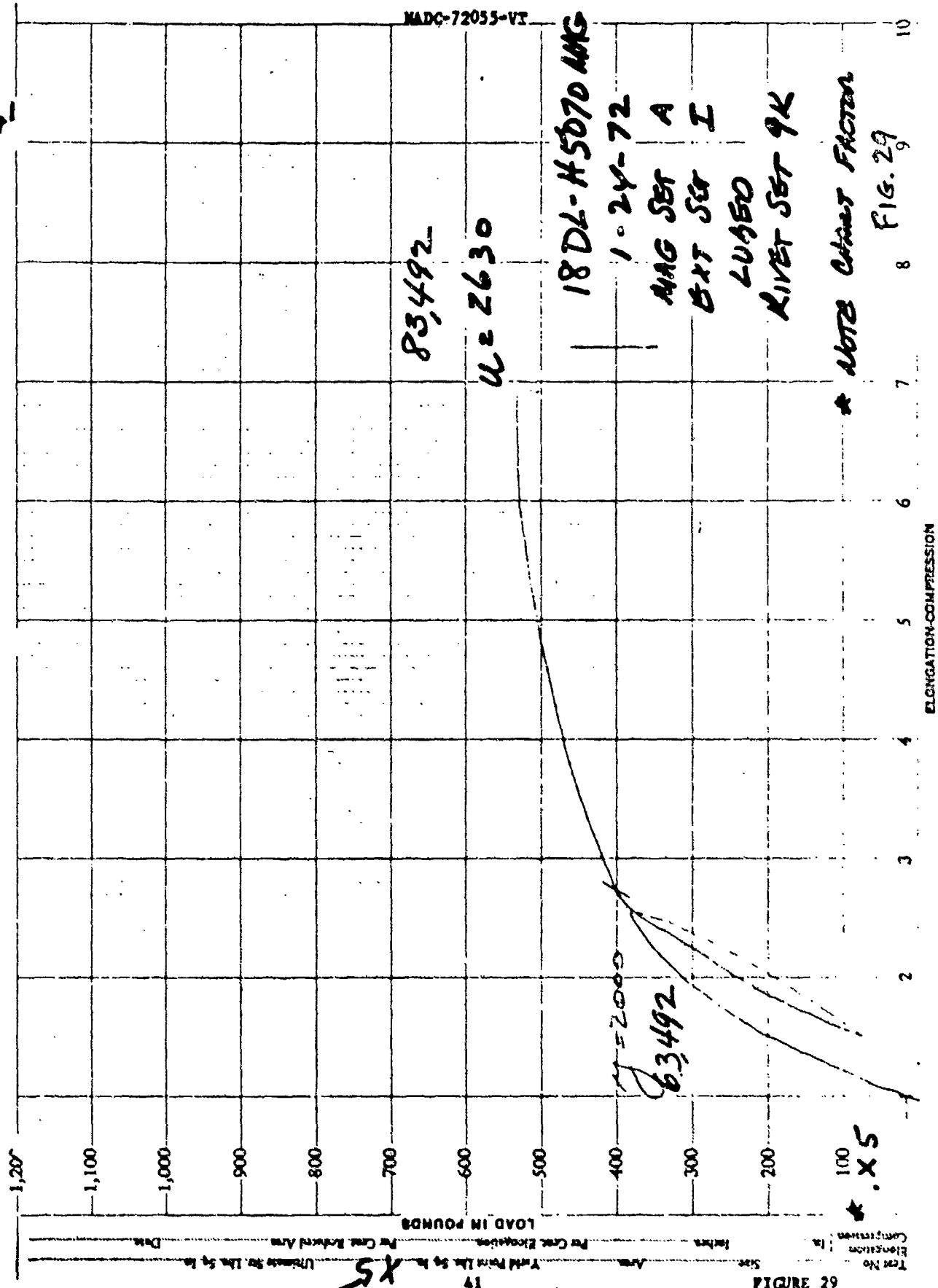
FIGURE 26

Test No. _____ Size _____ In. _____
 Elongation _____ In. _____
 Compression _____ In. _____
 Area _____ In. _____
 Yield Point Lbs. Sq. In. _____
 Per Cent. Elongation _____
 Per Cent. Reduced Area _____
 Ultimate Str. Lbs. Sq. In. _____
 Date _____



2





MADC-72055-VT

83,492

U = 2630

18 DL-H5070 MAG

1-24-72

MAG SET A

EXT SET I

LU450

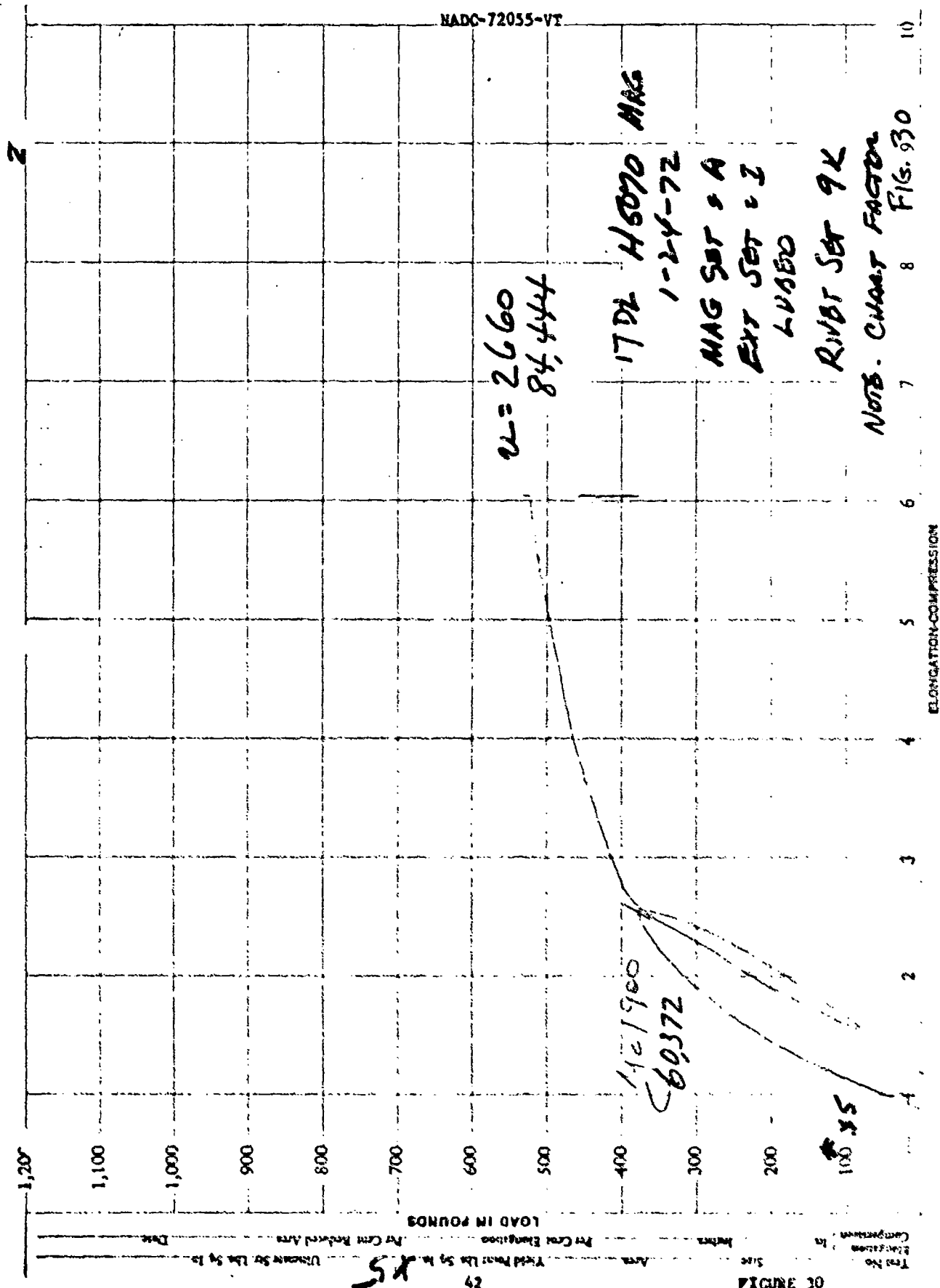
RIVET SET 9K

* NOTE CRACK FACTOR

FIG. 29

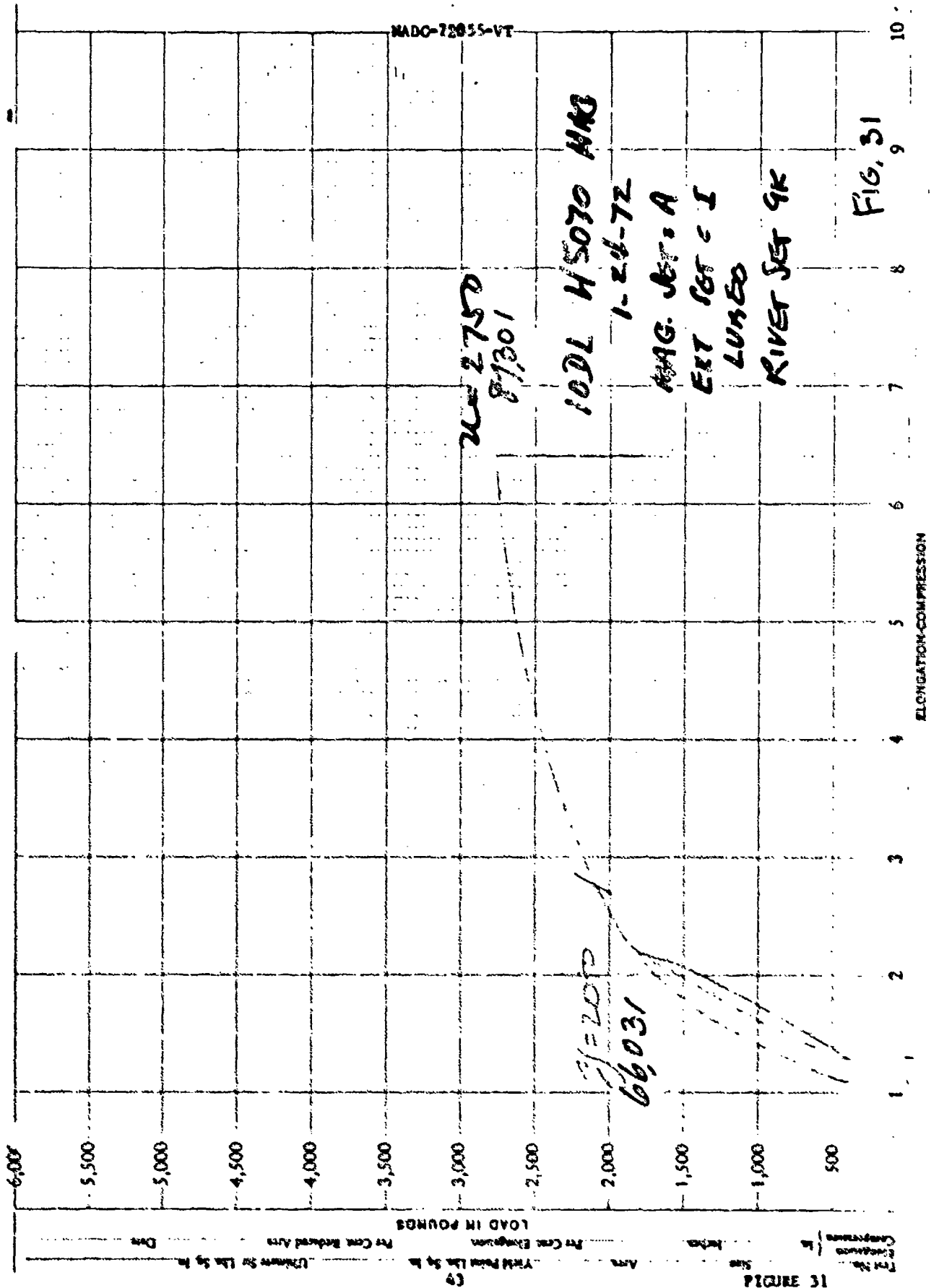
FIGURE 29

19 X5



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FIGURE 30



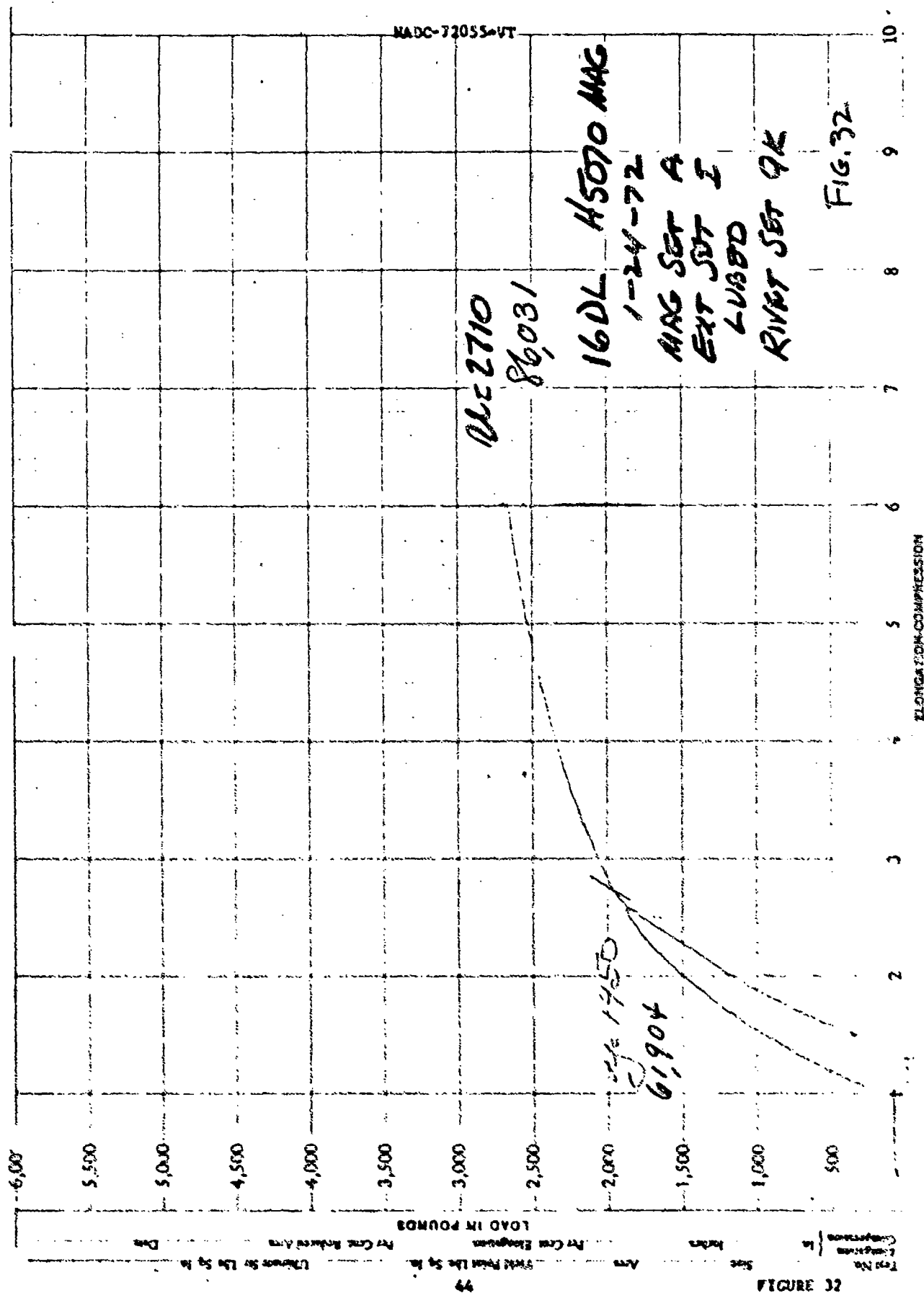
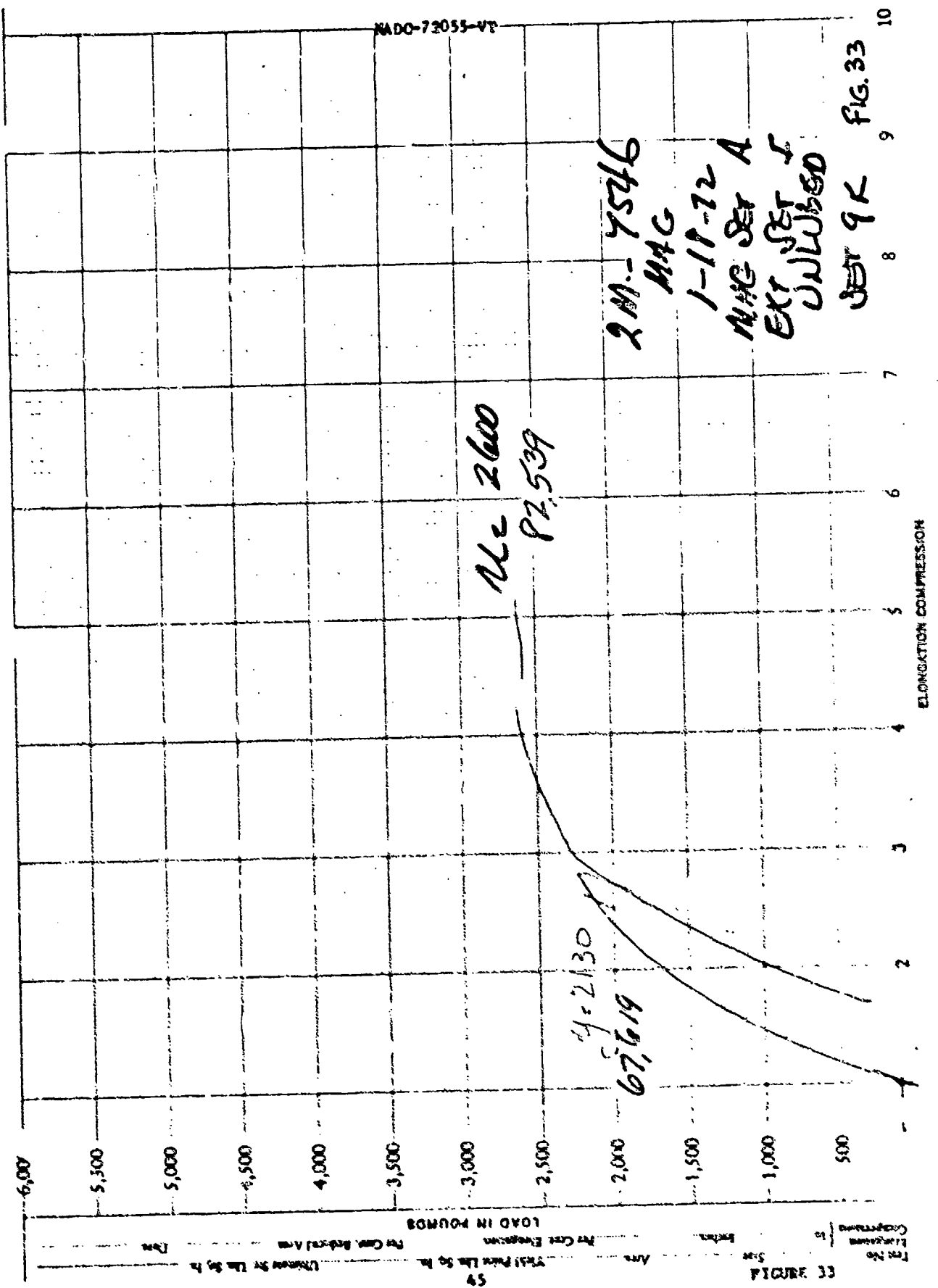


FIGURE 32



NADO-72055-VT

2M-7546
HAC
1-11-72
NHC SET A
EXT SET I
UNLUBED

VER 9K FIG. 33

10

9

8

7

6

5

4

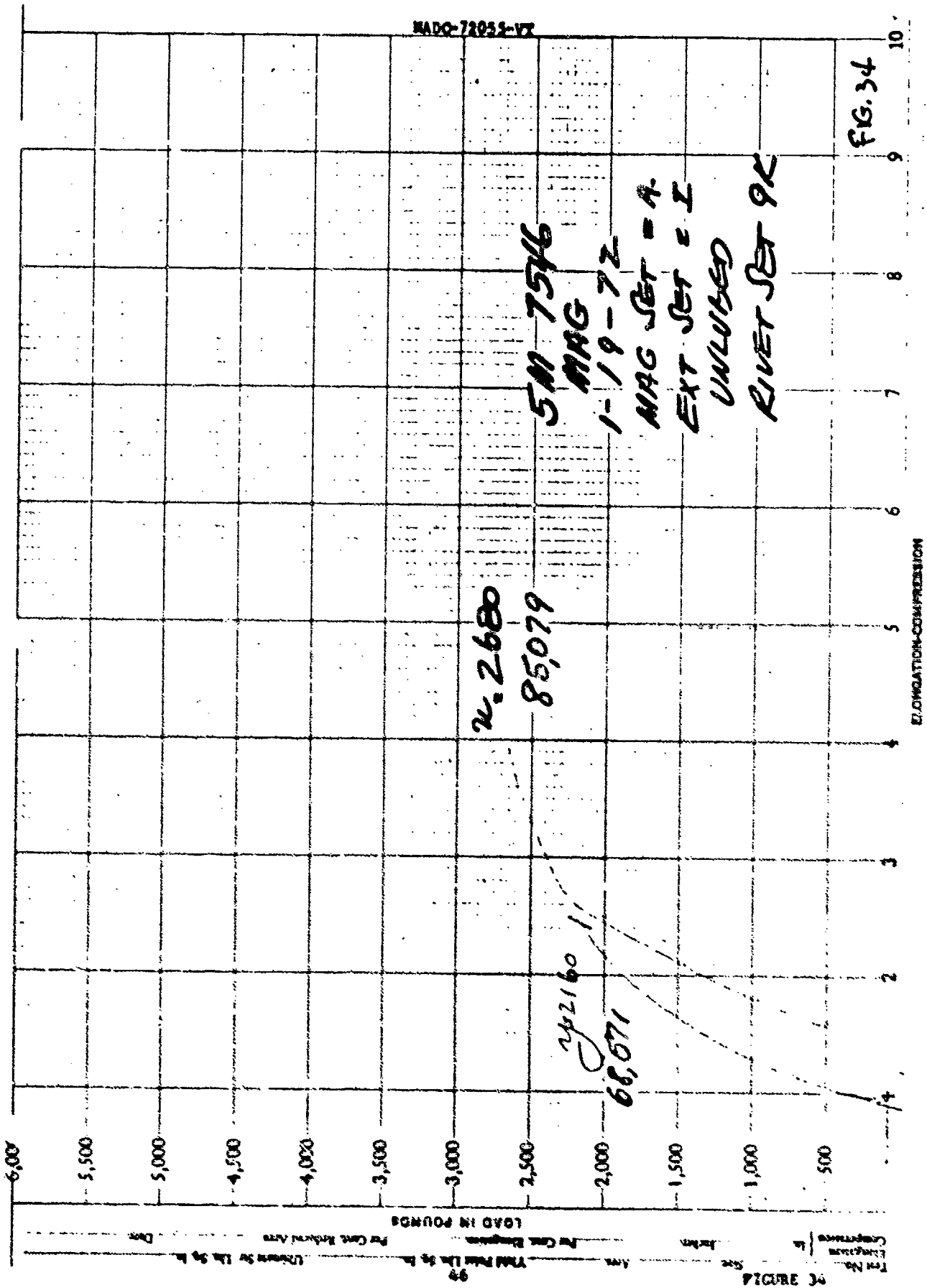
3

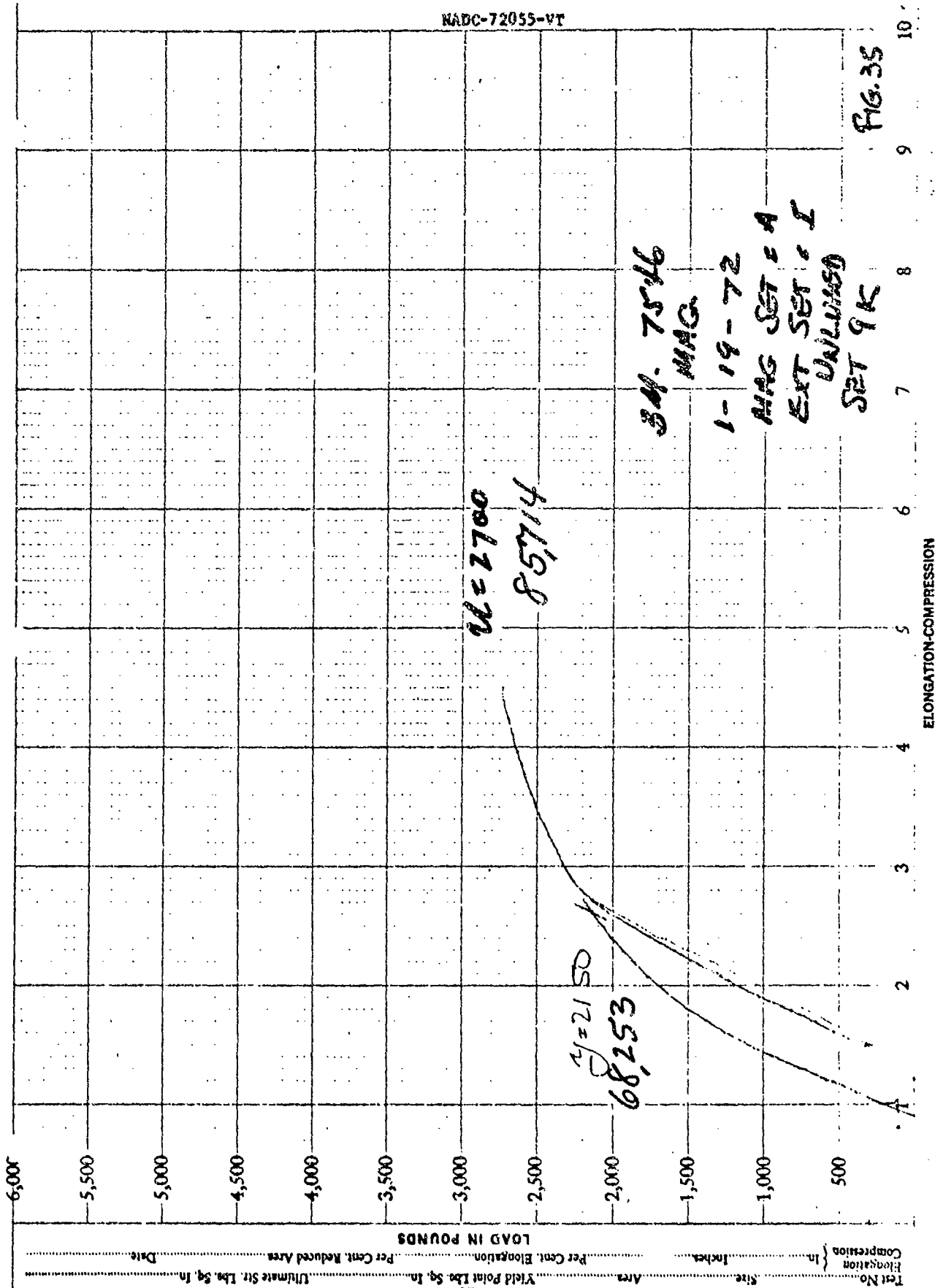
2

ELONGATION COMPRESSION

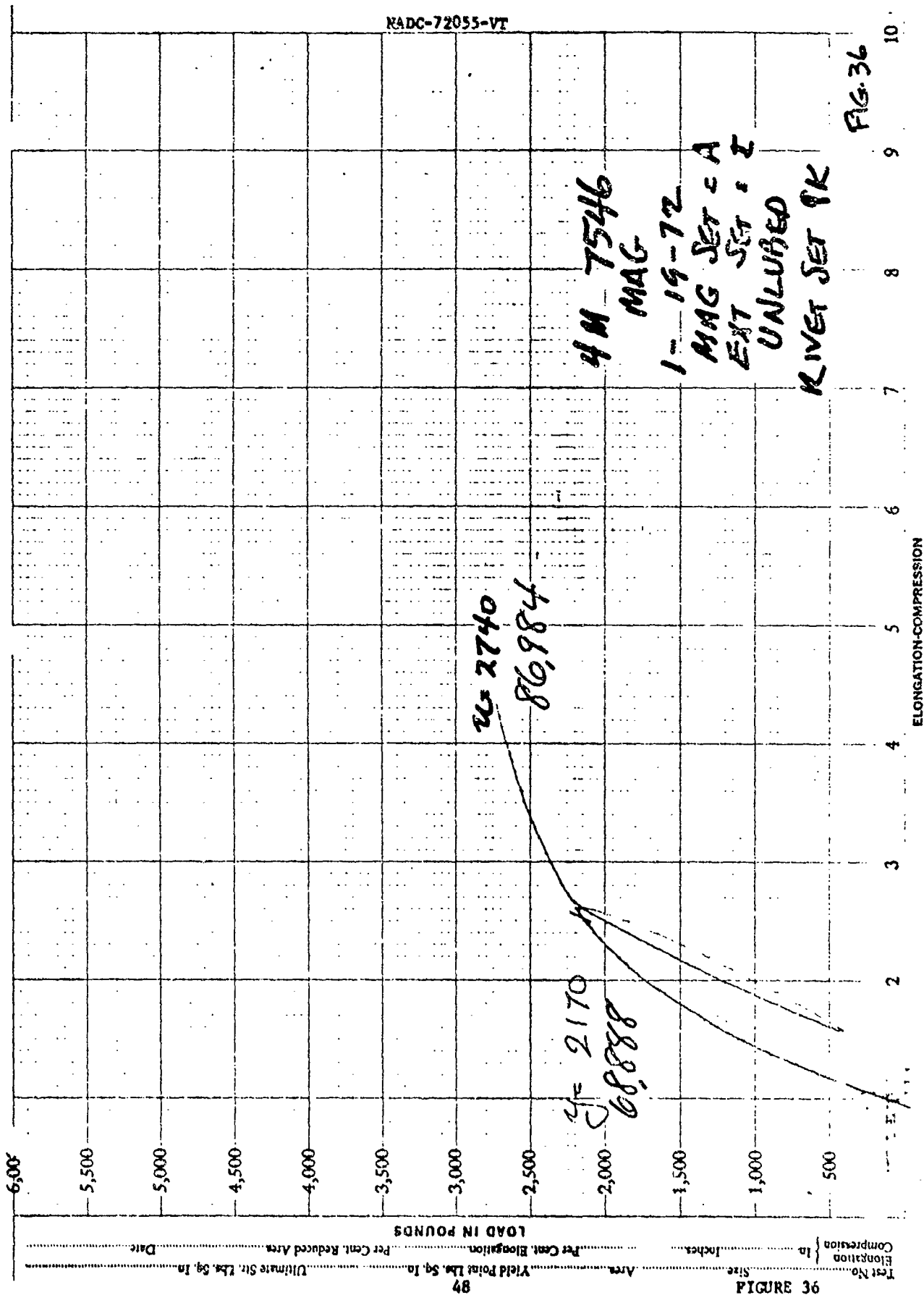
FIGURE 33

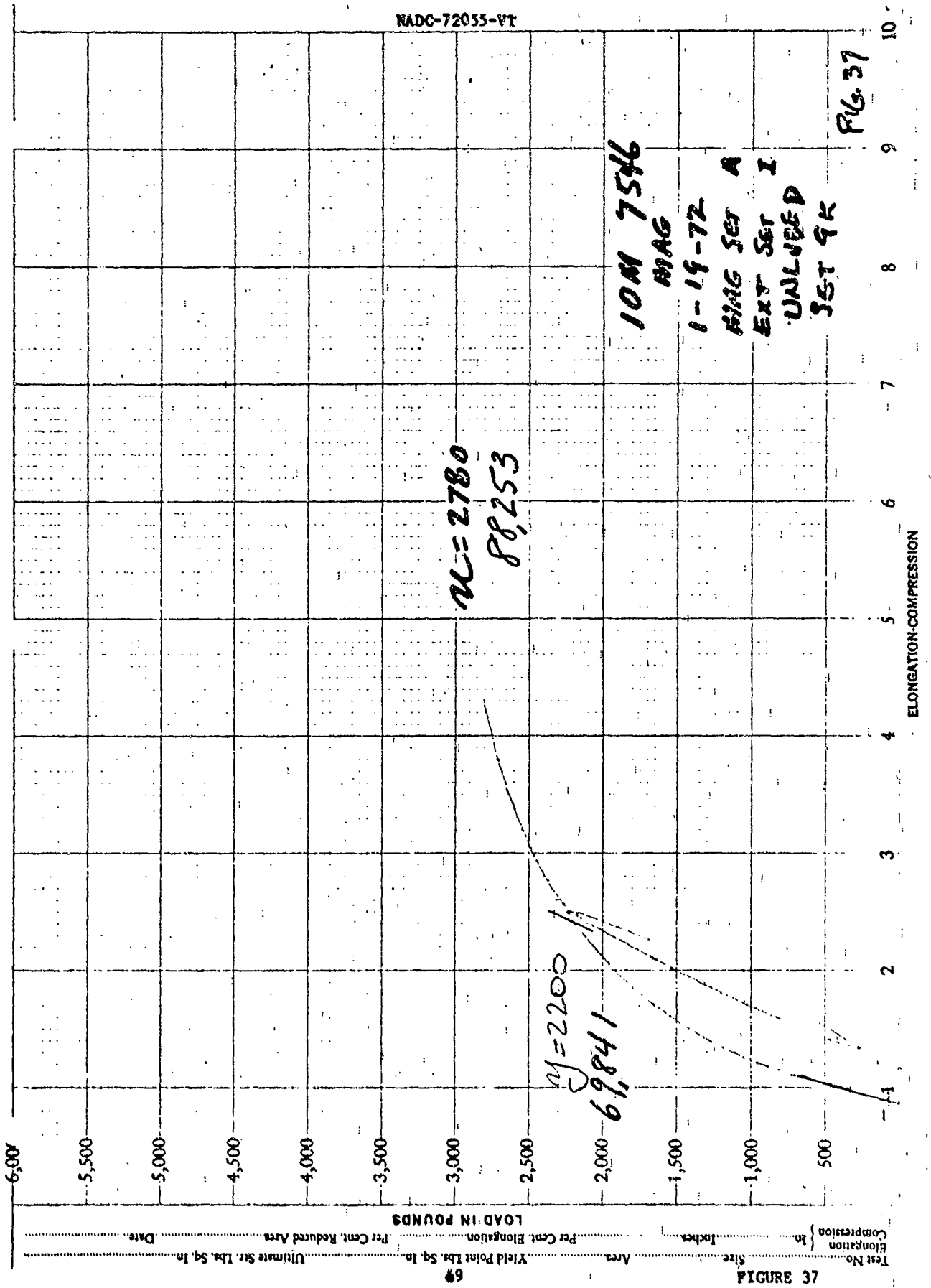
54

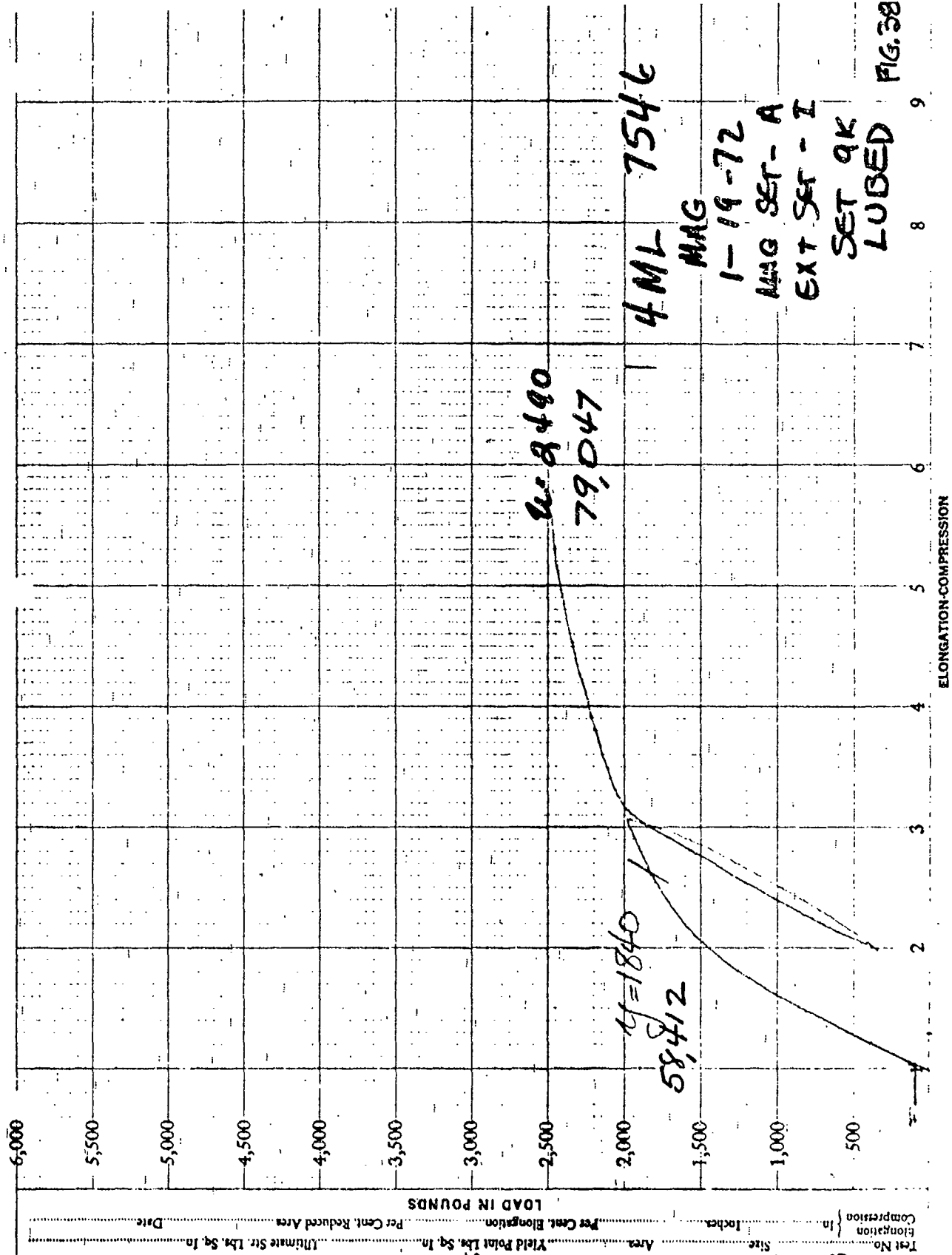


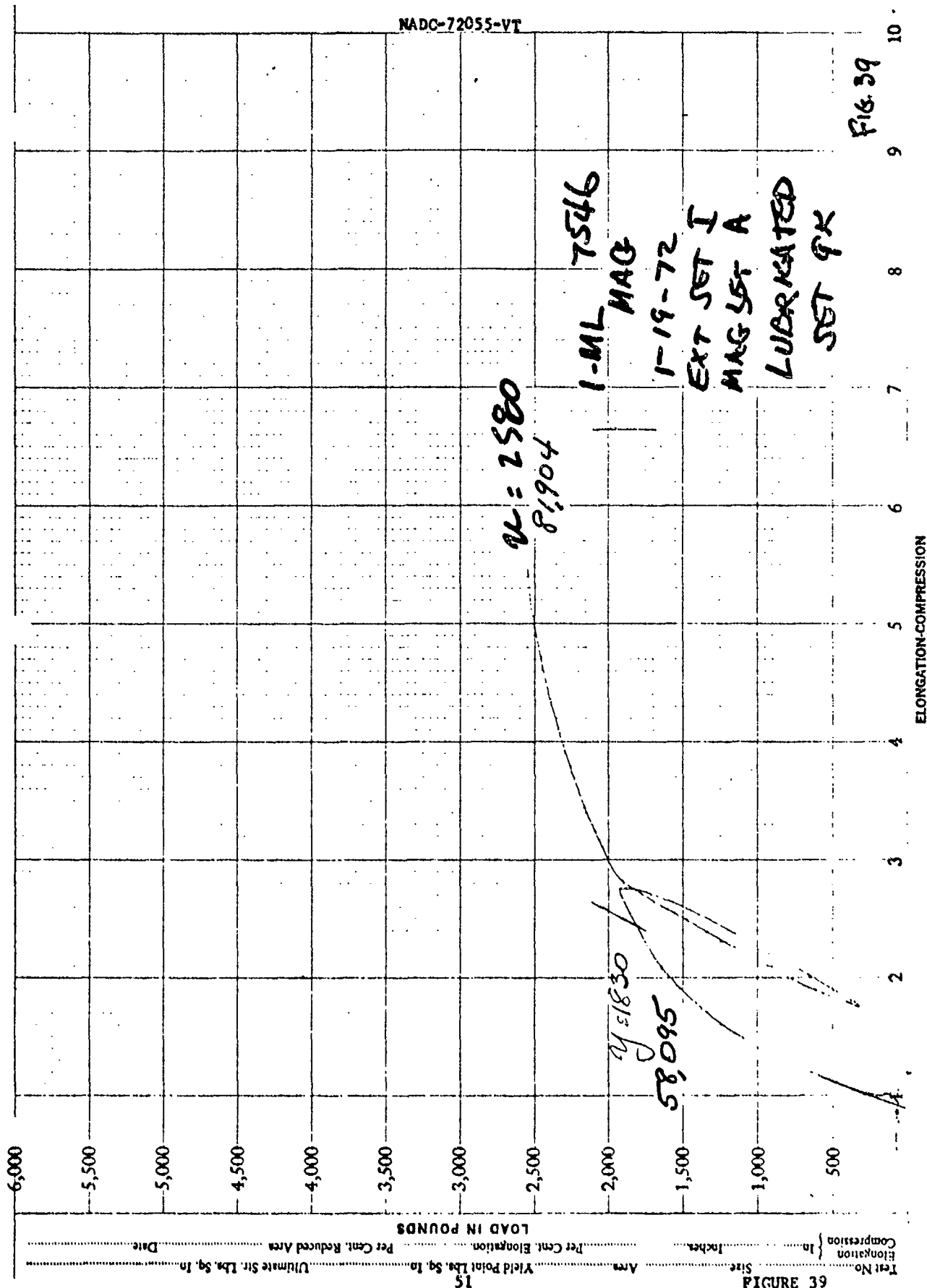


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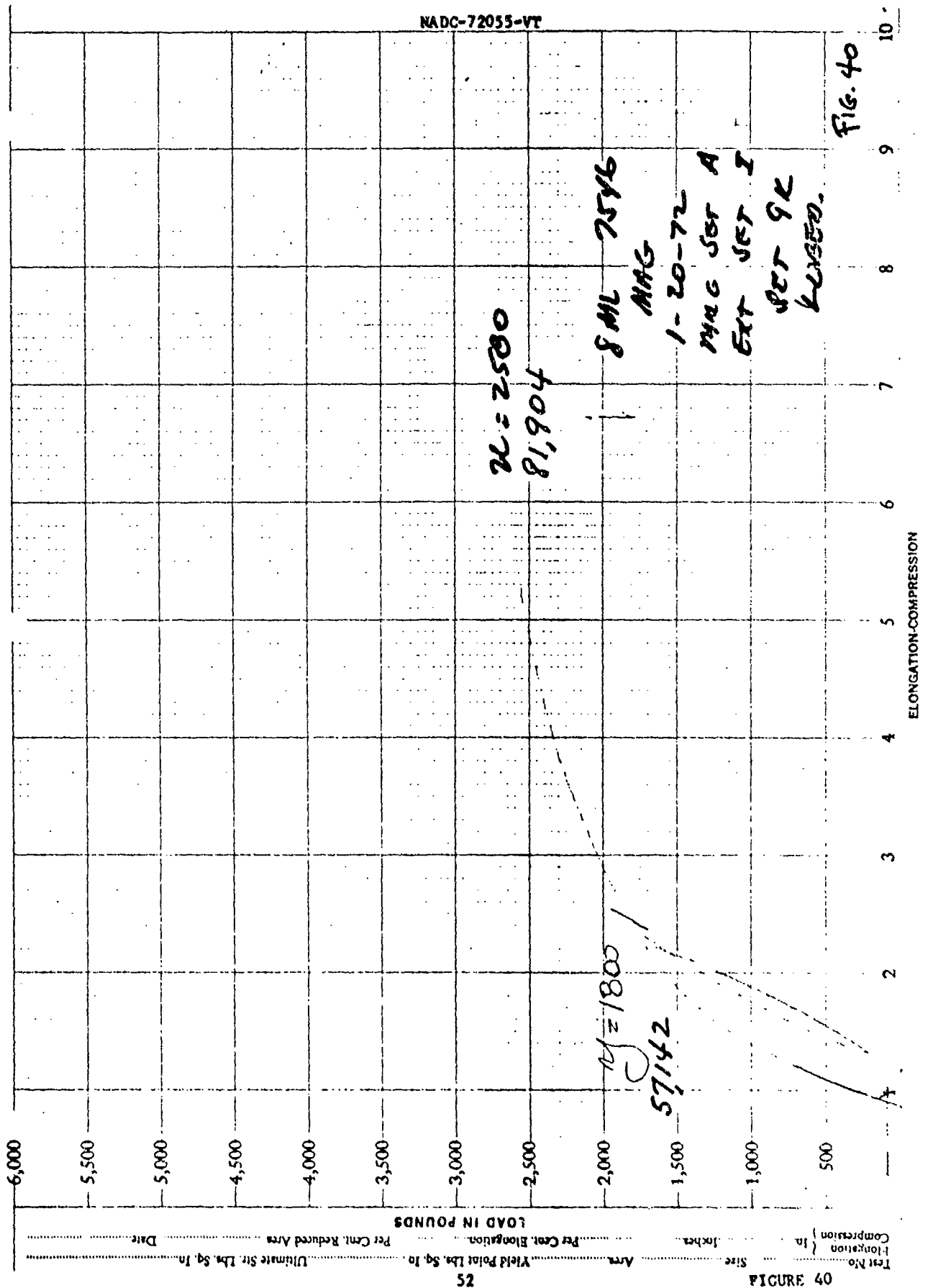


FIG. 40

FIGURE 40

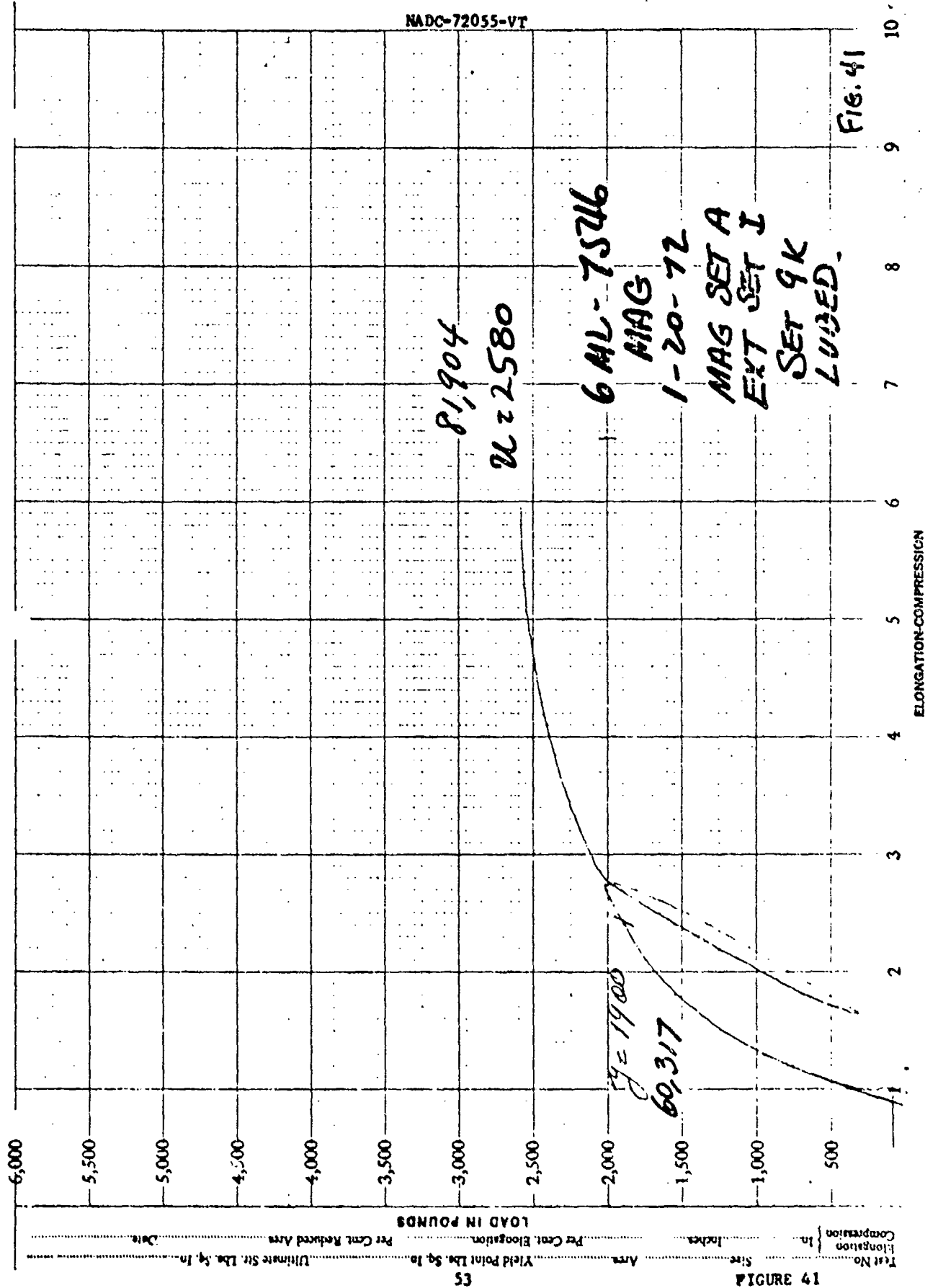


FIGURE 41

CS

Test No. _____
 Elongation _____ in. _____
 Compression _____ in. _____
 Area _____ sq. in. _____
 Yield Point Lbs. Sq. In. _____
 Ultimate Str. Lbs. Sq. In. _____
 Per Cent. Reduced Area _____
 Per Cent. Elongation _____
 Date _____

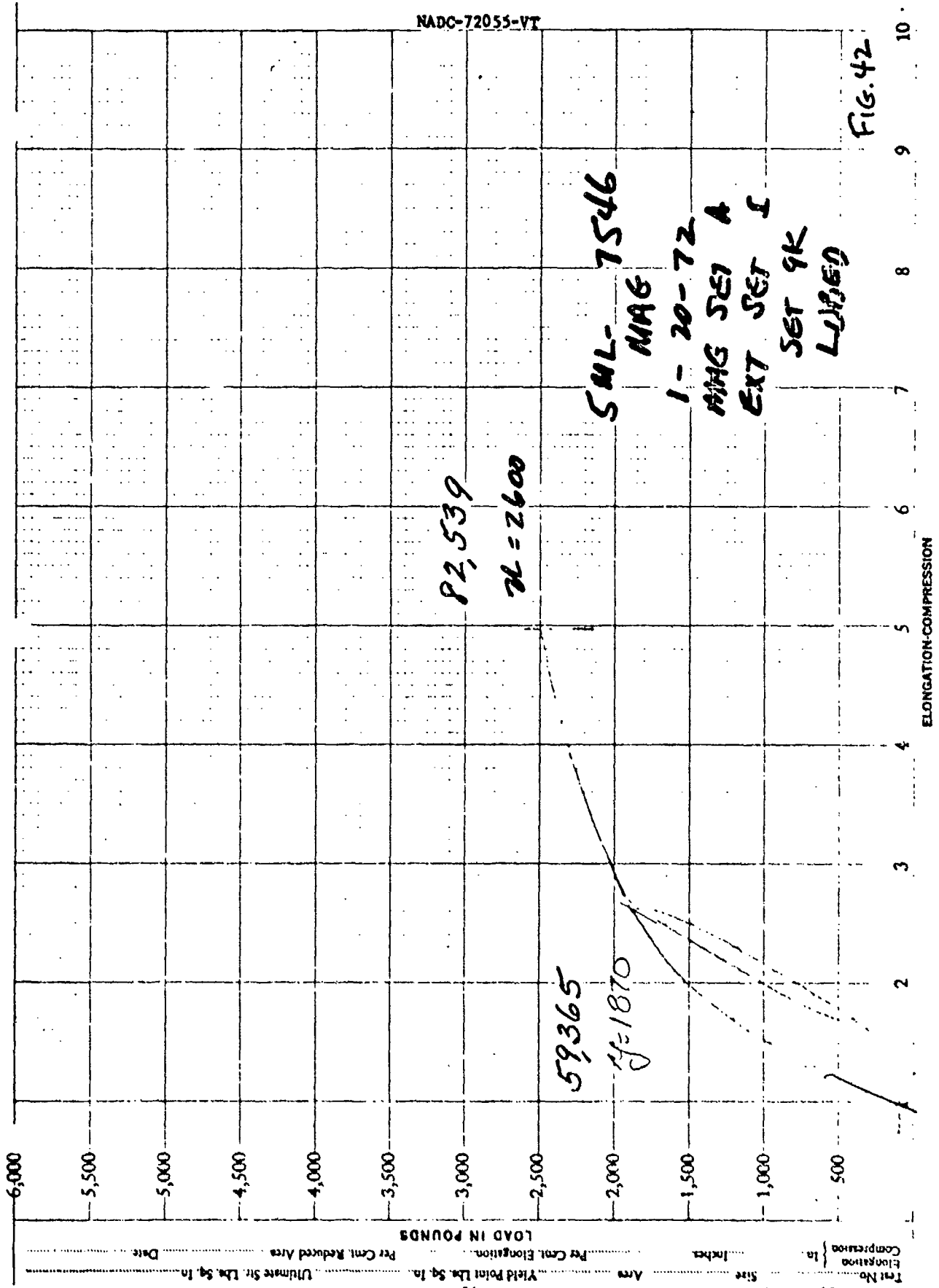
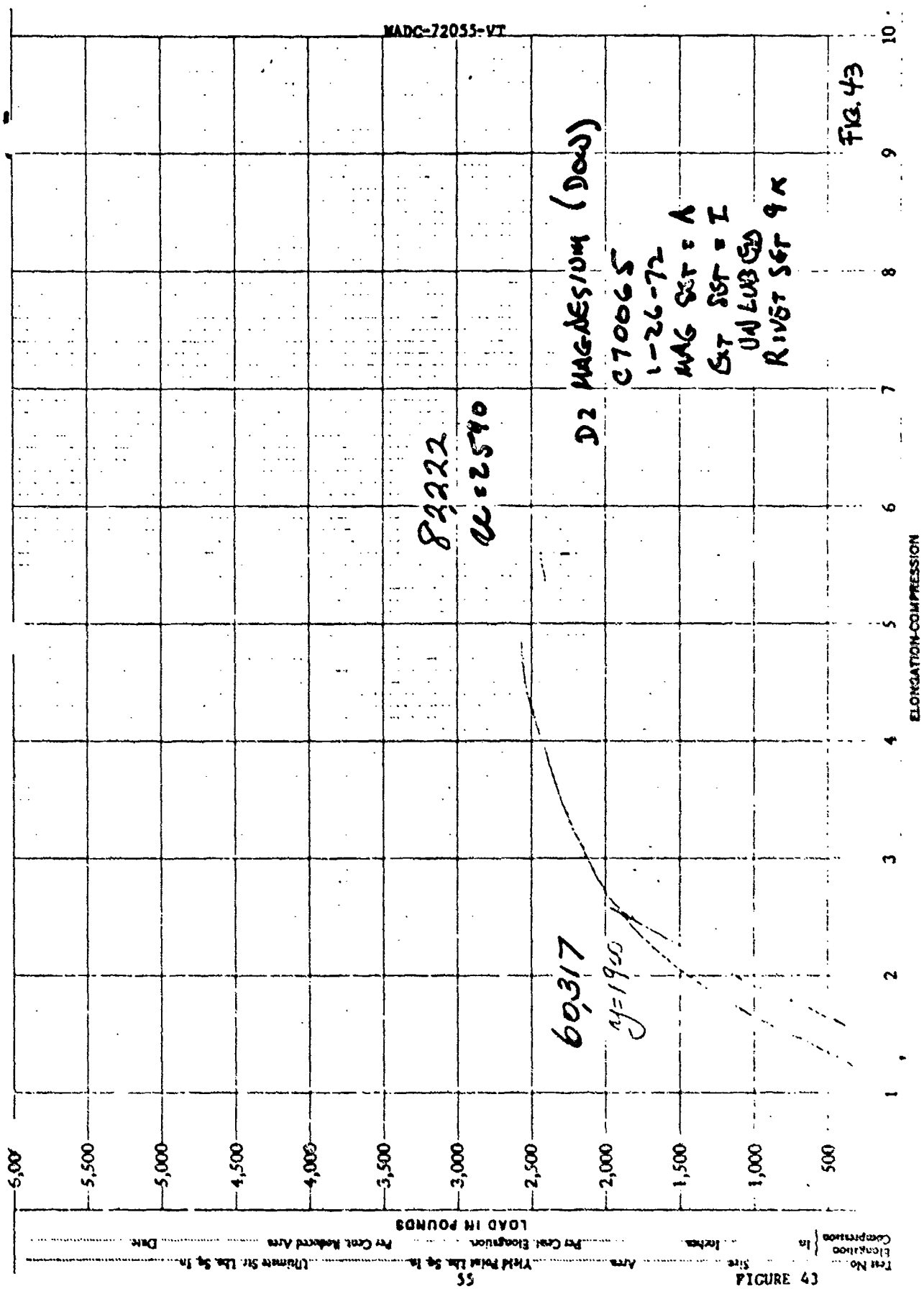


FIGURE 42

95

Test No. _____
 Elongation _____ in _____
 Compression _____ in _____
 Size _____ inches _____
 Area _____
 Yield Point Lbs. Sq. In. _____
 Per Cent Elongation _____
 Per Cent Reduced Area _____
 Ultimate Str. Lbs. Sq. In. _____
 Date _____



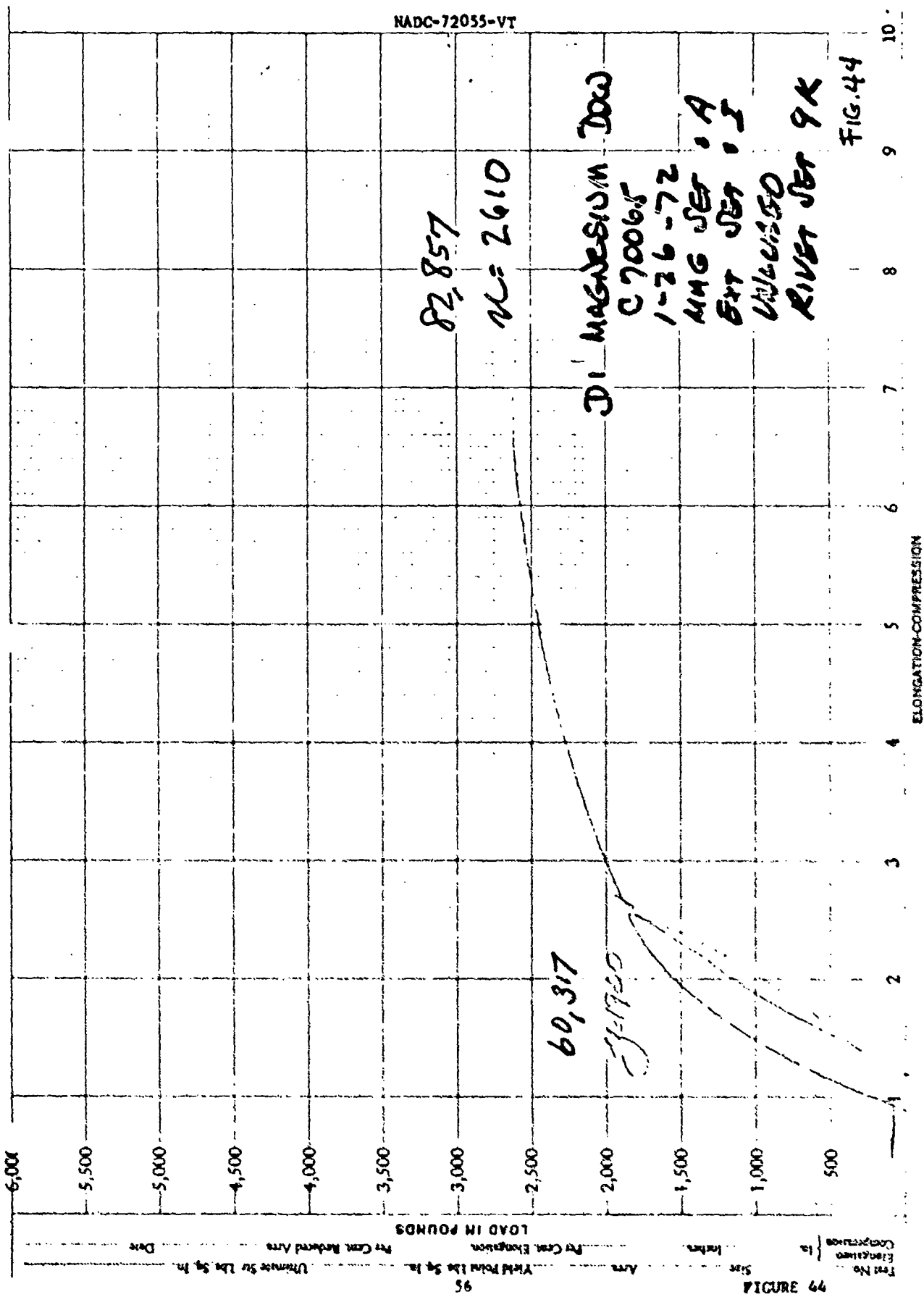


FIG. 44

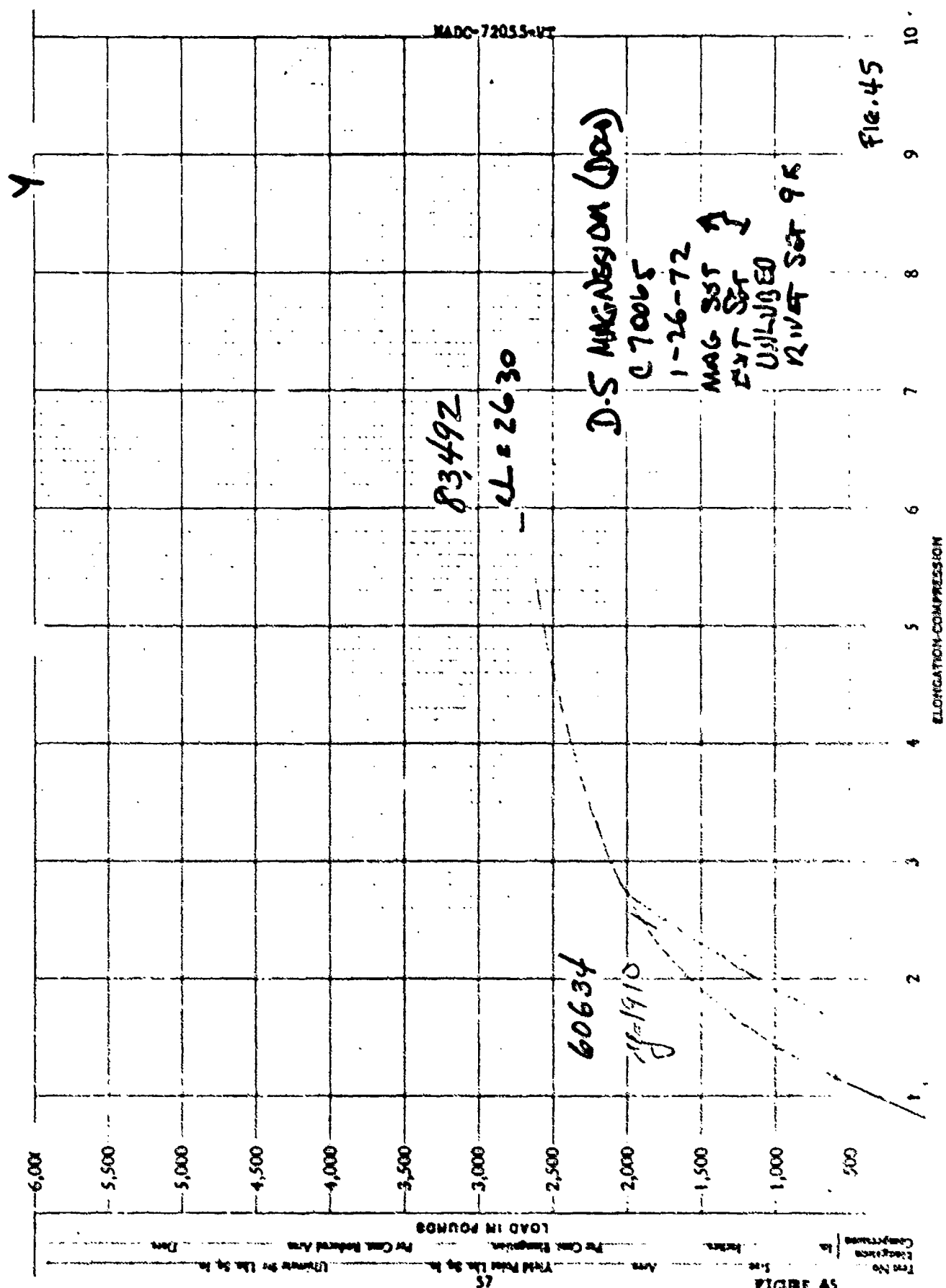


FIGURE 45

MADC-72055-VT

Fig. 45

ELONGATION-COMPRESSION

X

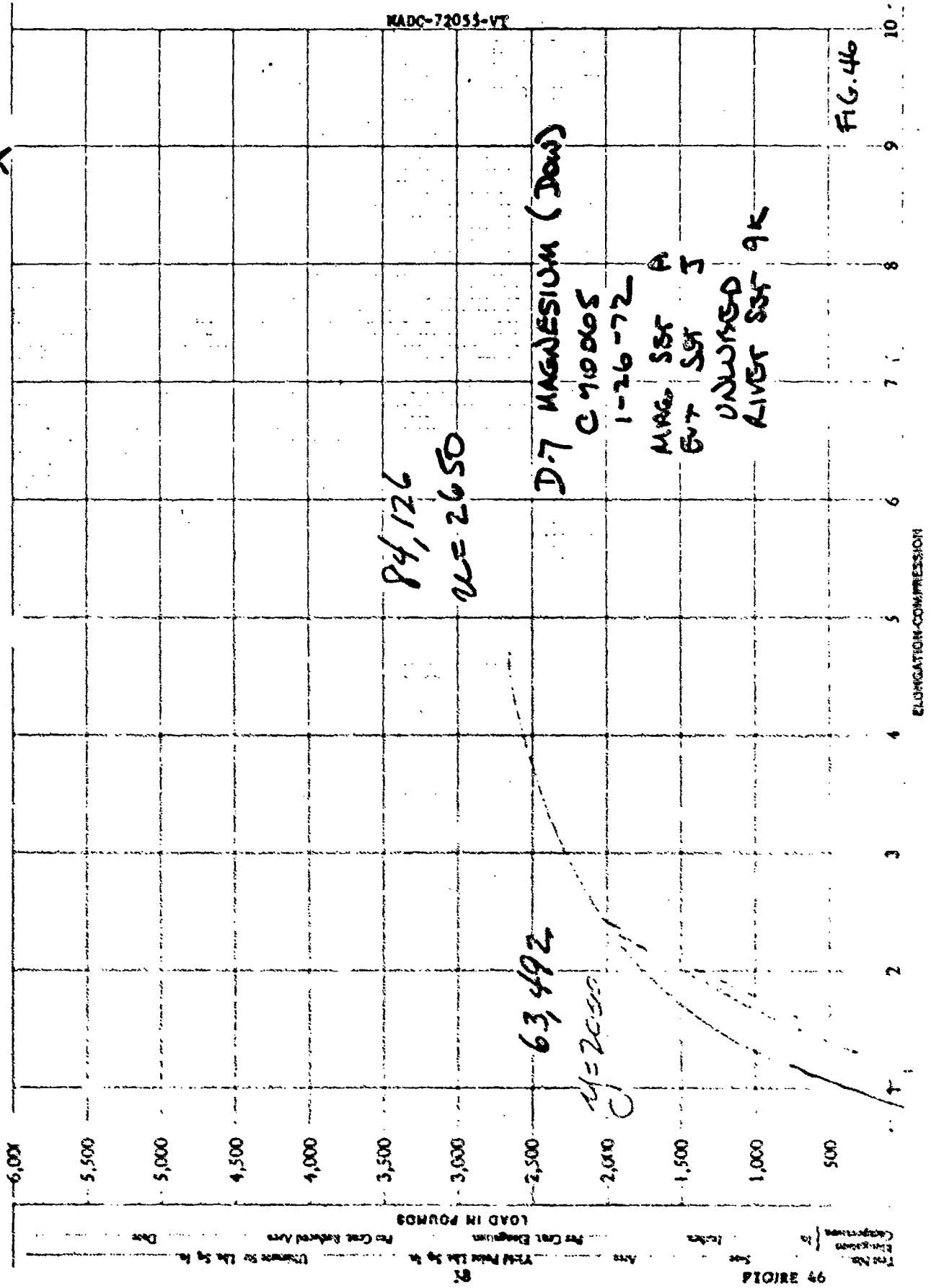
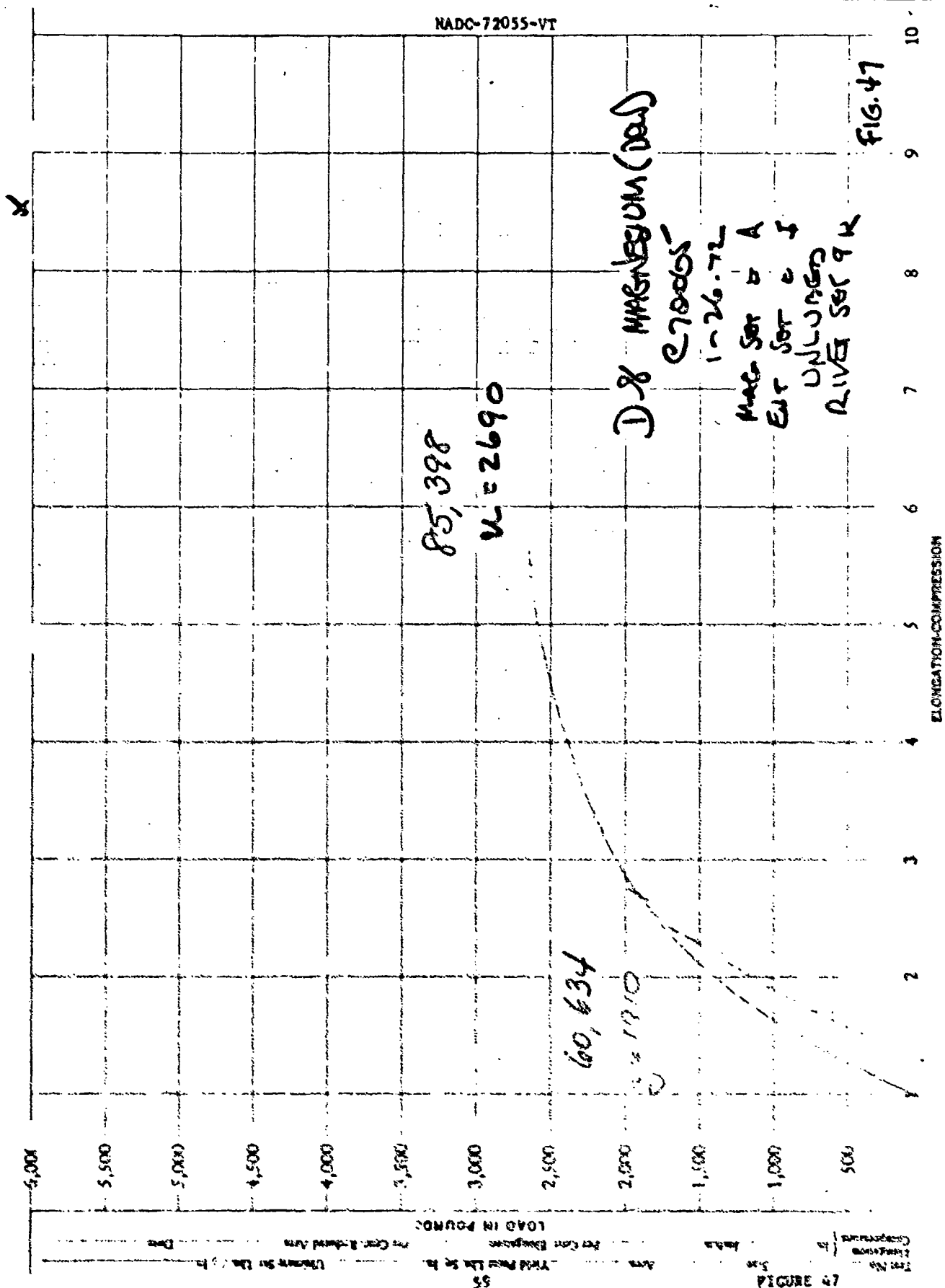


FIGURE 46

NADC-72055-VT



X

MAQC-72055-VT

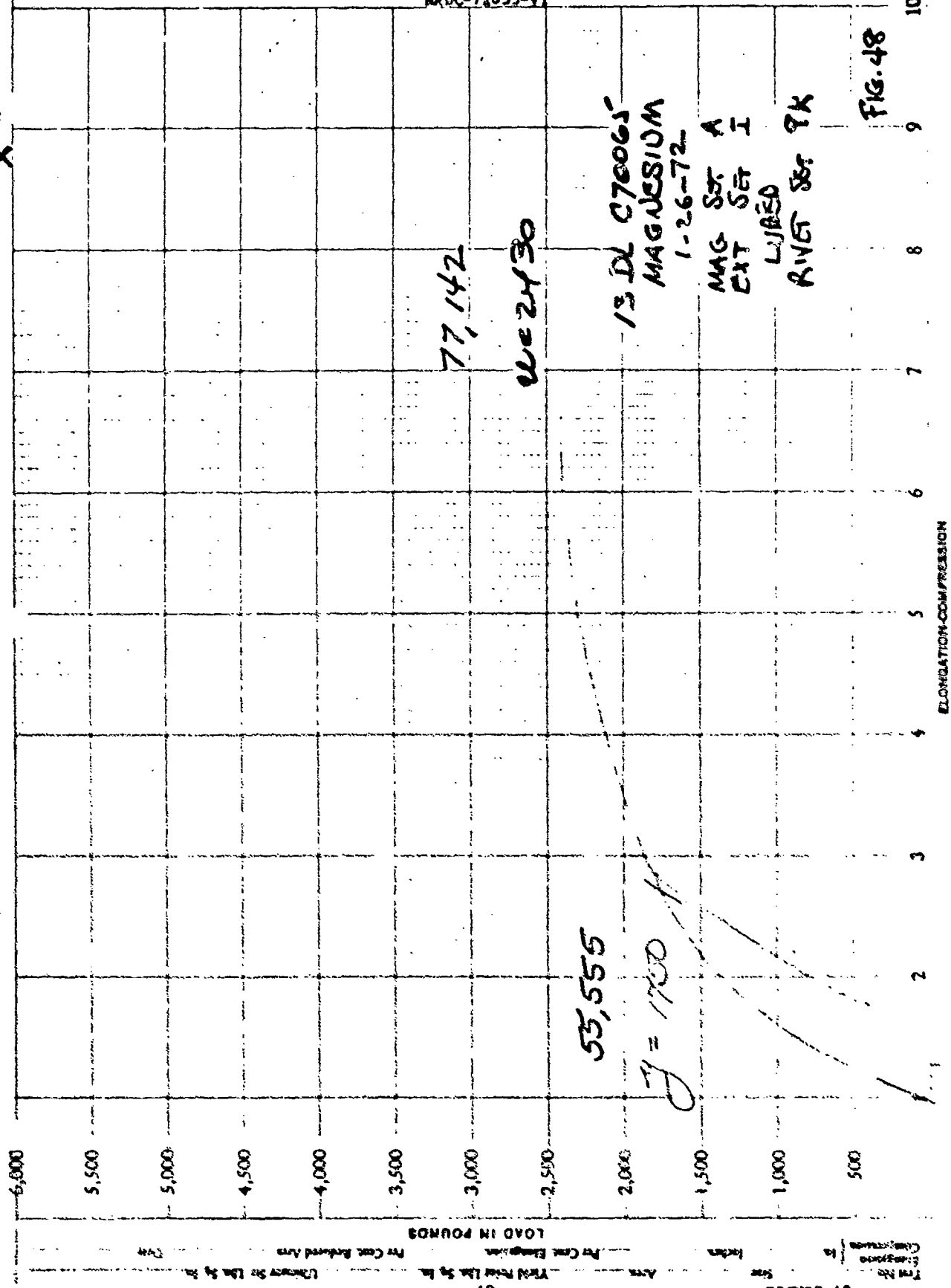
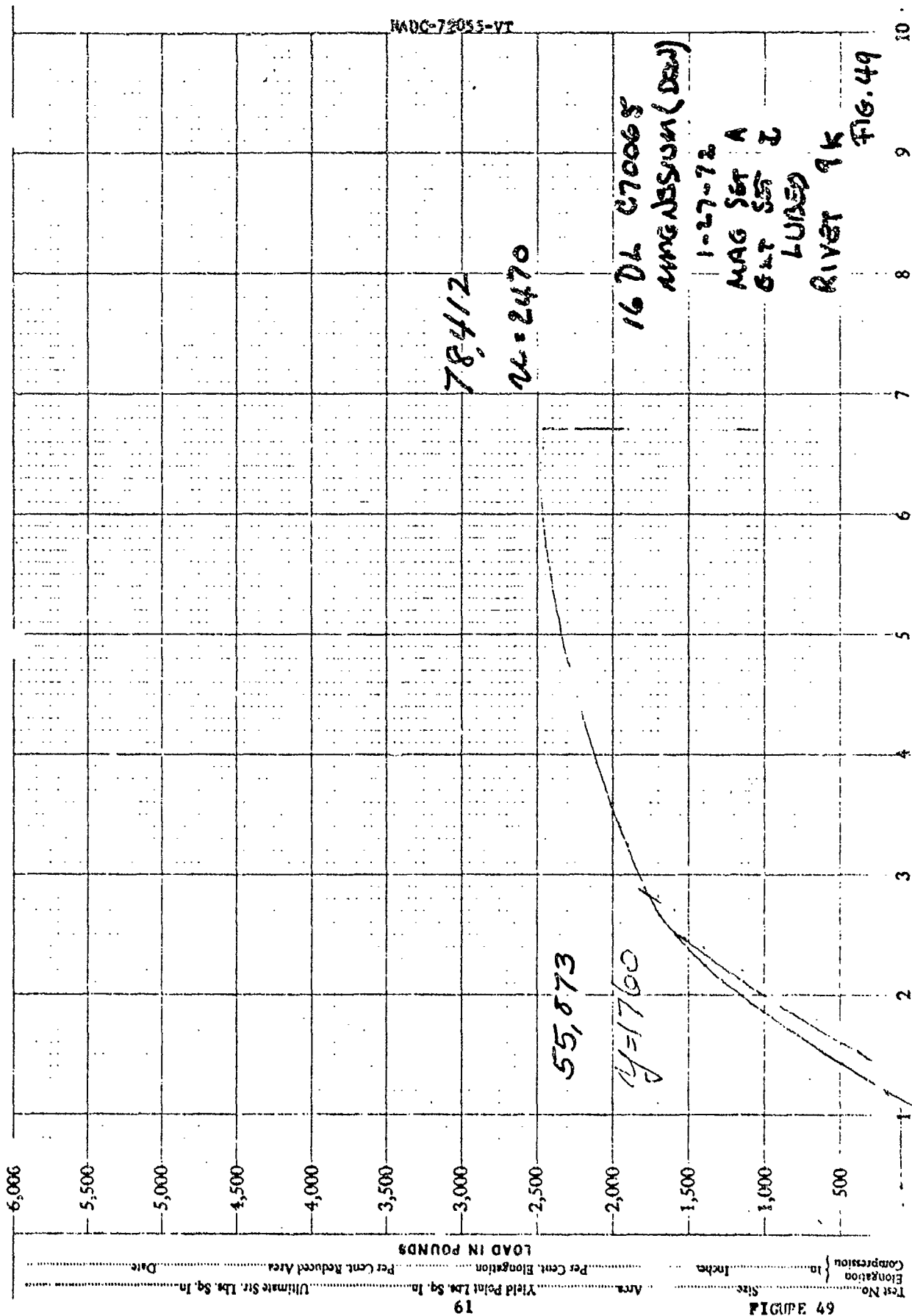
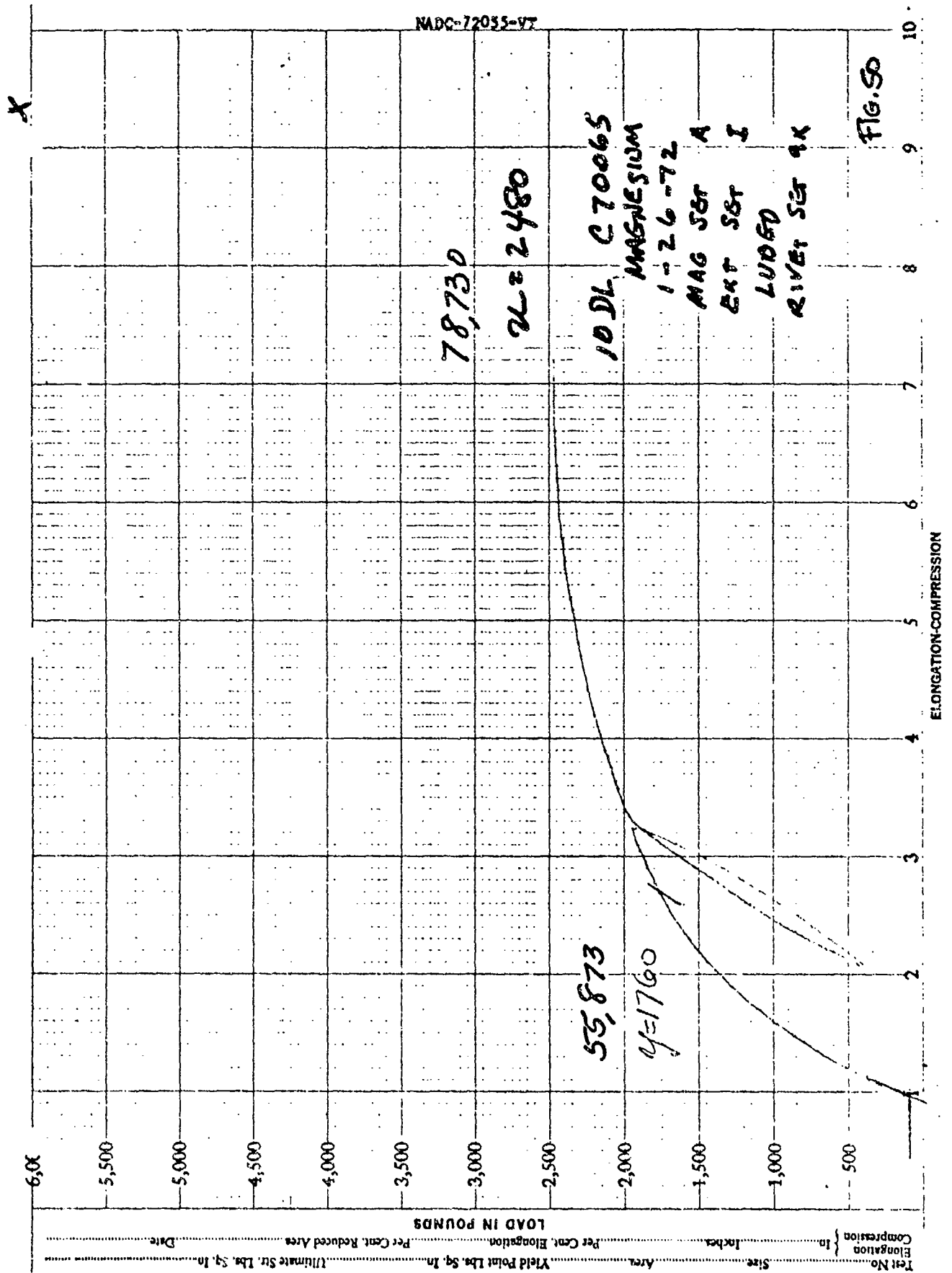


FIGURE 48







NADC-72055-VT

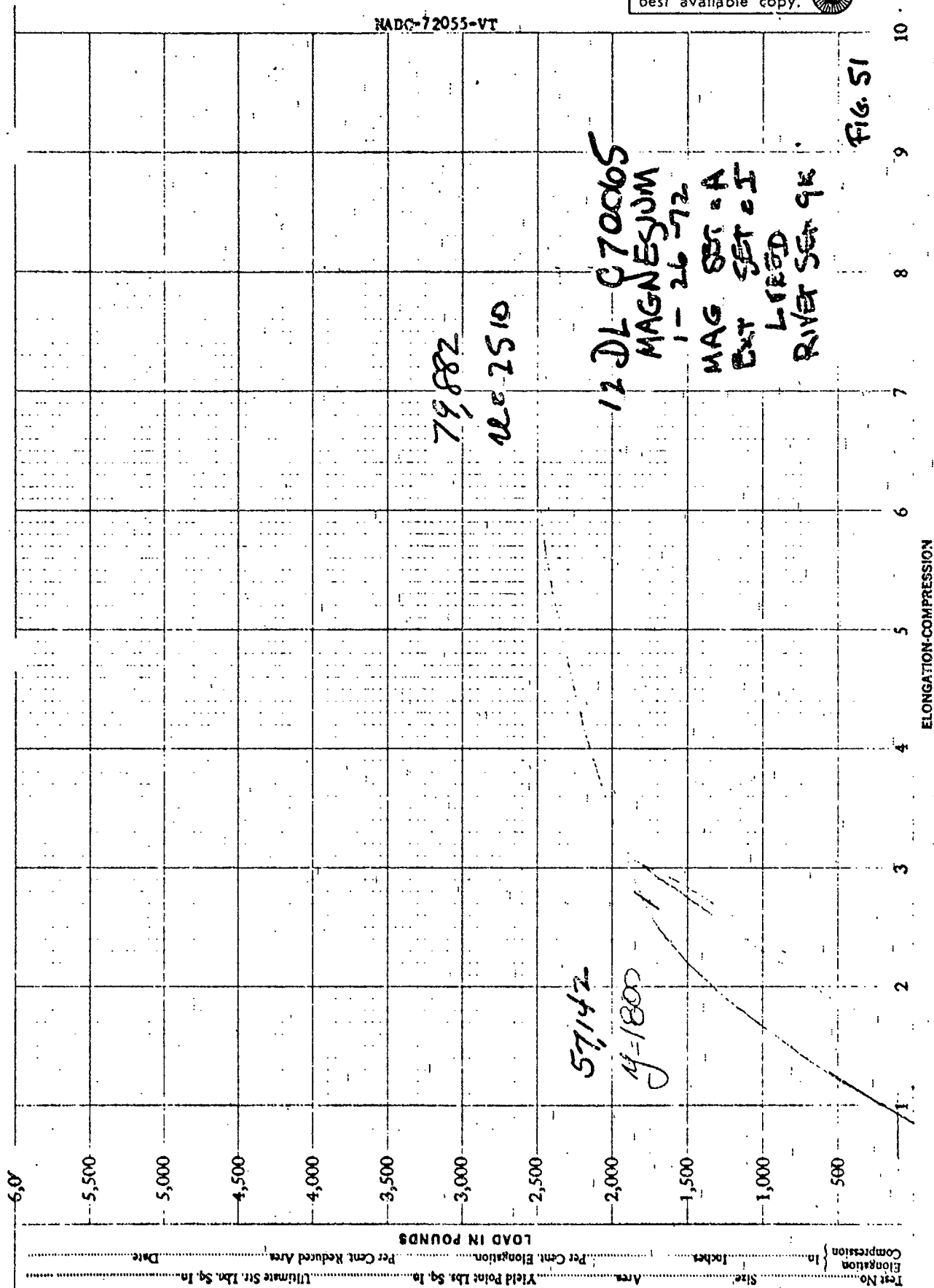


FIG. 51

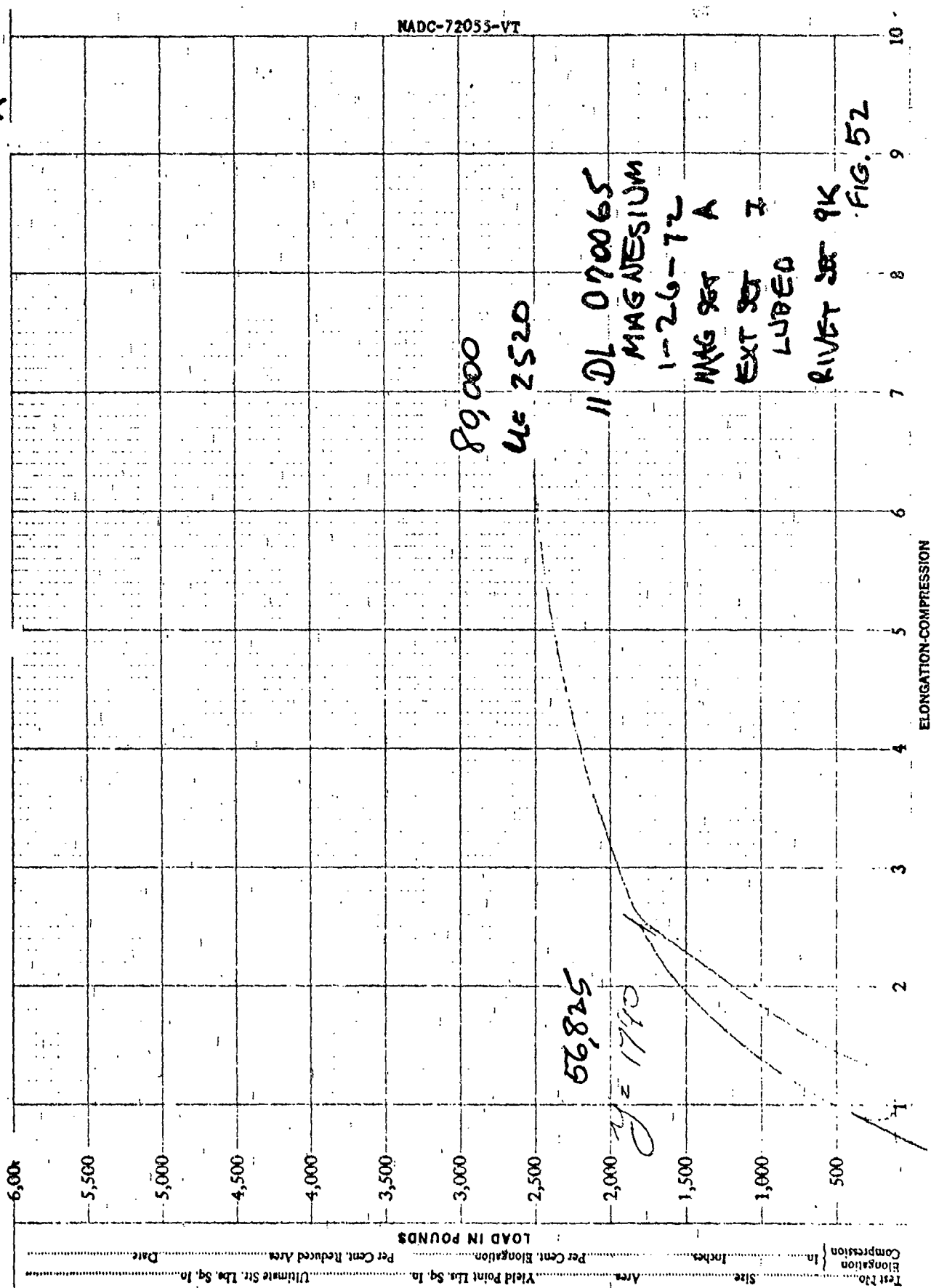


FIGURE 52

Test No. _____
 Elongation _____
 Compression _____
 Size _____
 Area _____
 Yield Point Lbs. Sq. In. _____
 Ultimate Str. Lbs. Sq. In. _____
 Per Cent. Elongation _____
 Per Cent. Reduced Area _____
 Date _____

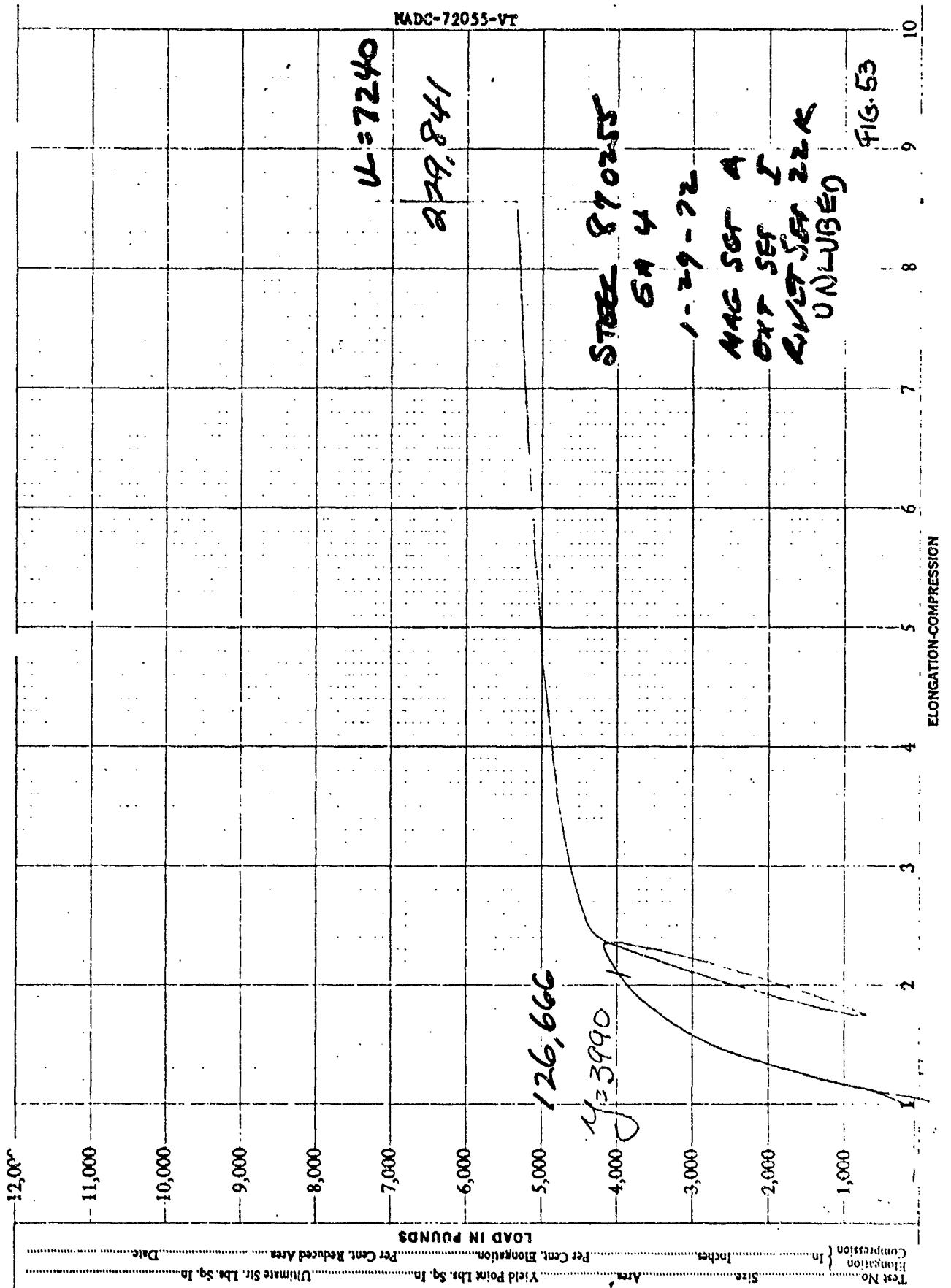


FIGURE 53

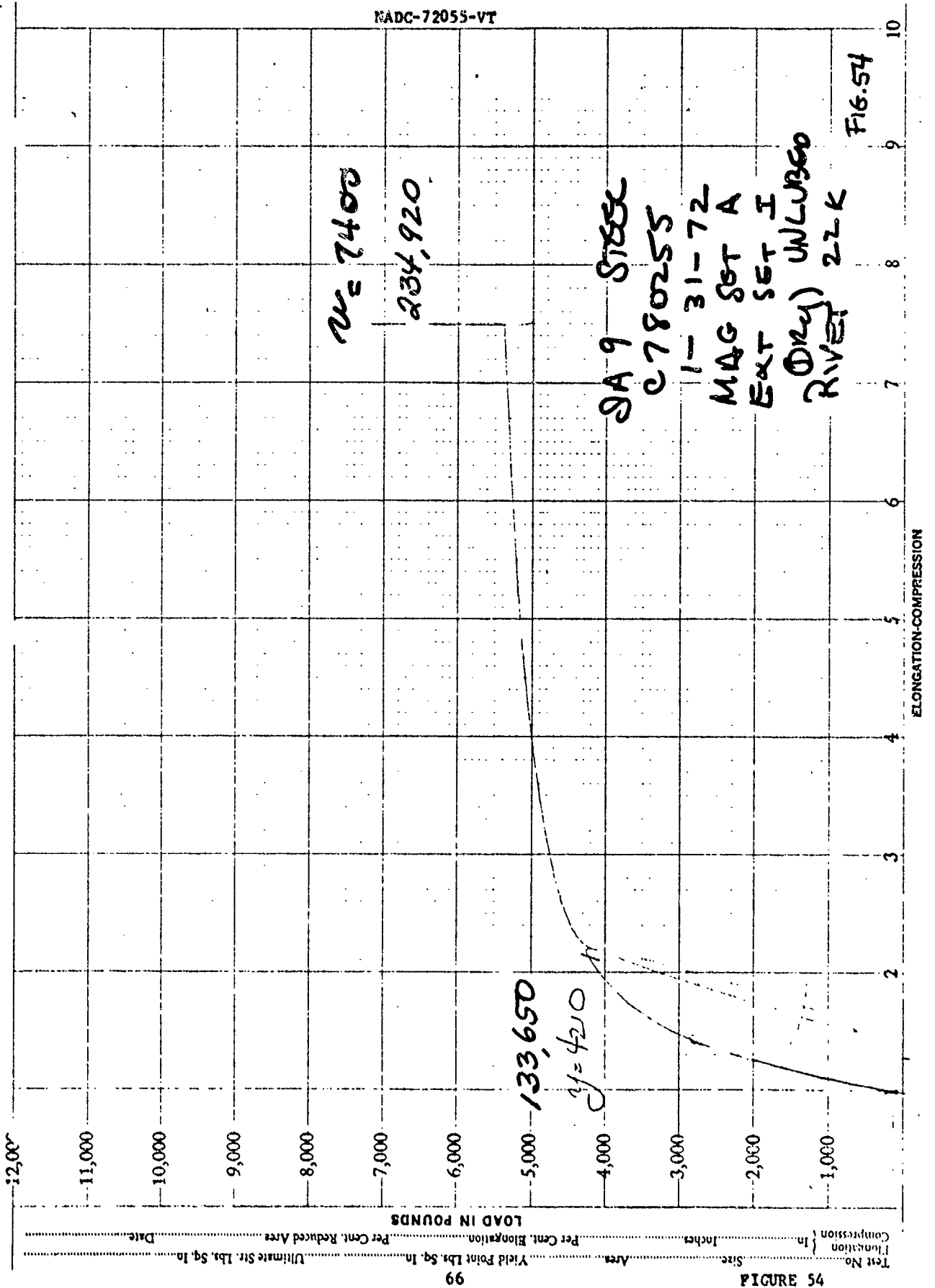
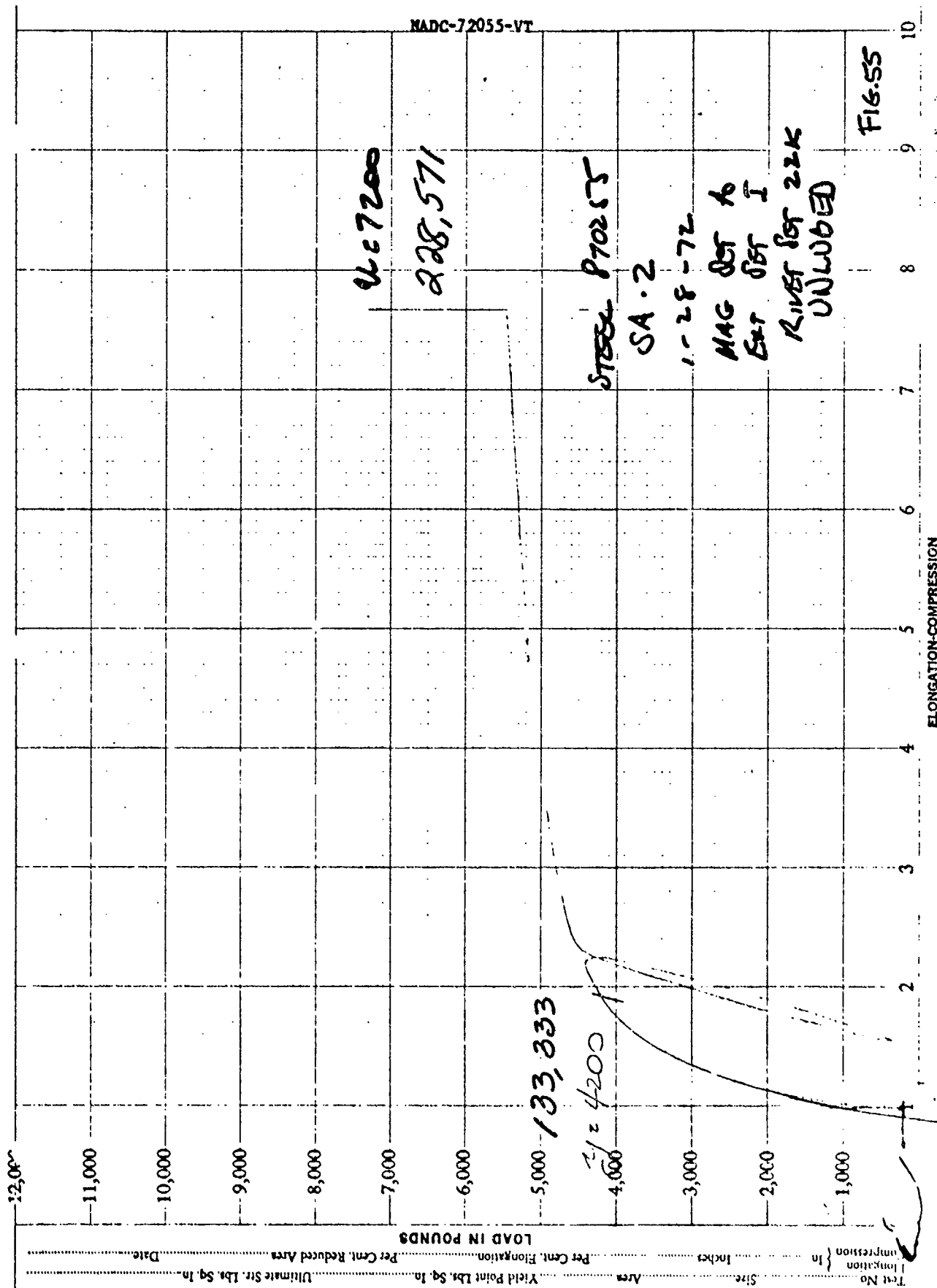


FIGURE 54



NADC-72055-VT

FIGURE 55

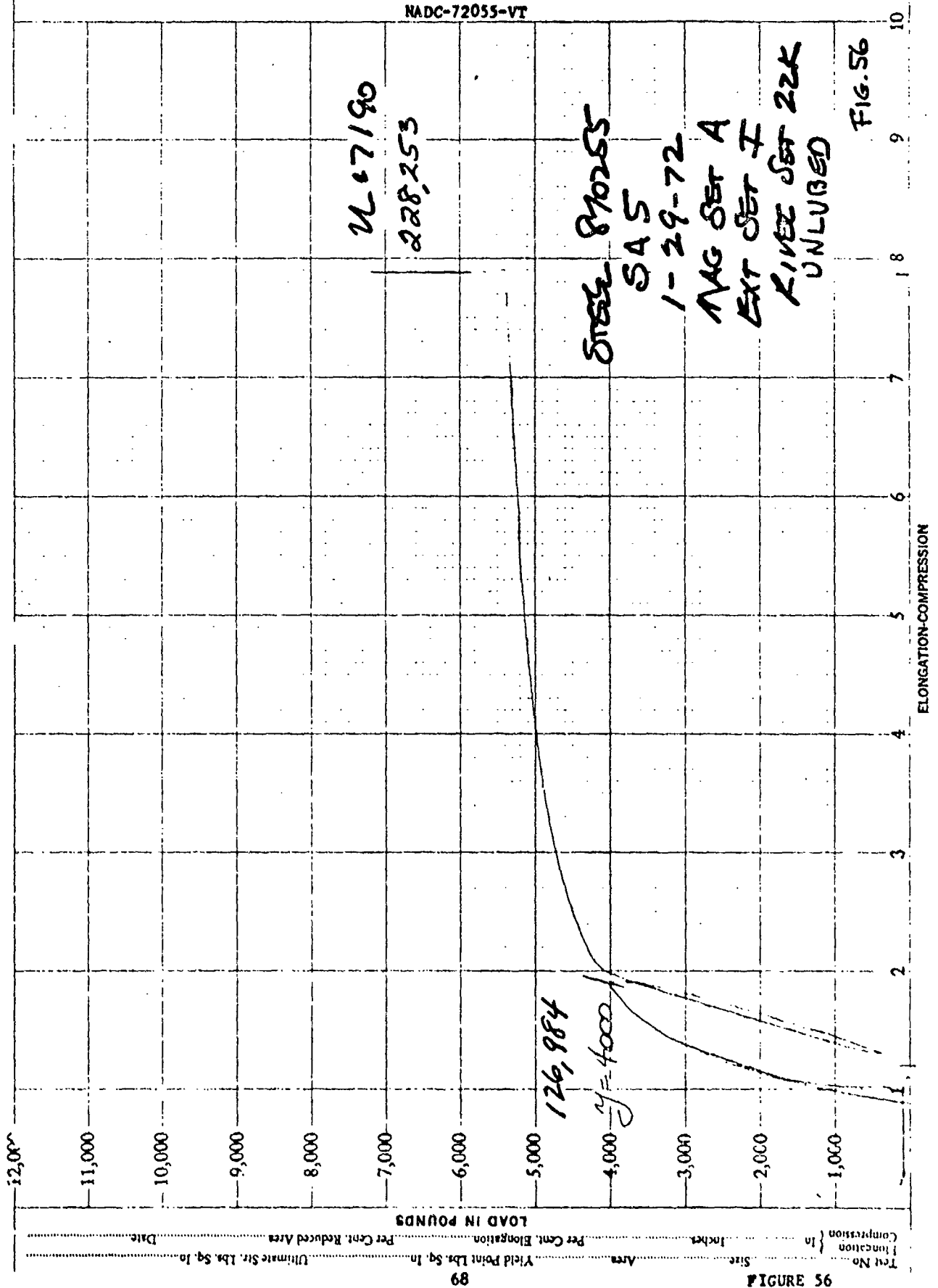


FIGURE 56

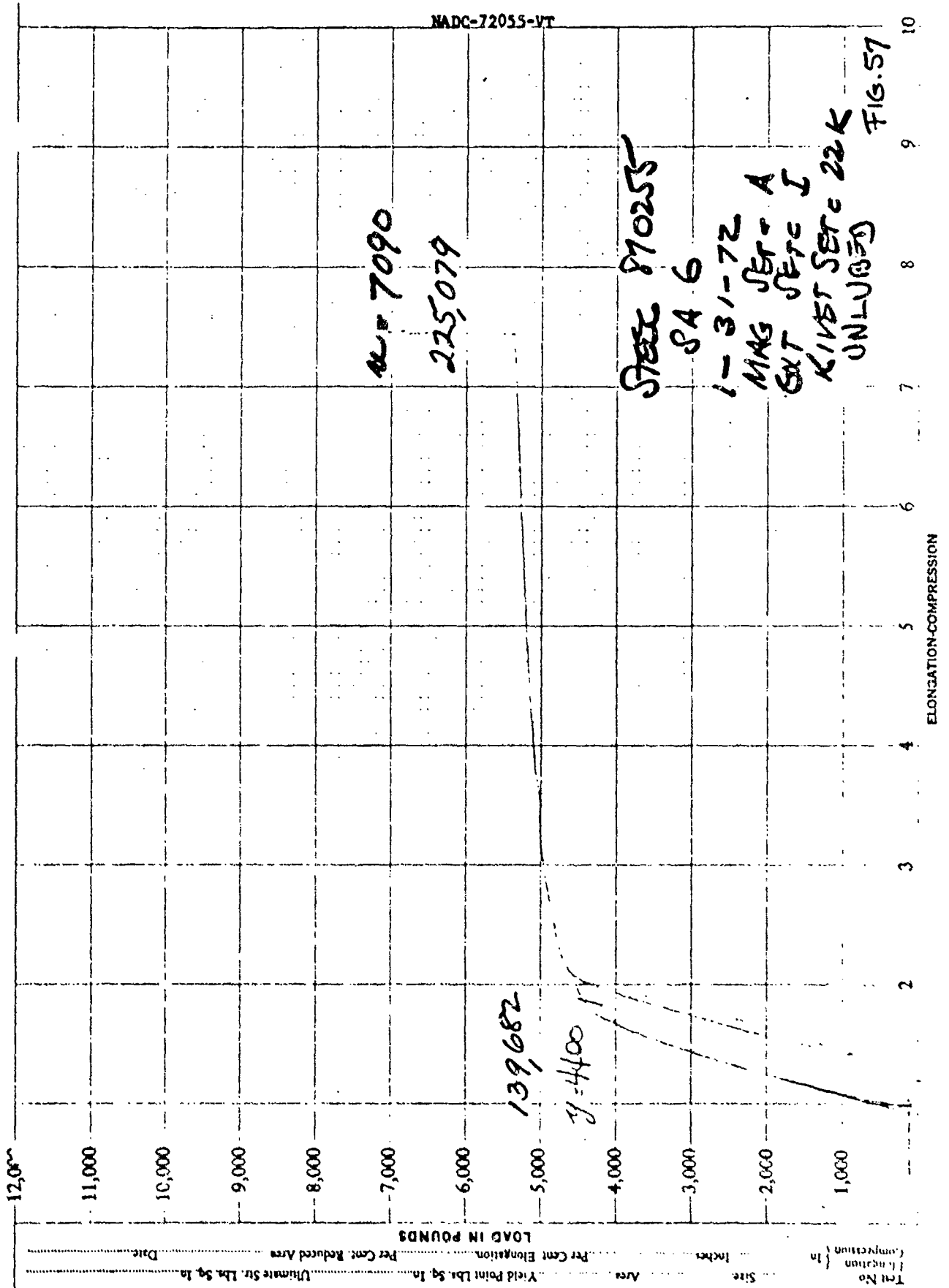


FIGURE 57

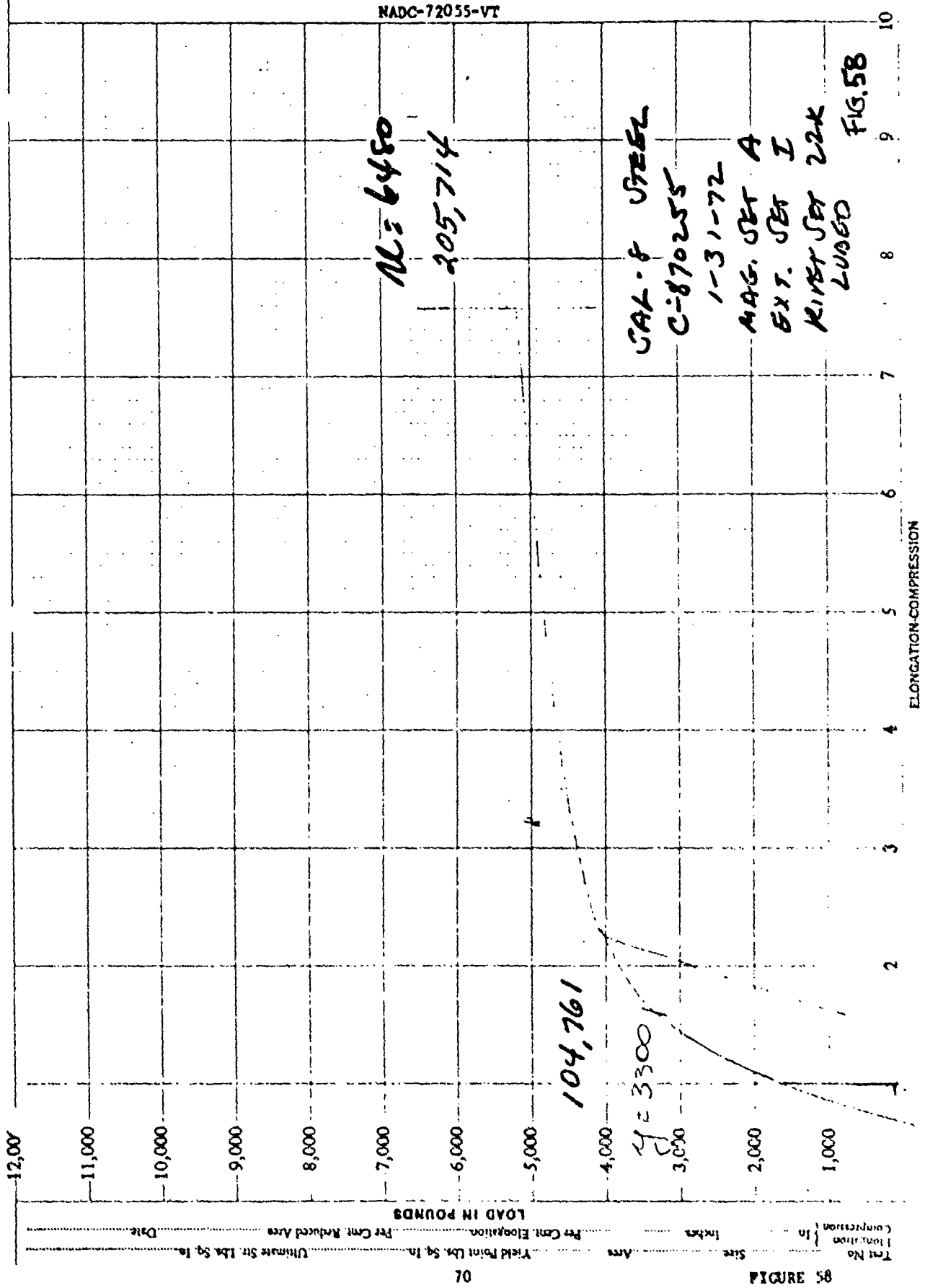
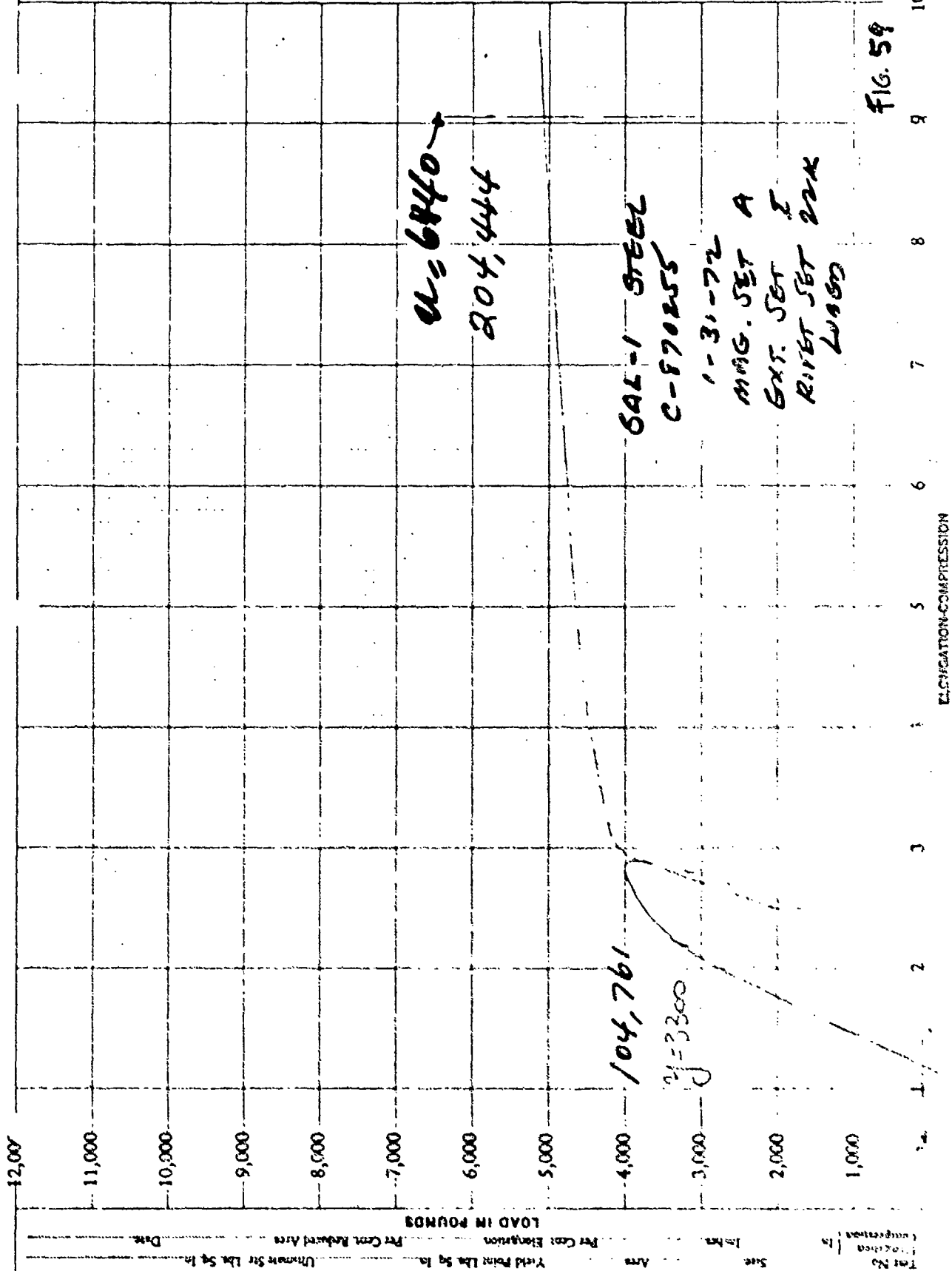


FIGURE 58



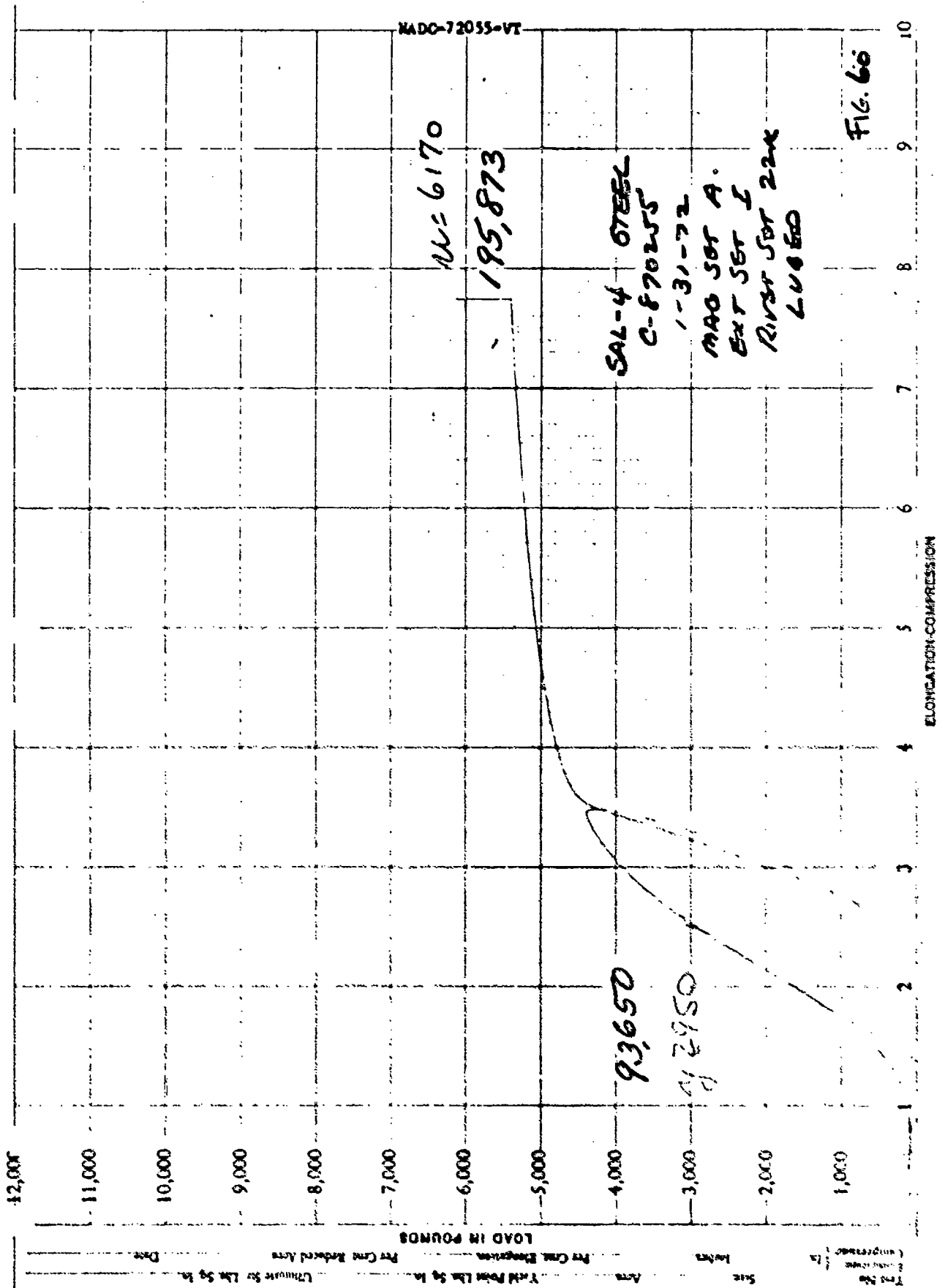
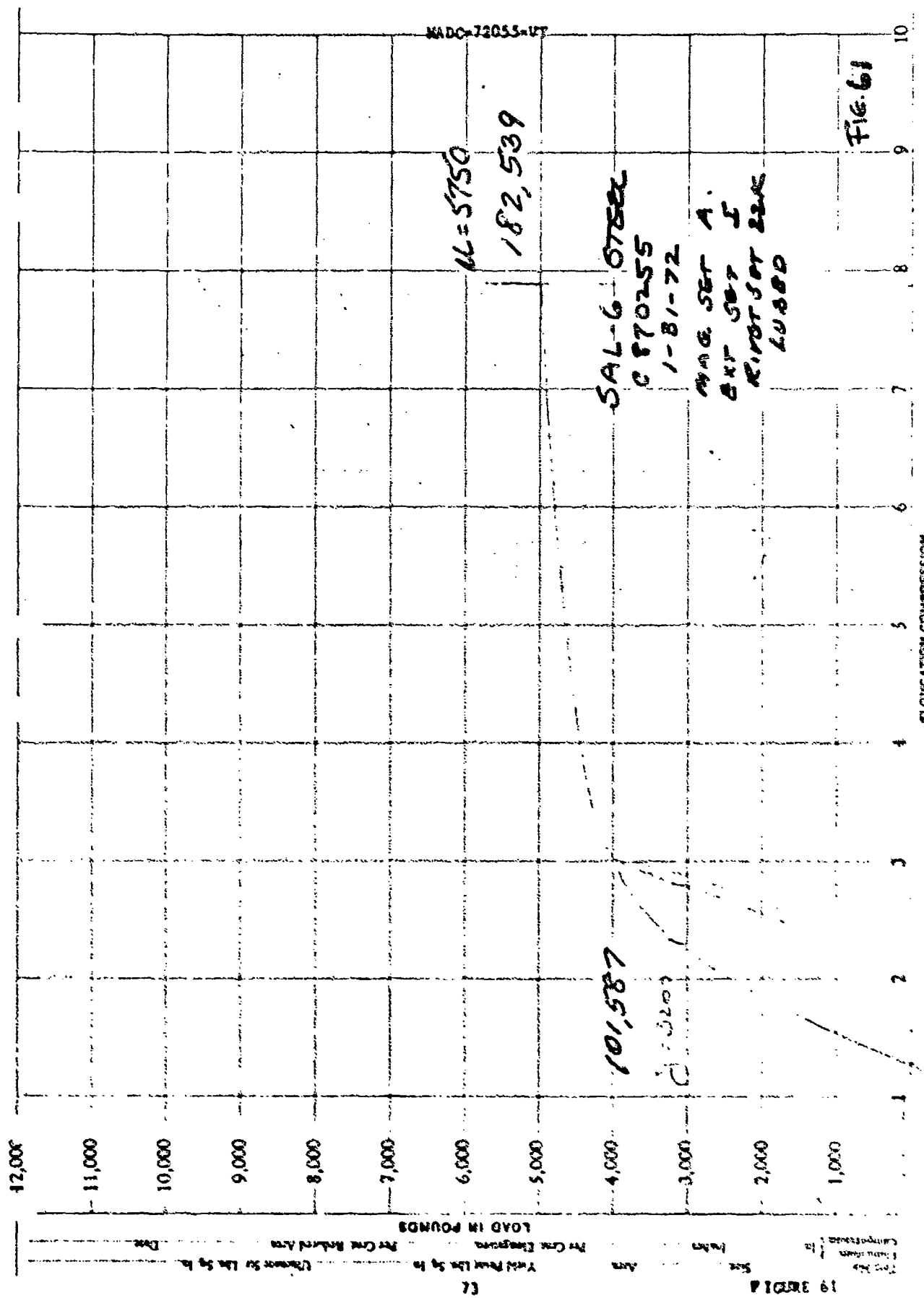
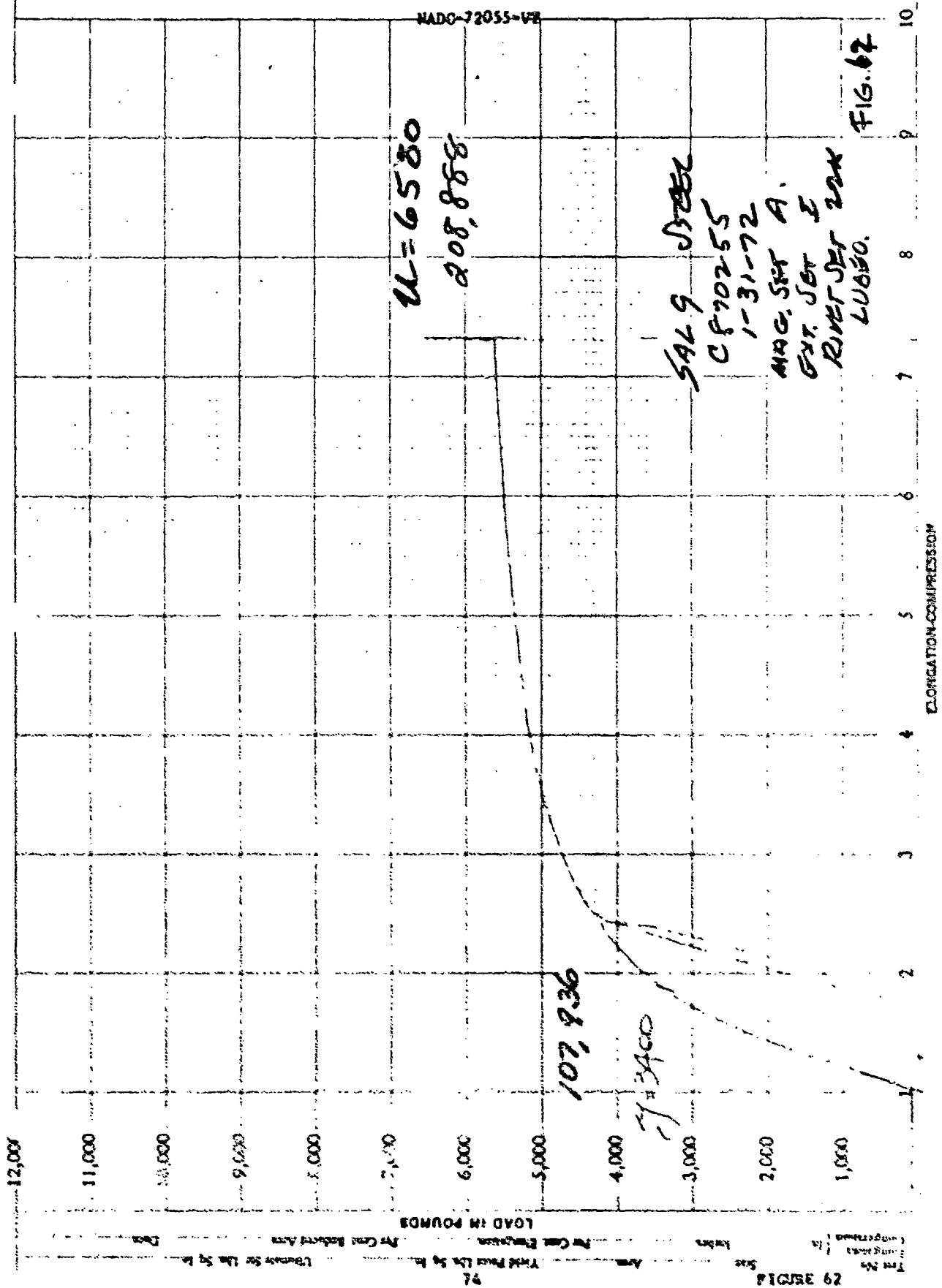
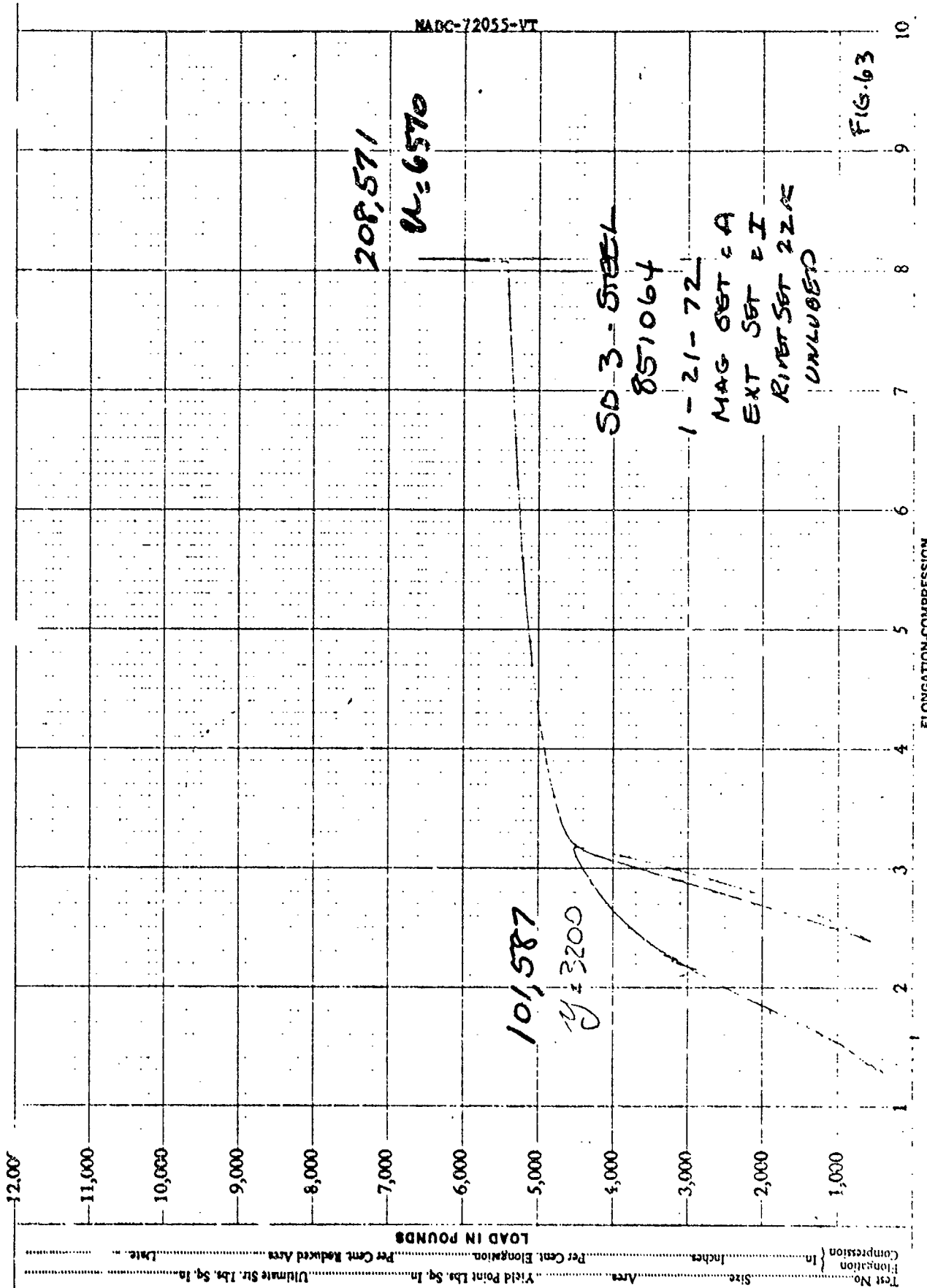


FIGURE 60

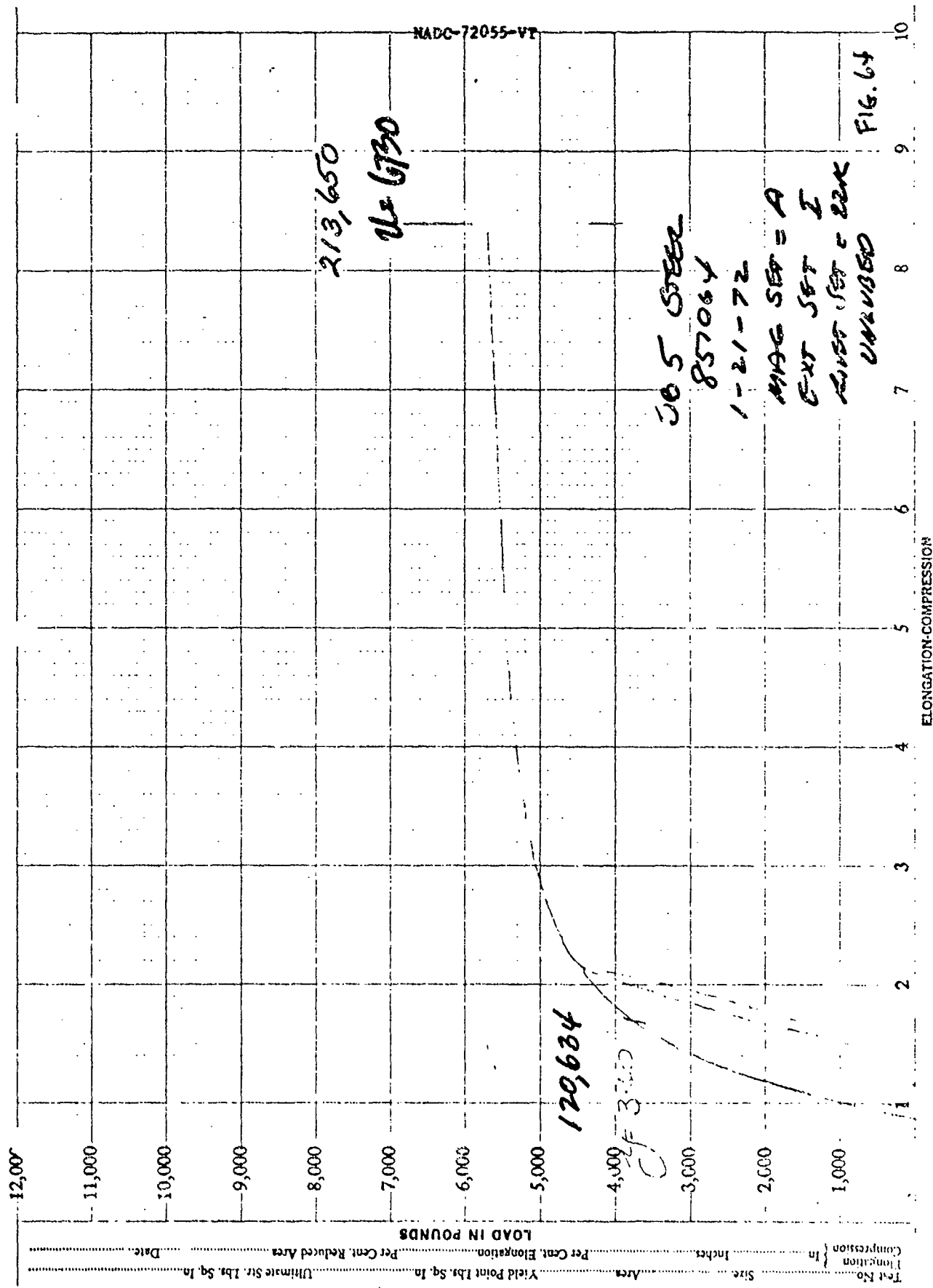


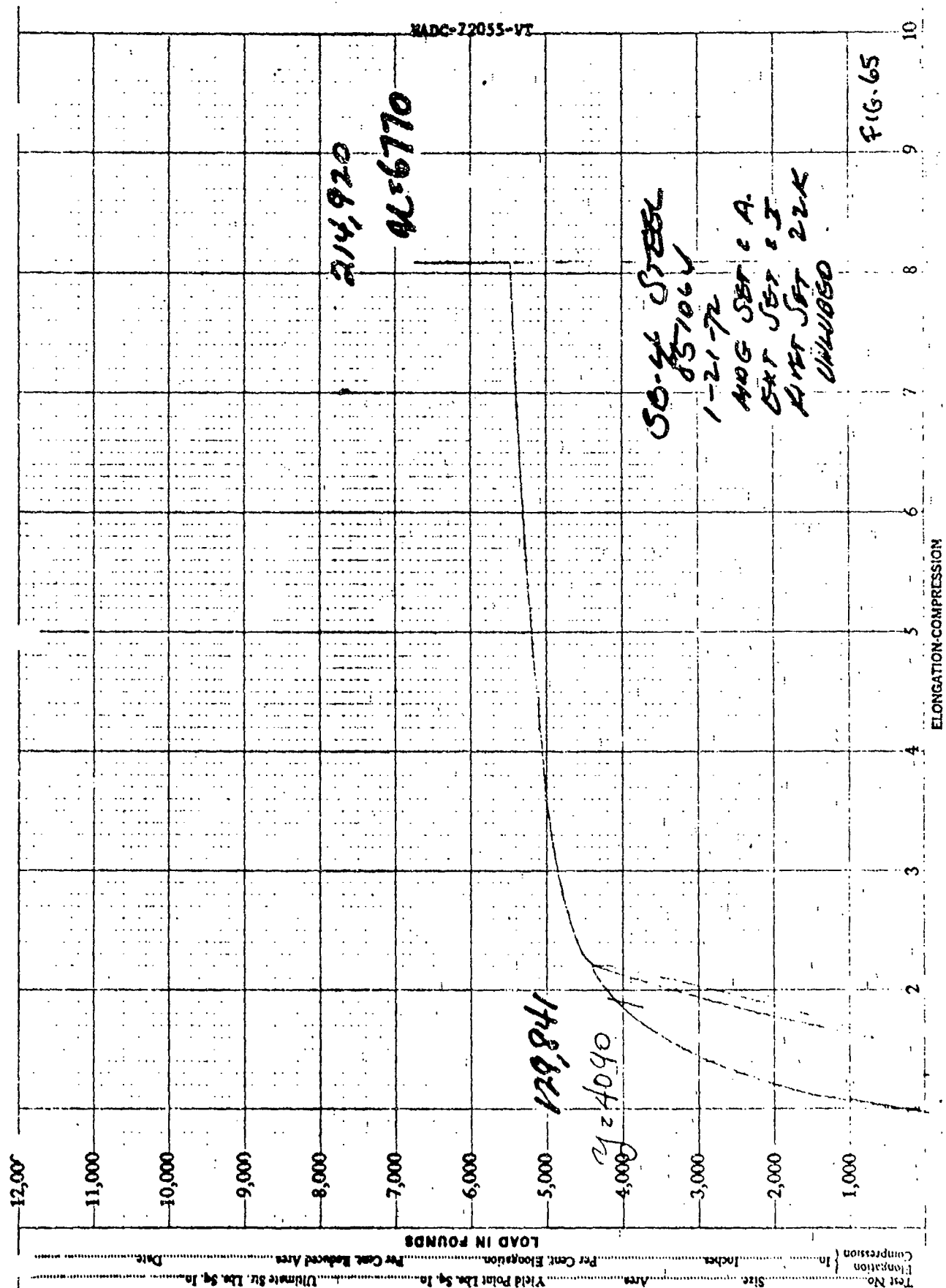




NABG-72055-VT

FIGURE 63





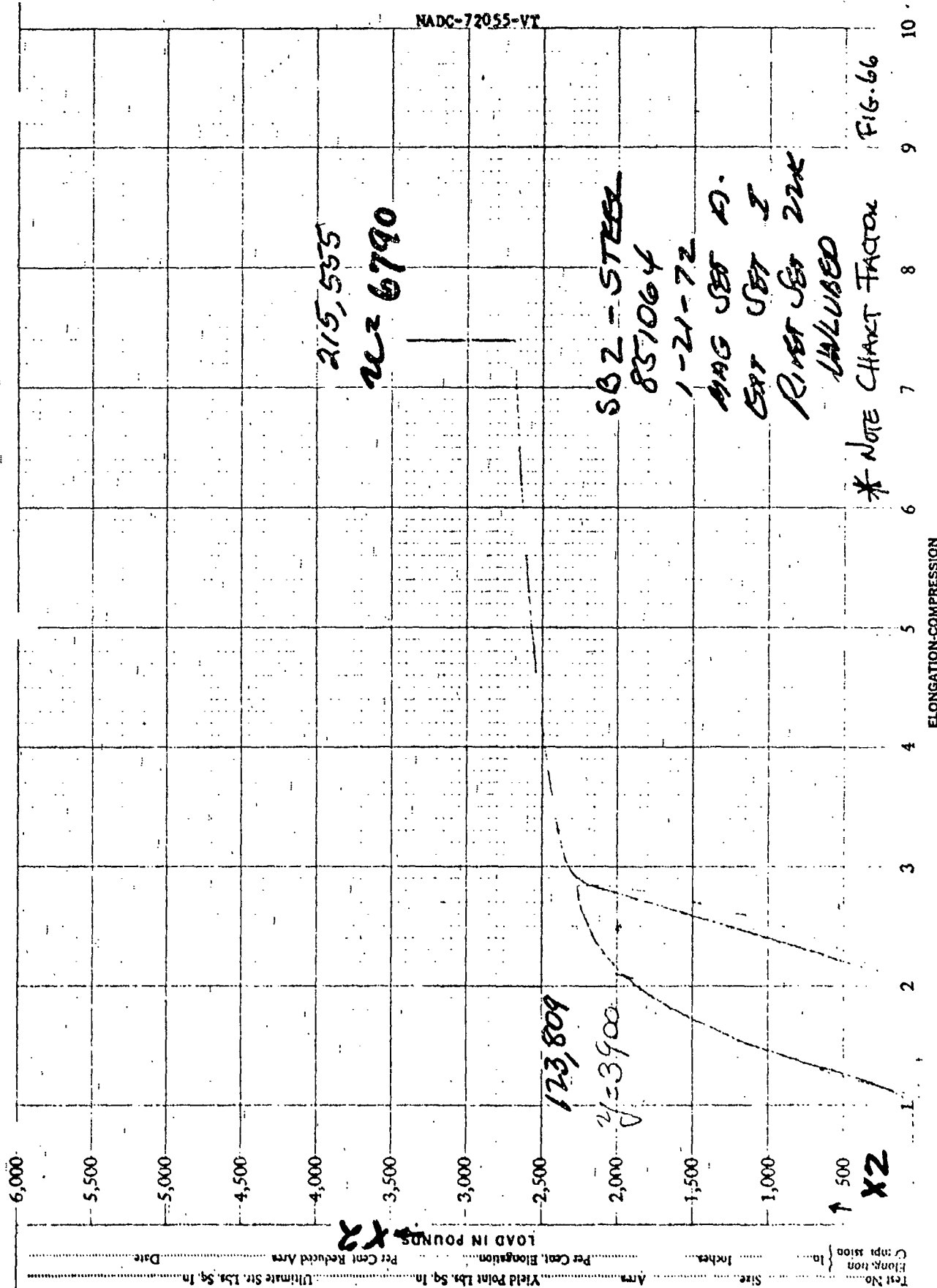
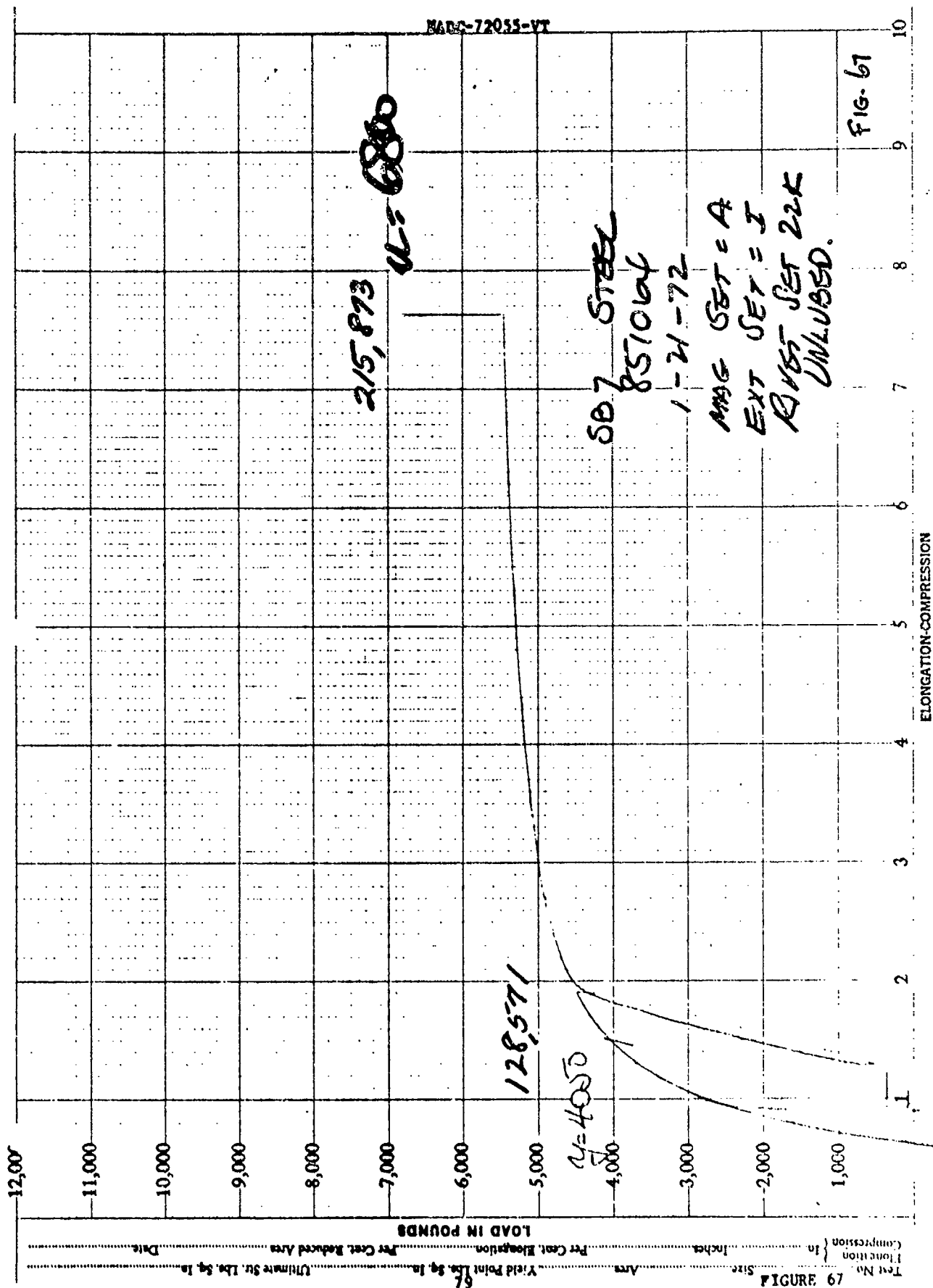
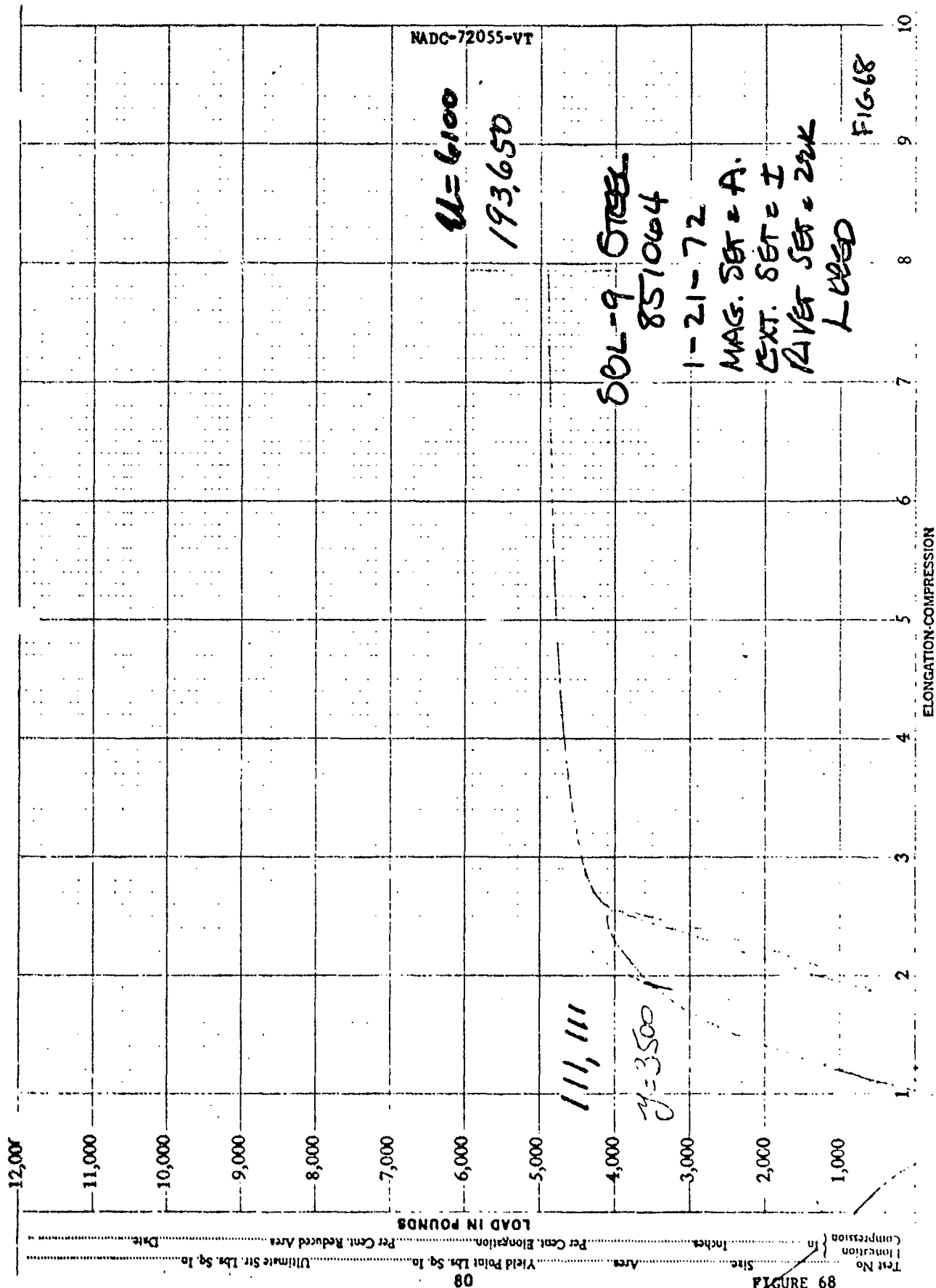
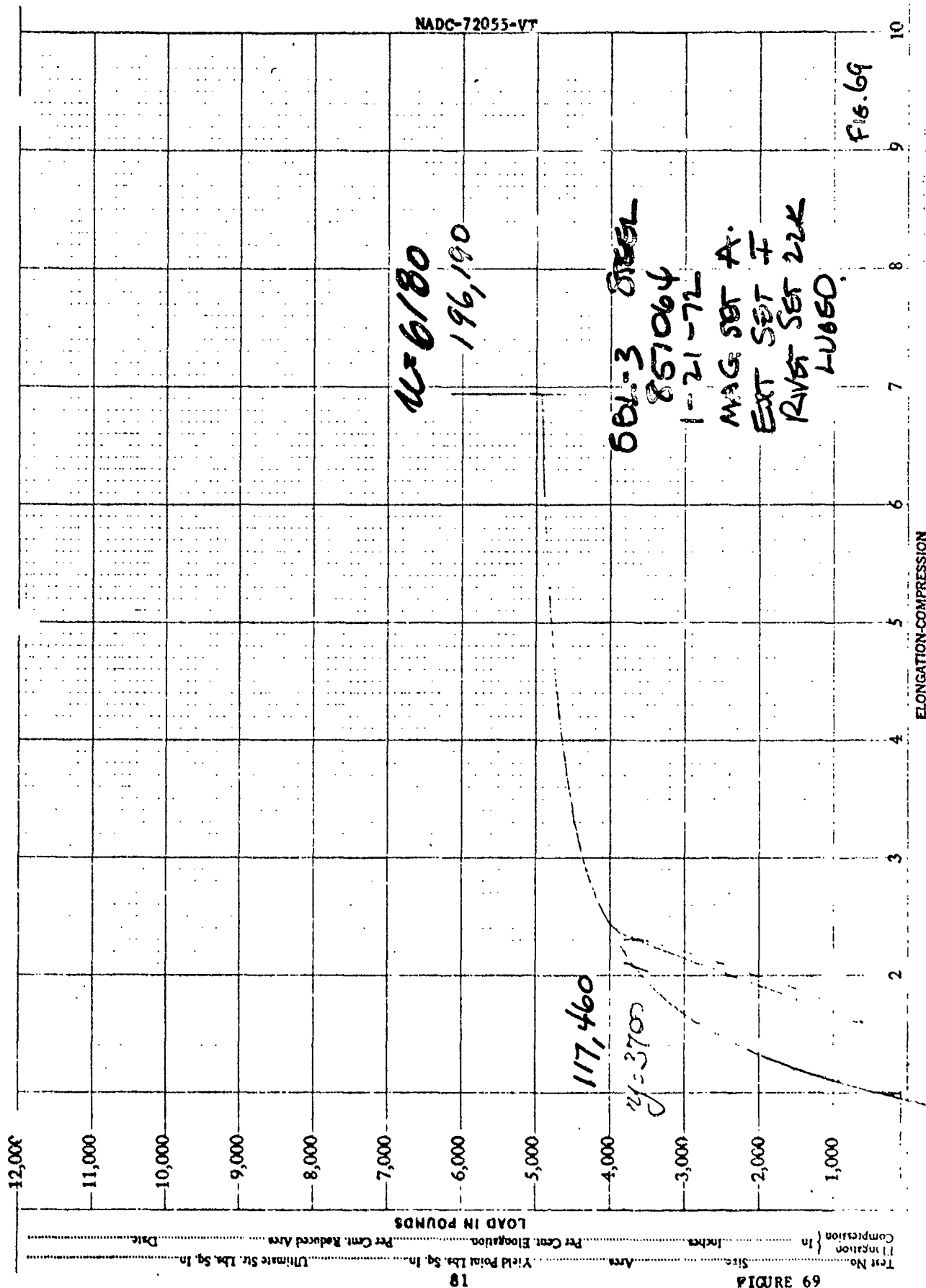


FIGURE 66

Test No. _____ Date _____
 Elongation _____
 Size _____
 Area _____
 Yield Point Lbs. Sq. In. _____
 Per Cent. Elongation _____
 Ultimate Str. Lbs. Sq. In. _____
 Per Cent. Reduced Area _____







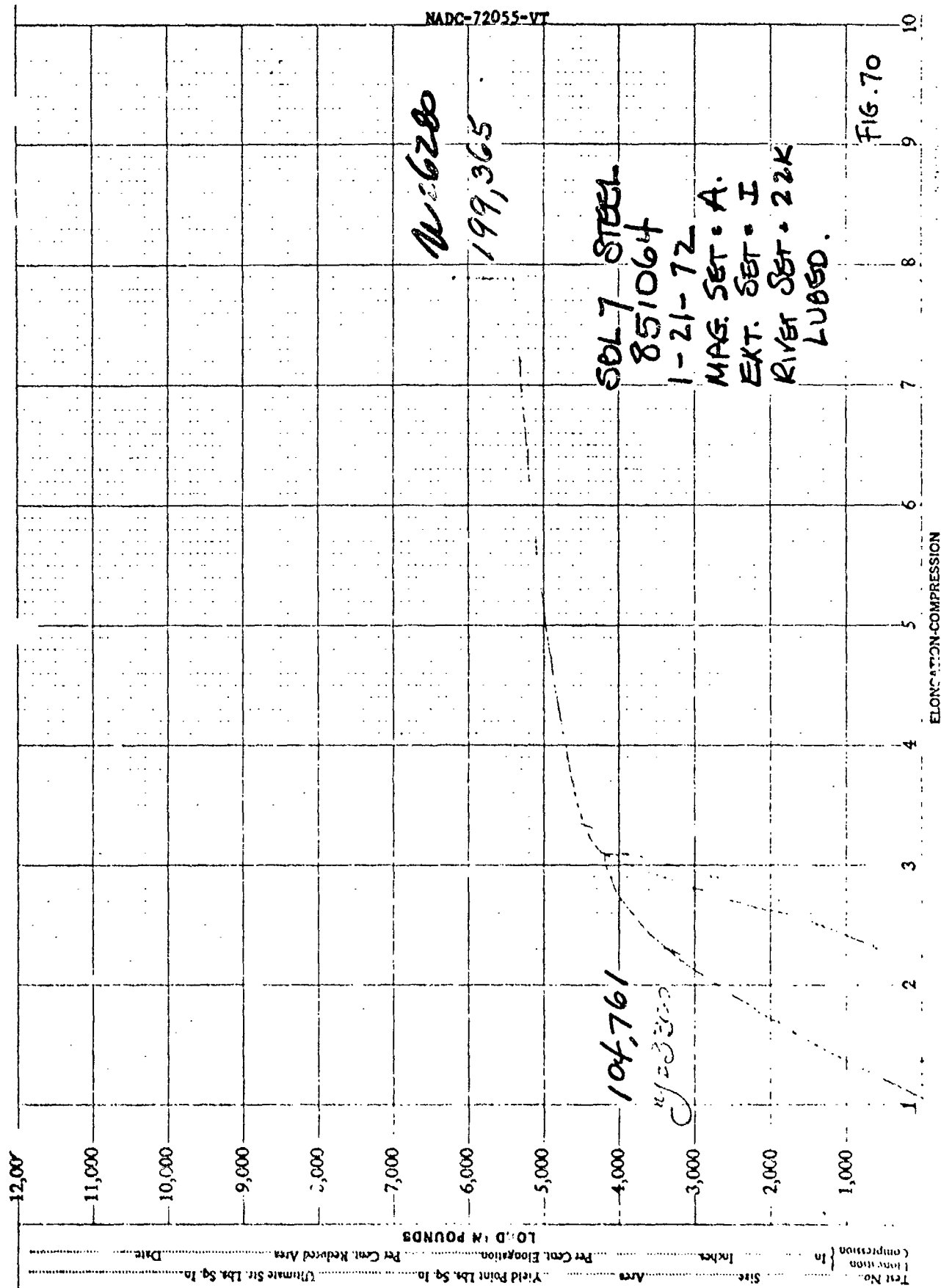


FIGURE 70

Test No. _____
 In _____
 Compression _____
 Area _____
 Yield Point Lbs. Sq. In. _____
 Ultimate Str. Lbs. Sq. In. _____
 Per Cent. Elongation _____
 Per Cent. Reduced Area _____
 Date _____

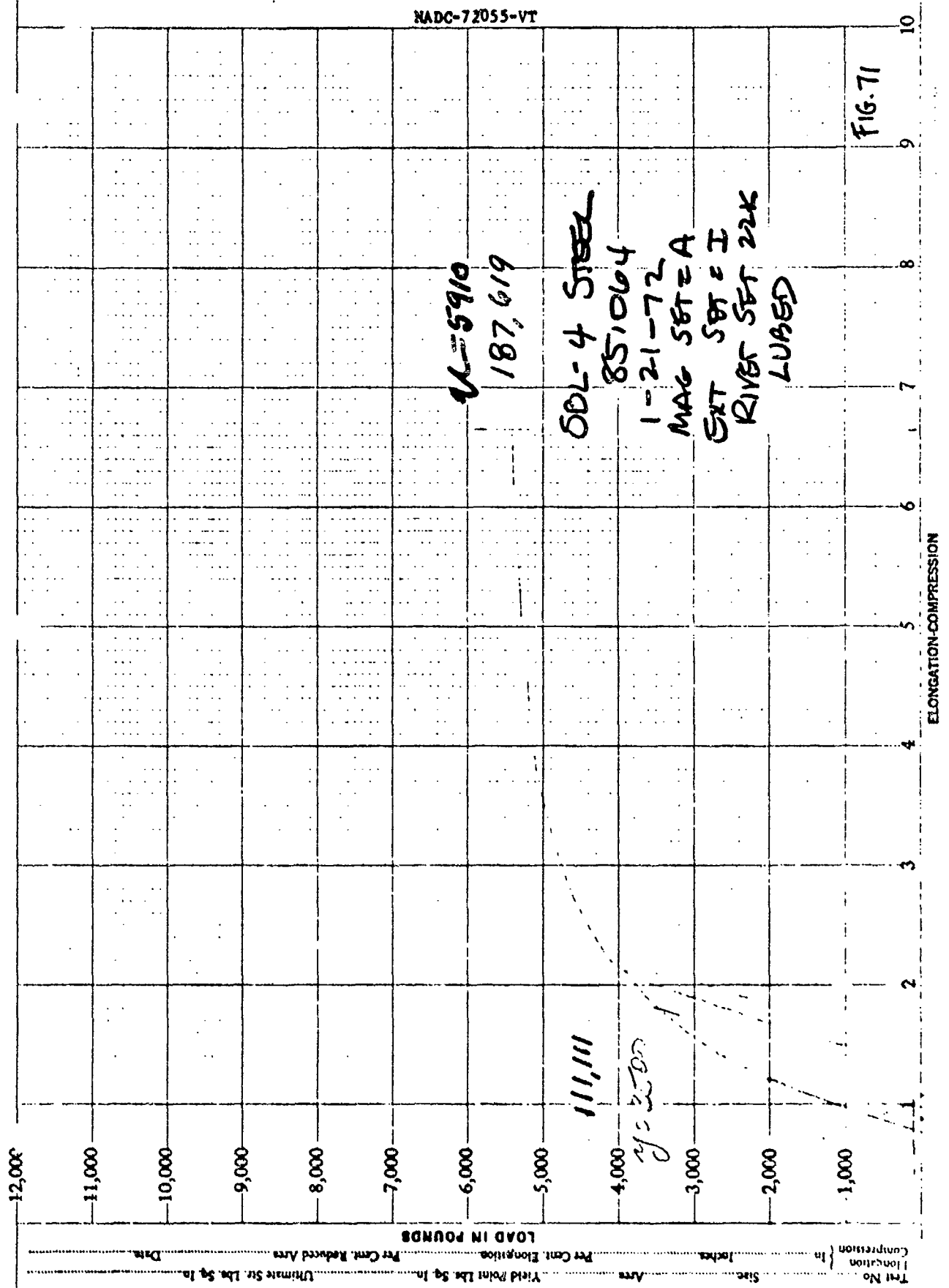
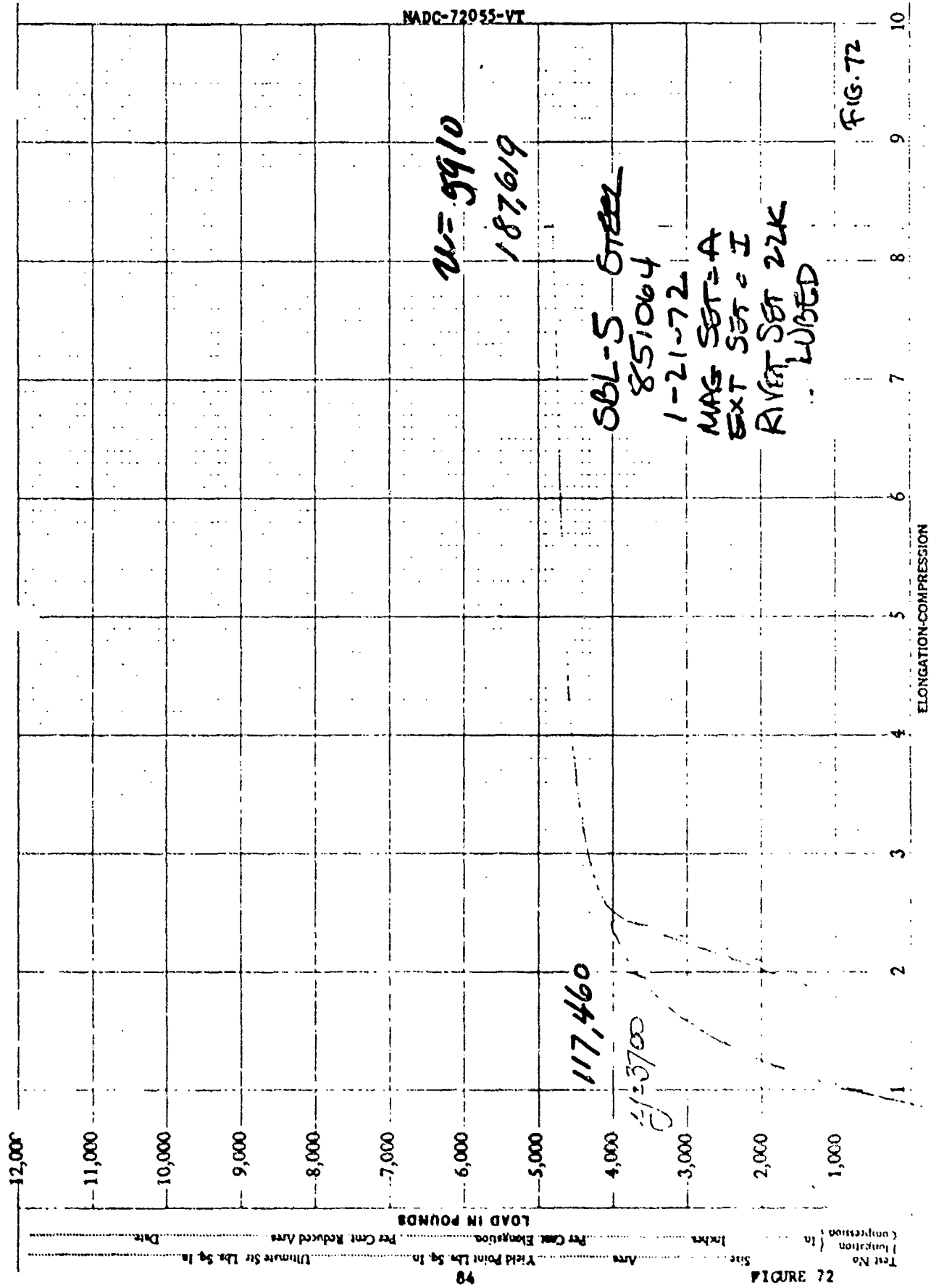
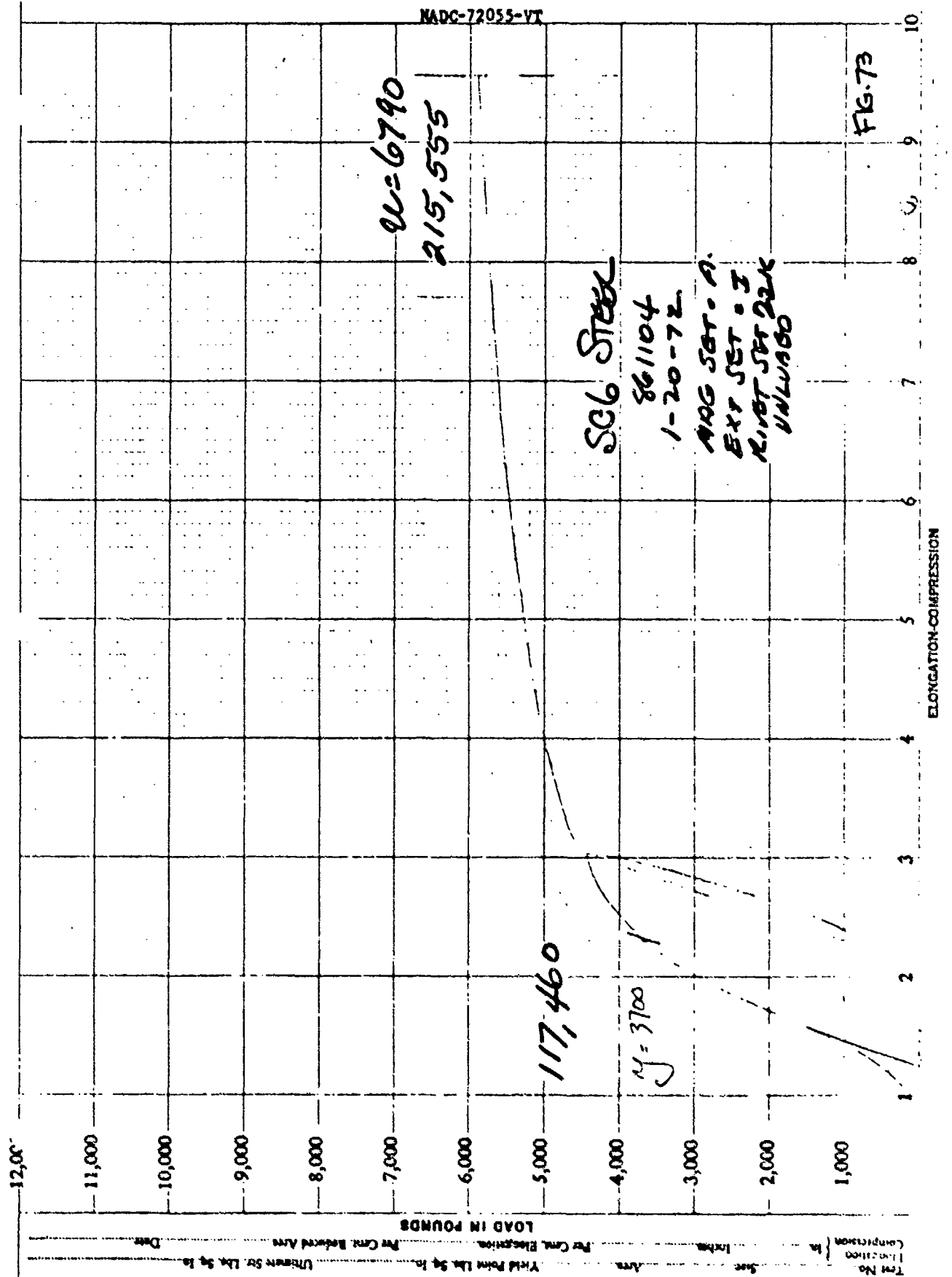


FIGURE 71



Test No. _____
 Elongation (compression) in _____
 Size _____
 Area _____
 Yield Point Lbs. Sq. In. _____
 Per Cent Elongation _____
 Ultimate Str. Lbs. Sq. In. _____
 Per Cent Reduced Area _____
 Date _____

FIGURE 72



NADC-72055-VT

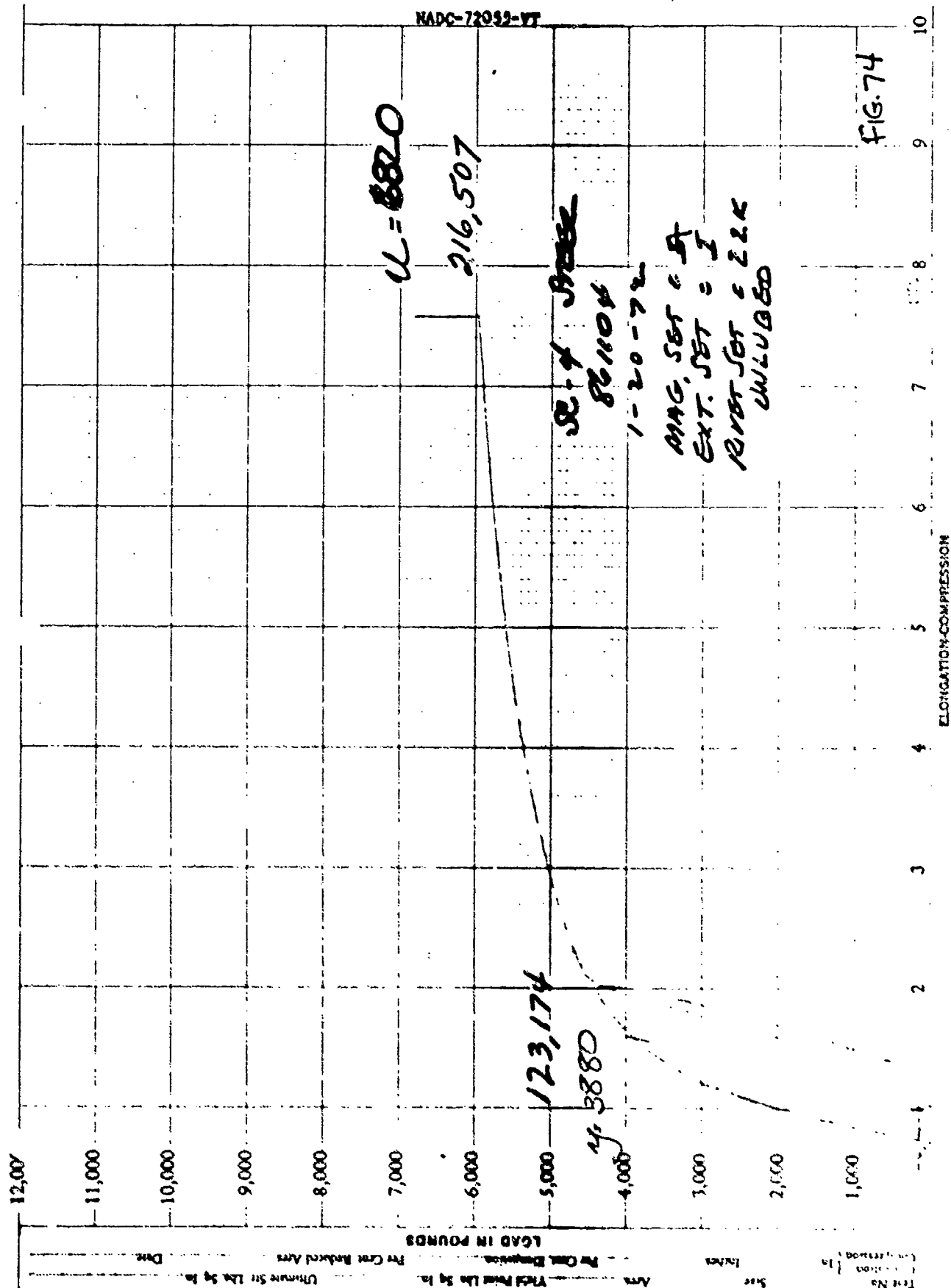
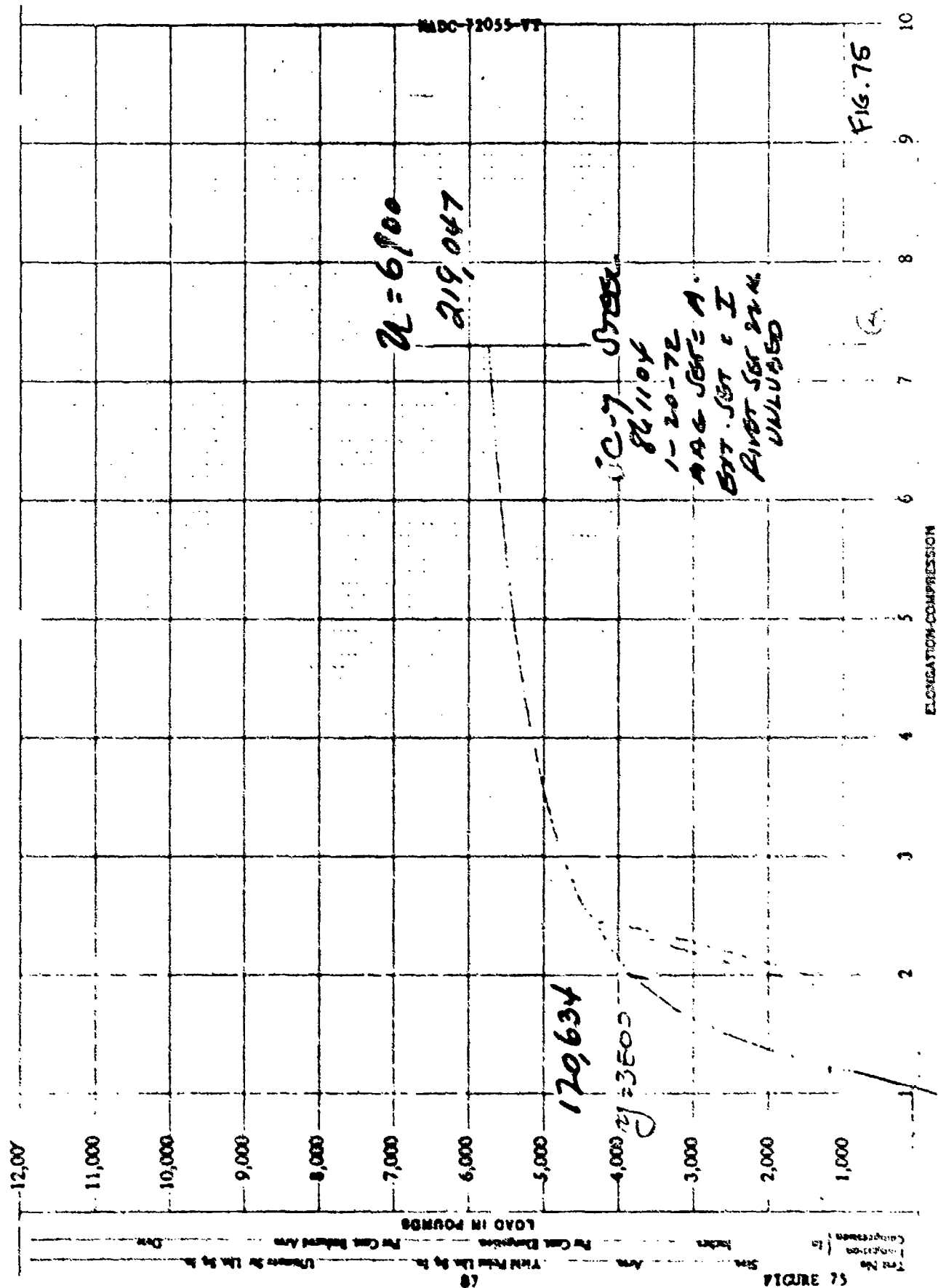
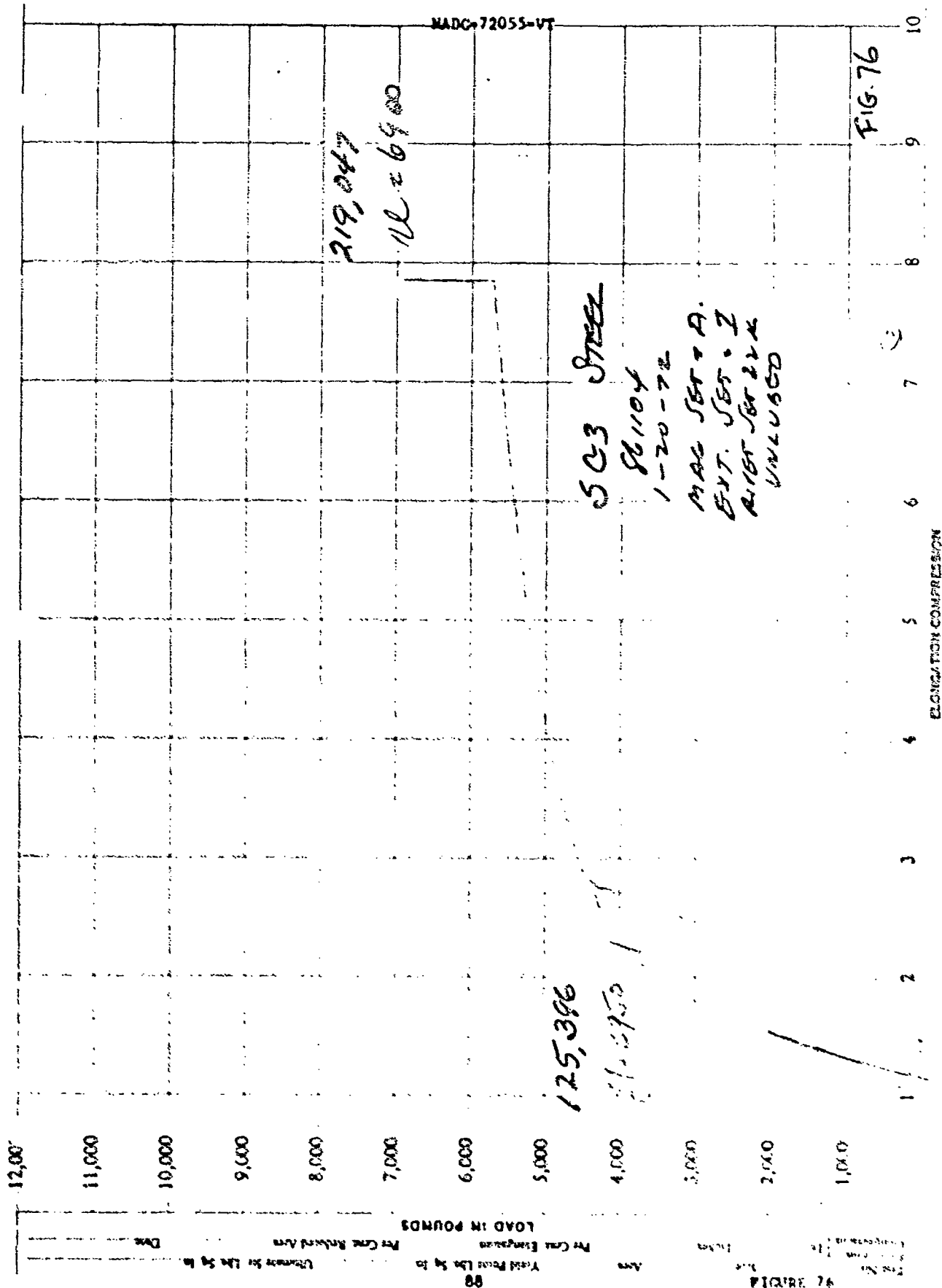


FIGURE 76





226,849

W. 7130

SC-5 STEEL

861104

1-20-72

MAG SET = A

EXT SET = I

RIVER SET = LK

UN/UNGO

128,571

128,571

11,000

10,000

9,000

8,000

7,000

6,000

5,000

4,000

3,000

2,000

1,000

0

11,000
10,000
9,000
8,000
7,000
6,000
5,000
4,000
3,000
2,000
1,000
0

114,285

114,285

196,190

216,6180

804-18 Steel
BB1104
1-20-12
MAG SET A.
BUT SET I
LIVE SET 22K
LAGE

FK 78

9

5

3

1

4

1

2

1

1

10

ELONGATION FORMER SECTION

12.00

11.000

10.000

9.000

8.000

7.000

6.000

5.000

4.000

3.000

2.000

1.000

104,761

104,761

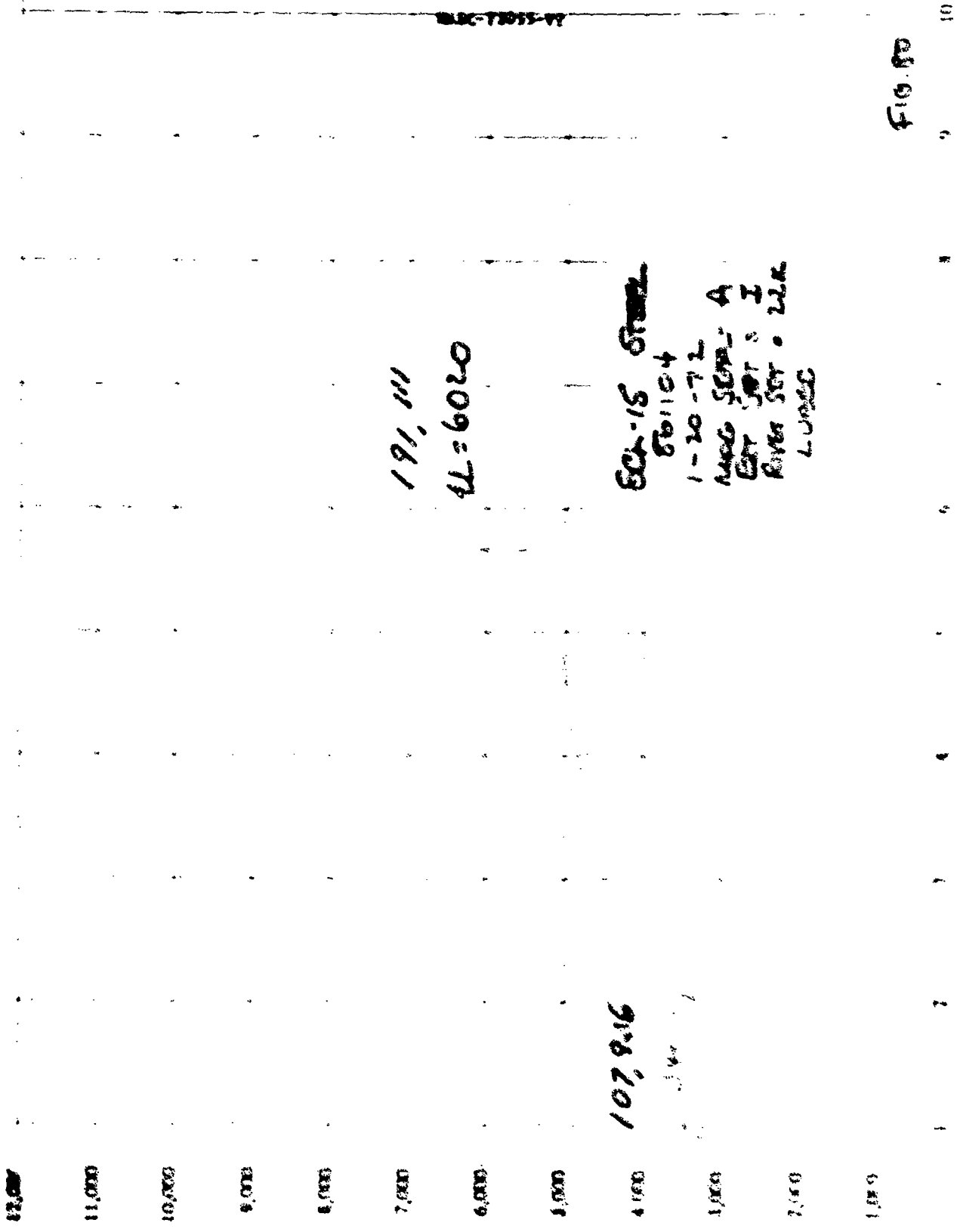
104,761

6-6080
193,015

SC-12 STEEL
861104
1-20-72
MAX. SET A
ENT SET I
RIVER SET = 224
LUBED

FIG. 79

10



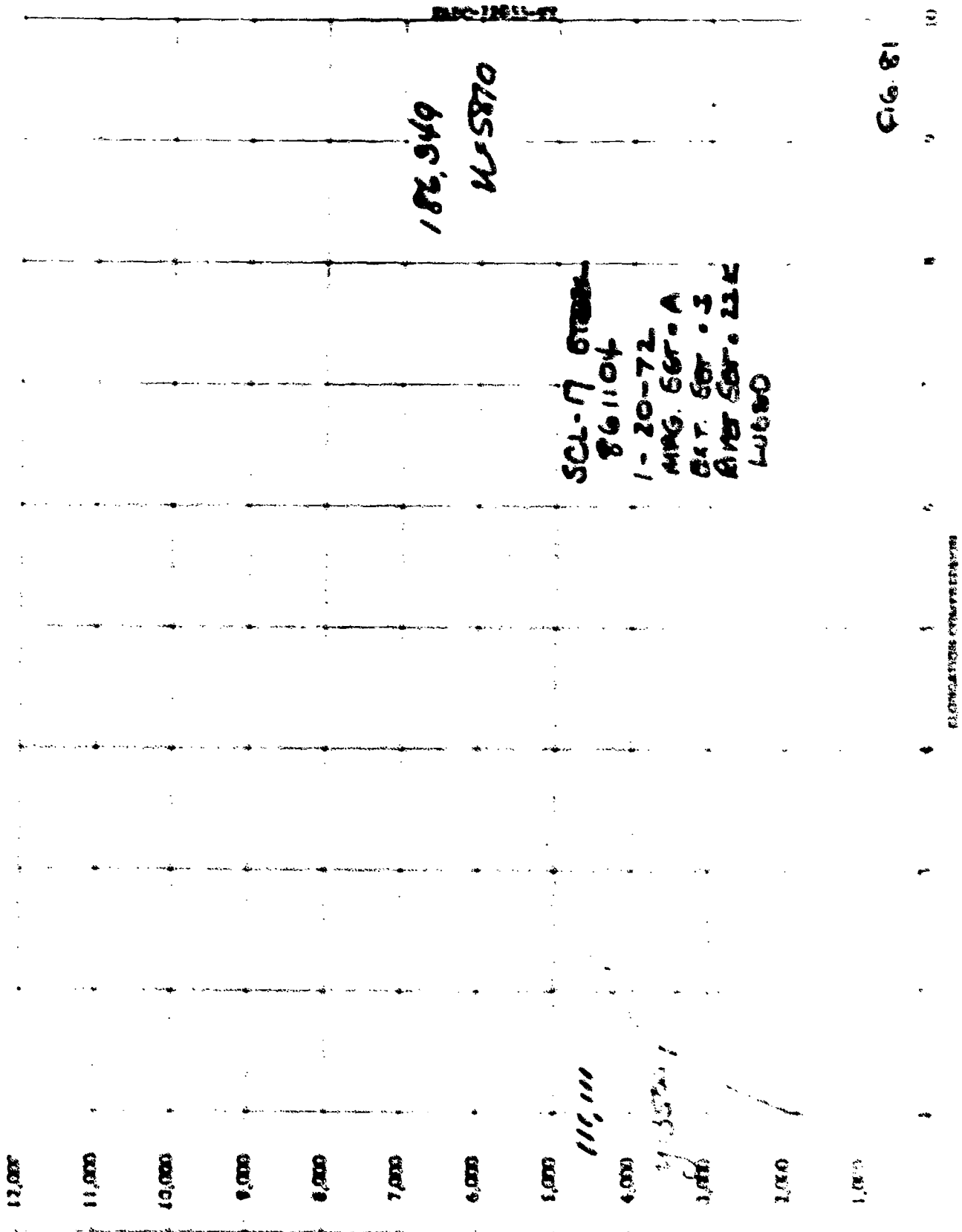
191, 111
 4L=6020

802-15 67022
 861104
 1-20-72
 NADG SERA-A
 EST JOT S I
 River Ser - 22K
 LUNGE

107,916

FIG. 80

CLASSIFICATION CODE: 100-100-100-100



12,000
11,000
10,000
9,000
8,000
7,000
6,000
5,000
4,000
3,000
2,000
1,000

616.81

CALCULATIONS COMPLETED

FIG. 82

10

9

8

7

6

5

4

3

2

1

RECEIVED AT THE OFFICE OF THE SECRETARY OF THE ARMY

801-11 - Sec 22

821104

1-20-72

MAG SET A.

507 SET I

6107 SET 22K

LU920.

205,079

U-6460

111111

111111

12,000

11,000

10,000

9,000

8,000

7,000

6,000

5,000

4,000

3,000

2,000

1,000